LEARNING MATERIAL

OF

ENERGY CONVERSION-II (5TH SEM)

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CHAPTER 1 EC-II NOTES

ELECTRICAL ENGINEERING 5th SEMESTER

(page-1)

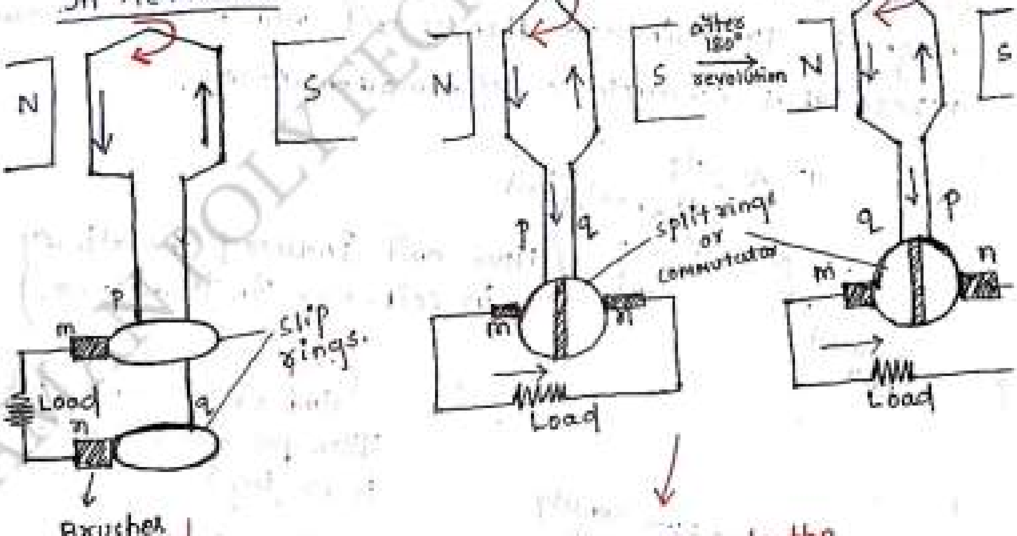
Chapter-1 ALTERNATOR

Q. What is the difference between Ac machine & dc machine?

- The only difference between Ac & dc machine is the commutator due to that only we are not using dc machine for many applications.
- In AC machine slip rings & In dc machine split rings or commutators are used. The commutators used for making the bidirectional Induced voltage in coil to unidirectional across load.

In Ac machine

In dc machine



In slip ring & brush arrangement bidirectional voltage is Induced across load.

(here due to the usage of split ring the load is having unidirectional current flowing through it.)

CHAPTER 1 EC-II NOTES

ELECTRICAL ENGINEERING 5th SEMESTER

(page-2)

- In Ac machine Armature conductor can be placed either in stator or rotor according to the rating of the machine.
- But in dc machine, the conductors have to be placed on the rotor so that commutation can be possible. so In dc Machine we can't place conductors in stator.

Q// 2. What is Faraday's law of electromagnetic Induction & why dc voltage can't be provided to Transformer?

- According to the Faraday's law of electromagnetic Induction if any conductor or coil experiences any rate of change of magnetic flux linkages then an emf will be going to Induced across that conductor or coil. mathematically,

$$e \propto \frac{d\phi}{dt}$$

$$\Rightarrow e = \underbrace{N}_{\text{no of turns of coil}} \frac{d\phi}{dt}$$

Induced emf

(Here emf Induced statically in coil. eg- In Transformer)

(coil is constant in limb of Transformer but flux produced by Ac current is varying)

$$\underbrace{e}_{\text{Induced emf}} \propto \underbrace{B}_{\text{flux density}}$$

$$\Rightarrow e = B l V$$

(Here emf Induced is ~~statically~~ dynamically Induced Voltage eg- In all rotating machines)

here l - length of the active conductor or active length of conductor

(V - Velocity of the active conductor)

Page-3

- Suppose we will provide dc to a transformer then the stationary conductor willn't experience any rate of change of flux linkage $\left(\frac{d\phi}{dt}\right)$ as dc current will produce constant flux which willn't vary w.r.t time. So as $\frac{d\phi}{dt}$ will be zero then,

$$\cancel{e} = N \frac{d\phi}{dt}$$

- So emf induced zero means short circuit of winding so if dc is provided to transformer the windings will burn.

Flemmings Right hand Rule :-

- If any conductor experiences rate of change of magnetic flux linkage then emf will going to induce across that conductor or coil, the direction of induced voltage can be found by Flemming's right hand rule.

where m(I)ddle finger → current.

ThuMb → motion of the conductor w.r.t field

(F)ore finger → Flux

Right hand thumb rule :-

$i \propto \phi$ (Ampere's law) (if μ_r = const) & $i \Rightarrow \phi$ (oersted)

- If my crawling fingers of my right hand will indicate the current then my thumb will indicate the flux & vice versa.

page-4

Basic principle of alternator & the Relation between speed & Frequency :-

- Basic principle of alternator is nothing but the Faraday's law of electromagnetic Induction.

(Imp) (advantages of stationary Armature)

- Here in Alternator field (which will create flux) is rotating & armature conductors are stationary & placed in stator due to the following advantages :-

(1) No need of brush & slip ring arrangement to collect current from armature which is stationary & placed in stator.

(2) Stationary Armature will feel less mechanic stress as it is not rotating. so hard composition Insulating materials needn't to be used so cost of machine will be less.

(3) cooling system can easily be designed with the stationary Armature.

- So In alternator field is rotating & armature conductors are constant, because Armature conductors are placed on stator & field is placed in rotor. As field is rotating in space some induced voltage will be induced in armature conductor in time.

page-5

So relation between speed (space) & frequency (time) is v.v. imp

$$\boxed{N_s = \frac{120f}{P}}$$

where N_s - synchronous speed (It is called synchronous becoz speed & frequency are synchronized)

f - frequency of induced emf in armature conductor

P - no of poles.

- The relation between electrical & mechanical degree is v.v imp (semester)

$$\boxed{\theta_m^{\circ} = \frac{P}{2}\theta_e^{\circ}}$$

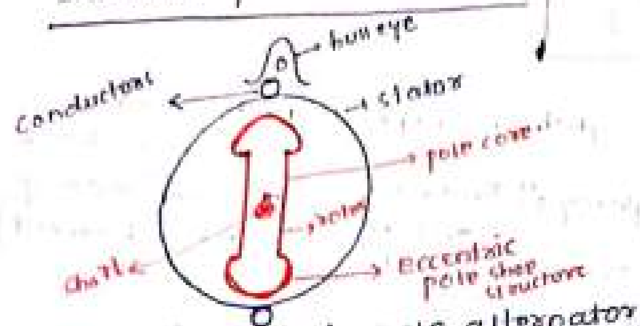
- For 2 pole machine, suppose my rotor will rotated 180° mechanical in space then half cycle of induced voltage will be induced.

Types of Alternator & their constructional features:-

- According to the rotor construction, the alternator is divided into two types -
  - (1) salient pole alternator
  - (2) Cylindrical pole alternator.

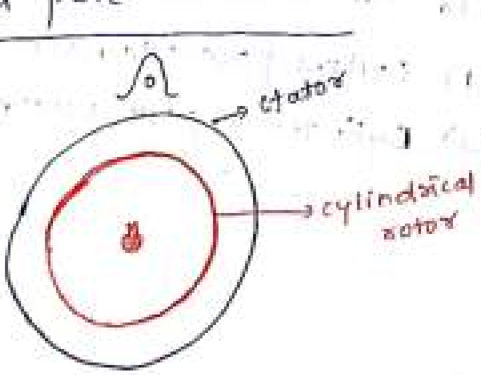
page-6

Salient pole Alternator



- Here In salient pole alternator eccentric pole shoe structure is used.
- Due to saliency or natural air flow the rotor can't rotate faster of the salient pole alternator so this type of rotor is used for less requirement of speed turbines for eg - In hydro turbines ($N_s \downarrow$)
- More no of poles can be Incorporated in salient pole alternator ($\downarrow N_s = \frac{120f}{P\uparrow}$)
- The axial length of the rotor is less but the radial diameter of the rotor is more.

Cylindrical pole alternator

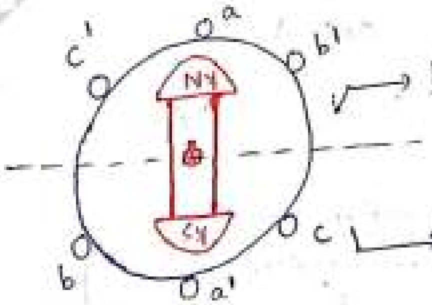


page-7

- In cylindrical pole alternator the rotor can be rotated at higher speeds as saliency (natural air flow) is not there here.
- It can be used for high speed turbine case for eg - In thermal, Nuclear power stations, cylindrical rotor alternators are used. ($N_s \uparrow$)
- Here less poles can be Incorporated. ($\uparrow N_s = \frac{120f}{P\downarrow}$)
- The axial length of the rotor is more & the radial diameter of the rotor is less here.

- Distribution of winding :-

- The winding are distributed uniformly in Armature to make the induced voltage sinusoidal so to reduced harmonics.
- But if the windings are concentrated then, voltage Induced will be not sinusoidal so harmonics will be Induced in the induced voltage.



here the windings of all 3 phases are distributed uniformly in Armature.

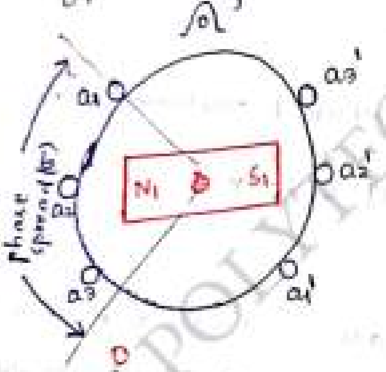
(Here under each pole all 3-phases slots should be there.)

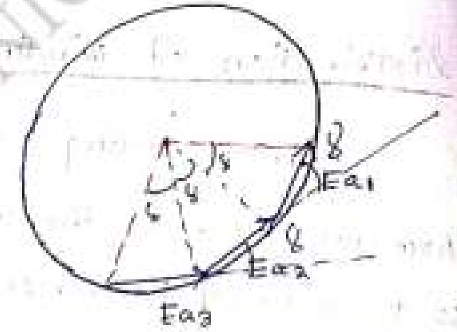
page-8

- Due to distribution of winding the induced emf in armature winding reduced the factor by which the emf is reduced is called distribution factor (Kd)

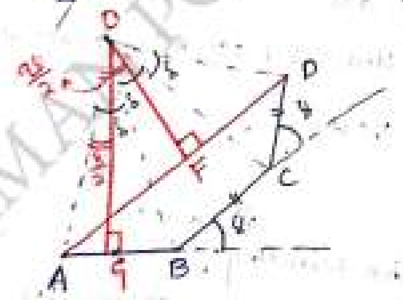
Imp
Distribution factor (Kd) :—

Distribution factor is a factor by which net induced voltage is reduced because of distribution of winding.





here δ – slot angle.



In OAG Δ,

$$\sin\frac{\delta}{2} = \frac{AG}{OA}$$

In OAF Δ,

$$\sin\frac{q\delta}{2} = \frac{AF}{OA}$$

$$K_d = \frac{\text{Induced voltage with distribution winding}}{\text{Induced voltage without distribution of winding}}$$

(means concentrated windings)

page-12

$$= \frac{AD}{q \cdot AB}$$

$$= \frac{2AP}{q \cdot 2AG}$$

$$= \frac{2 \cdot OA \sin\frac{q\delta}{2}}{q\, 2\, OA \sin\frac{\delta}{2}}$$

$$= \frac{\sin\frac{q\delta}{2}}{q \sin\frac{\delta}{2}}.$$

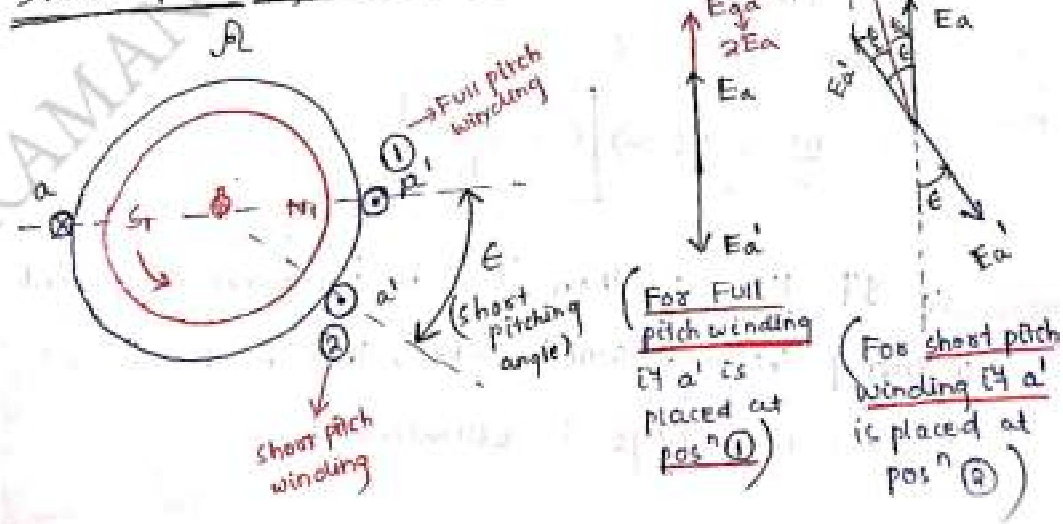
so $\boxed{K_d = \frac{\sin\frac{q\delta}{2}}{q \sin\frac{\delta}{2}}.}$ or K_d is $\frac{\sin\frac{\sigma}{2}}{\sigma/2}$ (where $\sigma = q\delta$ phase spread)

q = slots/pole/phase

$\delta = \frac{180 \times P}{\text{no of slots}}$ = slot angle

(P = no of poles)

short pitching of a coil :-



page-10

Imp

pitch Factor (kp) :-

pitch factor is a factor by which net induced voltage is reduced due to short pitch coils.

$$kp = \frac{\text{Induced Voltage with short pitched coils}}{\text{Induced voltage without short pitch coils or in full pitched coils.}}$$

$$= \frac{2E_a \cos\frac{\epsilon}{2}}{2E_a}$$

$$\Rightarrow \boxed{Kp = \cos\frac{\epsilon}{2}} \longrightarrow \text{(For fundamental)}$$

$$\boxed{Kp_h = \cos\frac{h\epsilon}{2}} \longrightarrow \text{(pitch factor for h-harmonic components)}$$

if $Kp_h = 0$

then $\cos\frac{h\epsilon}{2} = 0$

$$\frac{h\epsilon}{2} = 90 \Rightarrow \boxed{\epsilon = \frac{180}{h}}$$

so if $Kp_h = 0$, then for h-harmonic component induced voltage will be zero, thus h-harmonics induced voltage is elliminated.

page-11

Q. Explain or draw the short pitching angle for which 3rd harmonics Induced voltage will be eliminated?

Ans:- $K_{P_3} = \cos\frac{3\epsilon}{2}$.

$K_{P_3} = 0$ when $\frac{3\epsilon}{2} = 90^\circ$

$\Rightarrow \epsilon = \frac{180}{3} = 60^\circ$

So if $\epsilon = 60^\circ$, then $K_{P_3} = 0$ then Induced Voltage due to 3rd harmonic component is zero.

EMF EQUATION OF ALTERNATOR:—

We know according to Faraday's law —

$e_{cond} = B l v$

$= (B_m \sin\theta) \cdot l \cdot \left(2\pi r \times \frac{N}{60}\right)$ m/sec

rotation per min = N rev.
rotation per 60 sec = N rev.
rotation per sec = $\frac{N}{60}$ rev.
Distance traversed in one revolution = $2\pi r$
So per sec. for $\frac{N}{60}$ revolution the velocity will be → $\left(2\pi r \times \frac{N}{60}\right)$ m/sec

$= \phi \frac{N}{60} \pi \sin\theta$ (as $\phi = 2B_m l r$)

$\Rightarrow e_{cond} = \phi \pi f \sin\omega t$

$\Rightarrow e_{turn} = 2\phi\pi f \sin\omega t$

(Induced voltage per turn when it is full pitched coil & without having any distribution.)

(∵ 1 rev in space = 1 cycle in Time (for 2 pole)

$\frac{N}{60}$ rps = $\frac{N}{60}$ cycles/sec → f

Velocity = (per revolution distance × No of revolution per sec)

→ $2\pi r$, → $\frac{N}{60}$

So velocity = $\left(2\pi r \times \frac{N}{60}\right)$ m/sec.

(page-12)

$e_{coil} = 2\phi \pi f N_{se} \sin \omega t$

$$\Rightarrow \boxed{E_{ph} = \sqrt{2}\, \phi \pi f N_{se} K_p K_d}$$

where E_{ph} = phase Induced voltage

$E_L = \sqrt{3} E_{ph}$ (For star connected alternator)

$E_L = E_{ph}$ (For delta connected alternator)

ϕ = flux.

f = frequency of Induced voltage

N_{se} = No of series connected turns per phase

K_p = pitch factor

K_d = Distribution factor.

Q11 A 3-ϕ, 10 pole, star connected alternator runs at 600 rpm. It has 120 slots with 8 conductors per slot and the conductors of each phase are connected in series. Determine the phase & line emfs if the flux per pole is 56mwb.

Sol^n:- $P = 10$

3-ϕ, Y, $N_s = 600$ rpm

$N_s = \frac{120f}{P}$

Page-13

$\Rightarrow f = \dfrac{N_s \times p}{120}$

$= \dfrac{600 \times 10}{120}$

$= 50Hz.$

Number of series connected turns per phase =

$\left[\left(120 \text{ slots} \times 8 \dfrac{\text{conductors}}{\text{slot}}\right) \times \dfrac{1}{2}\right] \times \dfrac{1}{3} = 160$

Total no. of conductors

$\Rightarrow N_{se} = 160$ turns.

$K_d = \dfrac{\sin \frac{q\delta}{2}}{q \sin\frac{\delta}{2}}$

q = slots/pole/phase

$= 120/10/3$

$= 4$

$= \dfrac{\sin \frac{4 \times 15}{2}}{4 \sin \frac{15}{2}}$

$\delta = \dfrac{180 \times \text{no of poles}}{\text{no of slots}} = \dfrac{180 \times 10}{120}$

slot angle

$= 15°$

$= 0.957$

$K_p = 1$ (As nothing given about short pitching angle so assume full pitch winding)

$E_p = \sqrt{2}\,\pi f \phi N_{se} K_p K_d$

$= \sqrt{2} \times \pi \times 50 \times 56 \times 10^{-3} \times 160 \times 1 \times 0.957$

$= 1904.82$ volts.

$E_L = \sqrt{3}\,E_p = \sqrt{3} \times 1904.82$

$= 3299.25$ volts (Ans)

Page 14

**
Q11 A 3φ, 10pole, delta connected, alternator runs at 600rpm. It has 120 slots with 8 conductors per slot and the conductors of each phase are connected in series. The short pitching angle is 30°. Fi... the flux per pole is sam... the phase & line emfs if the ...

Ans:- 3φ, 10pole, Delta connected

$N_c = 600\,rpm$

$\epsilon = 30°$ (short pitching angle)

$N_s = \frac{120f}{P}$

$\Rightarrow f = \frac{600 \times 10}{120} = 50\,Hz$

Number of series connected turns per phase =

$$\left[\left(120 \text{ slots} \times \frac{8 \text{ conductors}}{\text{slot}}\right) \times \frac{1}{2}\right] \times \frac{1}{3} = 160$$

no of conductors

$K_d = \frac{\sin\frac{q\delta}{2}}{q\sin\frac{\delta}{2}}$

$\delta = \frac{180 \times \text{no of poles}}{\text{no of slots}} = \frac{180 \times 10}{120} = 15°$

$= \frac{\sin\frac{4 \times 15}{2}}{4\sin\frac{15}{2}}$

$q = \text{slots/pole/phase} = 120/10/3 = 4$

$= 0.957$

page 15

$K_p = \cos\frac{\alpha}{2}$

$= \cos\frac{30}{2}$

$= \cos 15$

$= 0.965$

$E_{ph} = \sqrt{2}\,\pi\, f\, \phi\, N_{se}\, K_p\, K_d$

$= \sqrt{2} \times \pi \times 50 \times 56 \times 10^{-3} \times 160 \times 0.965 \times 0.957$

$= 1838.155$ Volts.

$E_L = E_{ph}$

$= 1838.155$ Volts. (Ans)

Armature Resistance :— (R_a)

There are windings which gives some winding resistance, The armature resistance/phase (R_a) causes a voltage drop/phase of IR_a which is in phase with the armature current I. However this voltage drop is practically negligible.

Armature leakage Reactance :—

Due to the leakage flux some voltage drop occurs. Leakage can be modelled with a Inductor & represented as (X_L). The voltage drop across X_L is IX_L which leads exactly 90° to (IR_a).

(page-16)

Due to the load variation the terminal voltage in the alternator varied due to the following reasons :-

1. Voltage drop due to armature resistance (R_a)
2. Voltage drop due to armature leakage reactance (X_L)
3. Voltage drop due to armature reaction

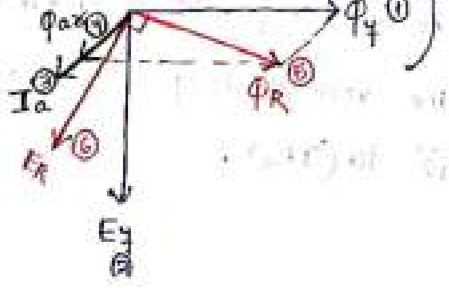
- In transformer armature reaction not occur but in alternator or synchronous machine Armature reaction takes place.

Armature Reaction :-

Effect of armature flux (which is created by the load current after alternator is loaded) on main field flux is called armature reaction.

when the load is lagging :-

(or when Alternator is operating @ lagging power factor).



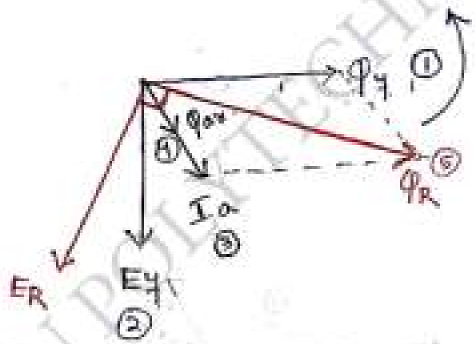
ϕ_f - main field flux
E_f - Induced emf
I_a - Armature current
ϕ_{ar} - Armature flux
ϕ_R - Resultant flux
E_R - Resultant Emf.

page-17

- Due to lagging load, the net resultant flux (ϕ_R) is reduced for which net Induced Voltage (E_R) is reduced. This is called demagnetising armature reaction. So in order to maintain the Induced voltage constant excitation is increased so @ lagging synchronous m/c will be overexcited.

So lagging ⟶ demagnetising Armature reaction ⟶ $\phi_R \downarrow$ ↳ $E_R \downarrow$ → overexcited synchronous m/c.

when the load is leading :-
(or when alternator is operated at leading power factor)

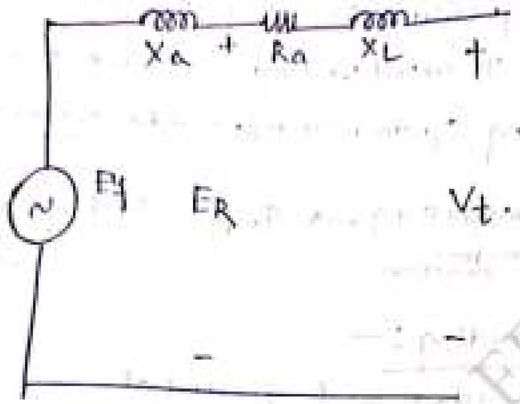


ϕ_f - main field flux
E_f - Induced emf @ no load
I_a - Armature current/ load current
ϕ_{ar} - Armature flux
ϕ_R - Resultant flux
E_R - Resultant emf.

- Due to leading load, the net resultant flux (ϕ_R) is increased for which net Induced voltage (E_R) is Increased which is called magnetising Armature reaction. So in order to maintain the Induced voltage the excitation of the alternator is reduced so @ leading alternator will be under excited.

page-18

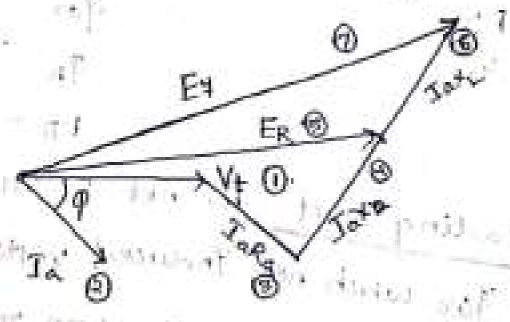
Vector Diagram of loaded Alternator :-



where
E_f - Internal Induced Voltage
R_a - Armature Resistance
X_L - Armature leakage Reactance
X_a - Reactance of Armature reaction

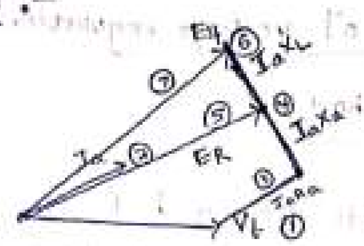
So $E_f = V_t + I_aR_a + I_aX_L + I_aX_a$

So @ lagging pf :-

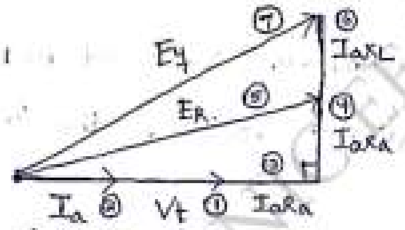


page-19

SO @ leading pf load :-



@ unity pf load :-



Voltage Regulation :-

- The magnitude of the terminal voltage depends not only on the load but also on its power factor.

- So voltage regulation is defined as, the rise in voltage when full-load is removed (field excitation & speed remaining the same) divided by the rated terminal voltage.

$$\% \text{ regulation} = \frac{E_0 - V}{V} \times 100$$

- In case of leading power factor, terminal voltage will fall on removing the full-load. Hence regulation is negative in that case.

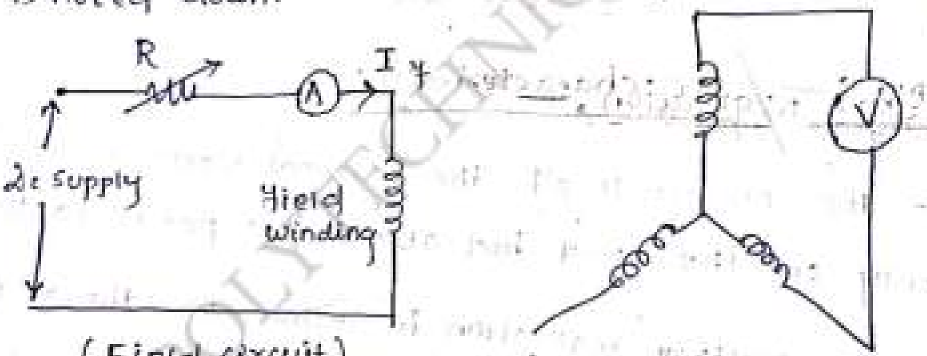
page-20 Imp for exams

Determination of voltage regulation by synchronous Impedance method :-

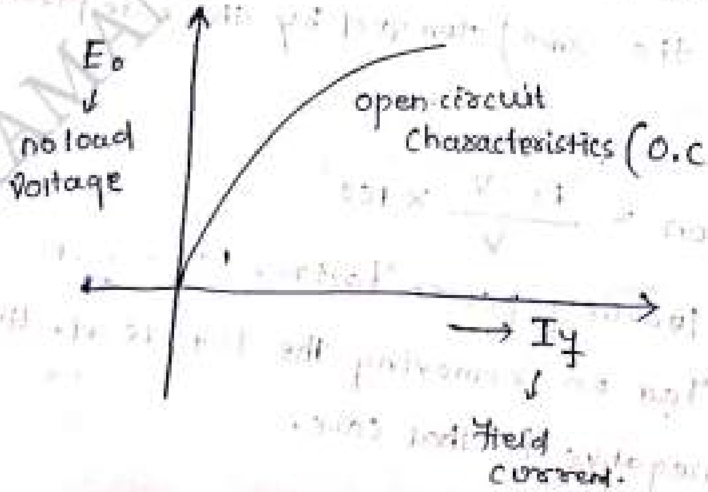
In this method both O.C (open circuit) & S.C short circuit tests is to be performed & the armature resistance is to be determined.

O.C Test :-

Here the alternator runs at noload & rated speed the field excitation is varied & the Induced voltage is noted down.



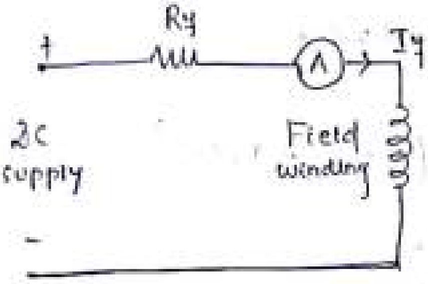
(Field circuit) (Armature circuit)



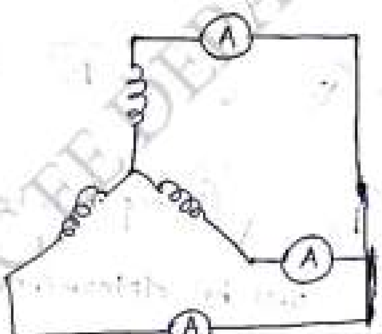
(page-21)

S.C. Test :-

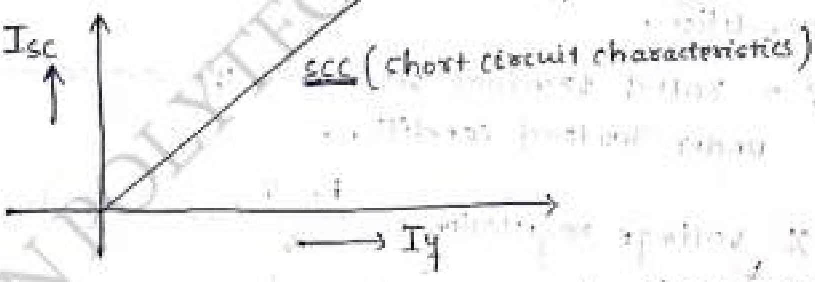
It is obtained by short-circuiting the armature (i.e stator) windings through a low-resistance ammeter. The excitation current (I_f) & I_{sc} (short circuit current) is plotted.



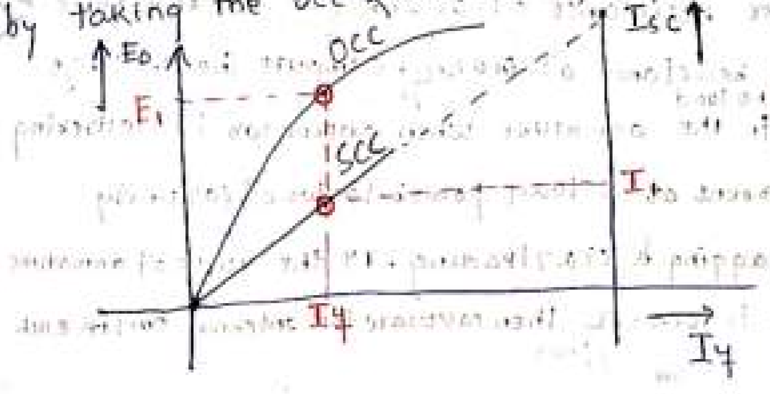
(Field circuit)



(Armature circuit)



The synchronous impedance Z_s will be determined by taking the OCC & SCC jointly as below.



page-22

Z_s = synchronous Impedance = $\frac{E_1}{I_1}$

i.e, $Z_s = \frac{E_1(O.C)}{I_1(S.C)}$

'R_a' (Armature resistance can be found by using Voltmeter - ammeter method.

$X_s = \sqrt{Z_s^2 - R_a^2}$ is found and

$E_0 = \sqrt{(V\cos\phi + I_aR_a)^2 + (V\sin\phi + I_aX_s)^2}$

will be determined.

I_a = rated current of armature under full load condition.

V = rated terminal voltage of the alternator under full load condition.

% voltage regulation = $\frac{E_0 - V}{V} \times 100$ will be found.

Imp 10 marks

Q11 A 60KVA, 220V, 50HZ, Y connected, 3-φ Alternator has effective armature resistance of 0.016 Ω/phase & an armature leakage reactance of 0.07 Ω/phase. Compute the voltage induced at no load in the armature when alternator is delivering rated current at a load power factor of (a) unity (b) 0.7 lagging & (c) 0.7 leading. If the value of armature reaction reactance is 0.05 Ω/phase then calculate the Internal emf in each case.

page 23

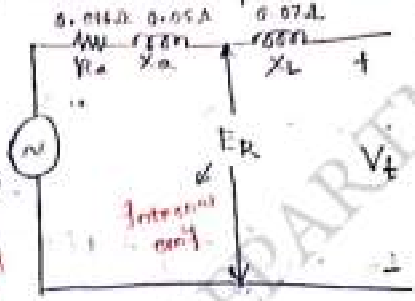
Solⁿ:-

60 kVA, 220V, 50Hz, Y connected, 3-φ alternator,

R_a = 0.016 Ω/phase

X_L = 0.07 Ω/phase

X_a = 0.05 Ω/phase



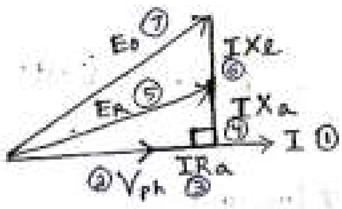
$P = \sqrt{3} V_L I_L$

$I_L = \frac{P}{\sqrt{3} V_L}$

$= \frac{60 \times 10^3}{\sqrt{3} \times 220}$ $\quad V_{ph} = \frac{V_L}{\sqrt{3}} = 127.01V$

$= 157.45$ Amp.

@ unity pf



$$E_R = \sqrt{(V_{ph} + IR_a)^2 + (IX_a)^2}$$

$$= \sqrt{(127.01 + 157.45 \times 0.016)^2 + (157.45 \times 0.05)^2}$$

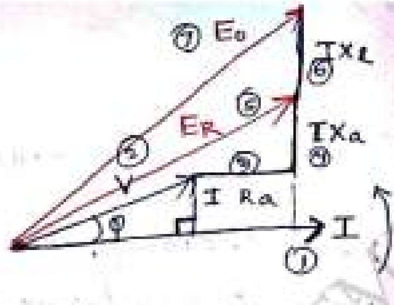
$= 129.76$ volts (Internal emf)

$$E_0 = \sqrt{(V_{ph} + IR_a)^2 + (IX_a + IX_L)^2}$$

$$= \sqrt{(127.01 + 157.45 \times 0.016)^2 + (157.45 \times 0.05 + 157.45 \times 0.07)^2}$$

$= 130.87$ (No load emf)

page-24



@ 0.7 lagging

$$\varphi = \cos^{-1}(0.7) = 45.57^\circ$$

$$E_R = \sqrt{(V\cos\varphi + IR_a)^2 + (V\sin\varphi + IX_a)^2}$$

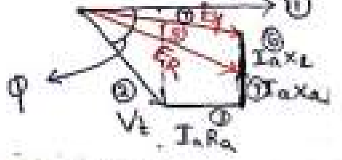
(Internal Induced Voltage)

$$= \sqrt{(127.01\times 0.7 + 157.45\times 0.016)^2 + (127.01\times 0.714 + 157.45\times 0.05)^2}$$

$$= 134.43 \text{ Volts.}$$

@ 0.7 leading

$$\varphi = \cos^{-1}(0.7) = 45.57^\circ$$



$$E_R = \sqrt{(V_t\cos\varphi + I_aR_a)^2 + (V_t\sin\varphi - I_aX_a)^2}$$

$$= \sqrt{(127.01\times 0.7 + 157.45\times 0.016)^2 + (127.01\times 0.714 - 157.45\times 0.05)^2}$$

$$= 123.35 \text{ Volts.}$$

CHAPTER 1 EC-II NOTES

ELECTRICAL ENGINEERING 5th SEMESTER

page-25

$$E_f = \sqrt{(V_t\cos\phi + I_a R_a)^2 + (V_t\sin\phi - I_a X_a - I_a X_L)^2}$$

$$= \sqrt{(127.01\times 0.7 + 157.45\times 0.016)^2 + (127.01\times 0.714 - 157.45\times 0.05 - 157.45\times 0.07)^2}$$

$$= 116.24 \text{ Volts. (Ans)}$$

Q. A 100KVA, 3000V, 50Hz, 3-phase, star connected alternator has effective armature resistance of 0.2 ohm. The field current of 40A produces short-circuit current of 200Amp, and an open-circuit emf of 1040V (line value). Calculate the full-load voltage regulation at 0.8 pf lagging and 0.8 pf leading. draw phasor diagrams.

Sol:- 100KVA, 3000V, 50Hz, 3-φ, Y connected alternator, $R_a = 0.2$ ohm

$I_f = 40A$, $I_{sc} = 200$ Amp, $(E_0)_{Line} = 1040V$

$$(E_0)_{ph} = \frac{(E_0)_{Line}}{\sqrt{3}} = \frac{1040}{\sqrt{3}} = 600.44 \text{ Volts.}$$

$$V_{ph} = \frac{3000}{\sqrt{3}} = 1732.05 \text{ Volts.}$$

$$P = \sqrt{3} V_L I_L$$

$$I_L = \frac{P}{\sqrt{3} V_L}$$

$$= \frac{100\times 10^9}{\sqrt{3}\times 3000} = 19.24 \text{ Amp}$$

page-26

$$Z_s = \frac{(E_0)_{ph}}{I_{sc}}$$

$$= \frac{600.44}{200}$$

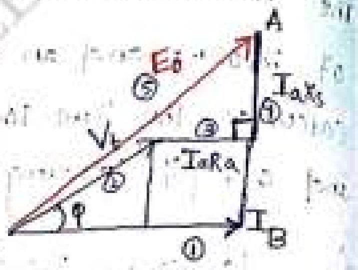
$$= 3.0022\,\Omega$$

$$X_s = \sqrt{Z_s^2 - R_a^2}$$

$$= \sqrt{(3.0022)^2 - (0.2)^2}$$

$$= 2.995\,\Omega$$

@ 0.8 pf lagging



In OAB triangle

$$OA = \sqrt{(OB)^2 + (AB)^2}$$

$$\Rightarrow E_0 = \sqrt{(V_t\cos\varphi + I_aR_a)^2 + (V_t\sin\varphi + I_aX_s)^2}$$

$$= \sqrt{(1732.05\times 0.8 + 19.24\times 0.2)^2 + (1732.05\times 0.6 + 19.24\times 2.995)^2}$$

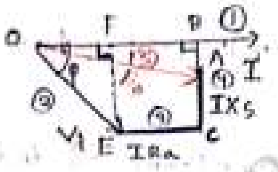
$$= 1770.24\,V$$

$$\%\text{ Voltage Regulation} = \frac{E_0 - V}{V}\times 100$$

$$= \frac{1770.24 - 1732.05}{1732.05}\times 100 = 2.204\%$$

page-27

@ 0.8 pf leading



In OAB triangle,

$$OA = \sqrt{(OB)^2 + (CB - AC)^2}$$

(AB)

[here BC = EF = $V_t \sin\phi$] (In DEF triangle)

$$= \sqrt{(V_t \cos\phi + I R_a)^2 + (V_t \sin\phi - I X_s)^2}$$

$$= \sqrt{(1732.05 \times 0.8 + 19.24 \times 0.2)^2 + (1732.05 \times 0.6 - 19.24 \times 2.115)^2}$$

= 1701.24 Volts.

$$\% \text{ Voltage Regulation} = \frac{E_0 - V}{V} \times 100$$

$$= \frac{1701.24 - 1732.05}{1732.05} \times 100$$

$= -1.778\%$ (Ans)

NOTE:-

In leading load the voltage regulation of the alternator becomes negative.

page-28

Imp 2marks

condition For parallel operation of Alternator with infinite bus bar

① - waveform of induced voltage of parallely connected alternators should be same.

② Frequency of all parallely connected synchronous machines should be same.

③ phase sequence of all parallely connected alternators should be same.

Chapter-1, 2 marks Alternator

1. State pitch factor (chording factor) and distribution factor.
2. what do you mean by voltage regulation of Alternator?
3. What are the types of alternator?
4. Which type of alternator is used in Hydroelectric power plants & why?
5. calculate the pitch factor for the winding of a stator having 36 slots, 4 poles, coil span 1 to 8.
6. At zero pf lagging load synchronous alternator is magnetising or demagnetising in nature?
7. calculate the distribution factor for a 36-slots, 4 pole, single layer 3-phase winding.
8. what are the conditions for parallel operation of a 3-φ Alternator into an infinite bus bar?
9. In which type of load, the voltage regulation of an alternator becomes negative?
10. what is the function of damper winding in an alternator?
11. An overexcited alternator gives current at which power factor.
12. The dc armature resistance of a delta connected alternator measured across its two terminals is 1Ω. what is the per phase dc resistance.
13. what is up-voltage regulation of alternator!

Chapter-1 10 marks Alternator

1. What is voltage regulation of an alternator? How do you find the voltage regulation of an alternator by synchronous Impedance method.
2. Describe about armature reaction of Alternator?
3. A 3φ, 50HZ star connected 2000KVA, 2300V alternator gives a short circuit current of 600Amp. For a certain field excitation, with the same excitation the open circuit voltage was 900V. The resistance between a pair of terminal was 0.12Ω. Find the full load regulation at (i) UPF (ii) 0.8 pf lagging.

(4) A 3φ, 10pole, Y connected alternator runs at 600rpm. It has 120 stator slots with 8 conductors per slot and the conductors of each phase are connected in series. Determine the phase & line emfs if the flux per pole is 56 mwb. Assume full pitch coils.

5. In a 50kVA, star connected, 400V, 3-φ, 50Hz alternator, the effective armature resistance is 0.25Ω/phase. The synchronous reactance is 3.2Ω/phase & leakage reactance is 0.5Ω/phase. Determine at rated load & UPF,

(i) Internal emf

(ii) No load emf

(iii) % voltage regulation on full load.

chapter-1 6 marks Alternator

1. A 500V, 50 KVA, 1-φ alternator has an effective resistance of 0.2Ω. A field current of 12Amp produces an armature current of 200A on short circuit and an emf of 450V on open circuit. Calculate the full load regulation at 0.8 pf lagging.
2. Derive the emf equation of alternator from 1st principle.

CHAPTER-2

SYNCHRONOUS MOTOR

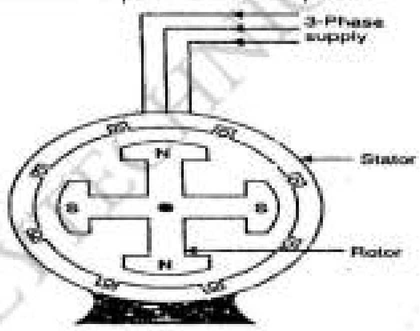
Constructional feature of Synchronous Motor:

A synchronous motor is a machine that operates at synchronous speed and converts electrical energy into mechanical energy. As the name implies, a synchronous motor runs at synchronous speed (Ns = 120f/P) i.e., in synchronism with the revolving field produced by the 3-phase supply.

Like an alternator, a synchronous motor has the following **two** parts:

(i) ***A stator*** which houses 3-phase armature winding in the slots of the stator core and receives power from a 3-phase supply.

(ii) ***A rotor*** that has a set of salient poles excited by direct current to form alternate N and S poles. The exciting coils are connected in series to two slip rings and direct current is fed into the winding from an external exciter mounted on the rotor shaft. The stator is wound for the same number of poles as the rotor poles.



Some salient features of a synchronous motor are:

(i) A synchronous motor runs at synchronous speed. Its speed is constant (synchronous speed) at all loads. The only way to change its speed is to alter the supply frequency (Ns = 120 f/P).

(ii) The characteristic of a synchronous motor is that it can be made to operate over a wide range of power factors (lagging, unity or leading) by adjustment of its field excitation. Therefore, a synchronous motor can be made to carry the mechanical load at constant speed and at the same time improve the power factor of the system.

(iii) Synchronous motors are generally of the salient pole type.

(iv) A synchronous motor is not self-starting and an auxiliary means has to be used for starting it.

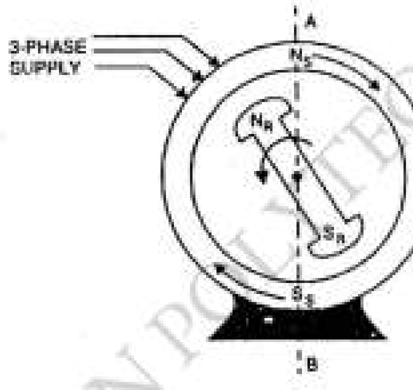
CHAPTER 2 EC-II NOTES

EE 5th SEMESTER

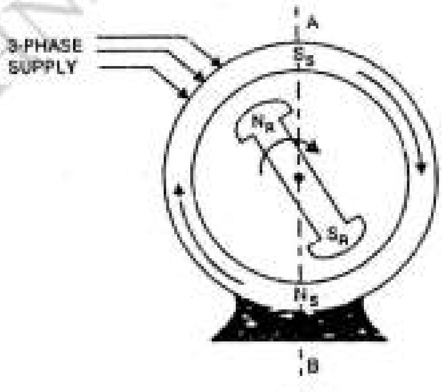
Principles of operation:

Consider a 3-phase synchronous motor having two rotor poles N_R and S_R. Then the stator will also be wound for two poles N_S and S_S. The armature winding of a 3-phase synchronous motor is connected to a suitable balanced 3-phase source and the field winding to a D.C source of rated voltage. When a 3 phase armature winding is fed by a 3 phase supply then a magnetic field of constant magnitude but rotating synchronous speed is produced in the stator. Consider two stator pole Ns and Ss rotating at synchronous speed in clockwise direction. The direct current sets up a two-pole field which is stationary. Thus, there exists a pair of revolving armature poles (i.e., N_S- S_S) and a pair of stationary rotor poles (i.e., N_R- S_R).

Suppose at any instant, the stator poles are at positions A and B as shown in Fig.(i). It is clear that poles N_S and N_R as well as the poles S_S and S_R will repel each other. Therefore, the rotor tends to move in the anticlockwise direction. After a period of half-cycle (or 1/2f = 1/100 second), the polarities of the stator poles are reversed but the polarities of the rotor poles remain the same as shown in Fig.(ii). Now S_S attracts N_R and N_S attracts S_R. Therefore, the rotor tends to move in the clockwise direction. Since the stator poles change their polarities rapidly, they tend to pull the rotor first in one direction and then after a period of half-cycle in the other. Due to high inertia of the rotor, the motor fails to start.



(i)



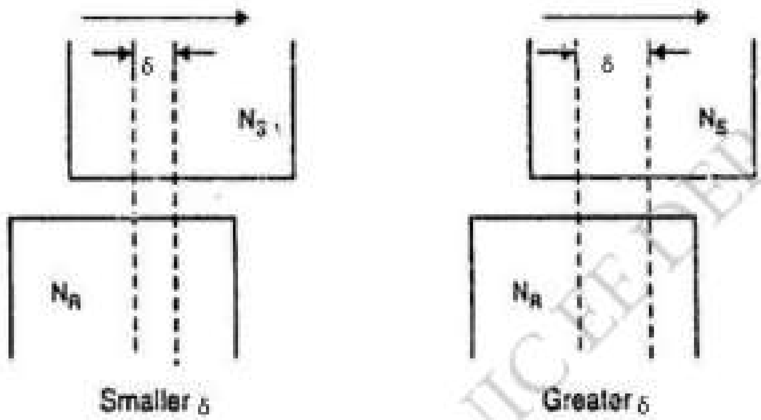
(ii)

Hence, a synchronous motor has no self-starting torque i.e., a synchronous motor cannot start by itself.

Motor on Load:

In d.c. motors and induction motors, an addition of load causes the motor speed to decrease. The decrease in speed reduces the counter e.m.f. enough so that additional current is drawn from the source to carry the increased load at a reduced speed. This action cannot take place in a synchronous motor because it runs at a constant speed (i.e., synchronous speed) at all loads.

The rotor poles fall slightly behind the stator poles while continuing to run at synchronous speed. The angular displacement between stator and rotor poles (called torque angle δ) causes the phase of back e.m.f. Eb to change w.r.t. supply voltage V. This increases the net e.m.f. Er in the stator winding. Consequently, stator current Ia (= Er/Zs) increases to carry the load.



The following points may be noted in synchronous motor operation:

i. A synchronous motor runs at synchronous speed at all loads. It meets the increased load not by a decrease in speed but by the relative shift between stator and rotor poles i.e., by the adjustment of torque angle δ.
ii. If the load on the motor increases, the torque angle δ also increases (i.e., rotor poles lag behind the stator poles by a greater angle) but the motor continues to run at synchronous speed. The increase in torque angle δ causes a greater phase shift of back e.m.f. Eb w.r.t. supply voltage V. This increases the net voltage Er in the stator winding. Consequently, armature current Ia (= Er/Zs) increases to meet the load demand.
iii. If the load on the motor decreases, the torque angle δ also decreases. This causes a smaller phase shift of Eb w.r.t. V. Consequently, the net voltage Erin the stator winding decreases and so does the armature current Ia (=Er/Zs).

Load angle (or Torque angle):

The load angle is defined as the angle between Induced EMF and terminal voltage.For a synchronous generator, rotor field and stator field are rotated at synchronous speed. These two fields are not fully aligned. The stator field lags the rotor field. This lagging expressed in angle is called ***load angle***. This angle is represented by δ.

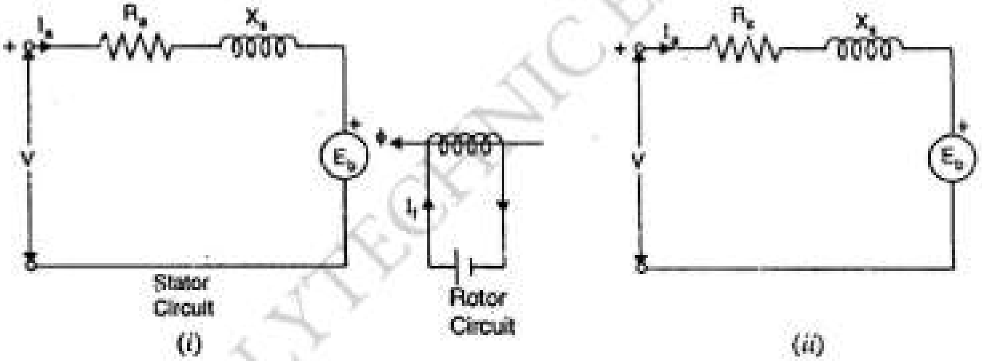
The power developed by the generator is directly proportional to sine of this angle. This angle plays an important role for the stability of the generator. If the angle goes beyond 90º, the generator becomes unstable. This may happen when sudden change of large load occurs or fault sustains longer time.

For the case of synchronous motor, the angle is called ***torque angle*** and the **rotor field lags the stator field** in this case.

Equivalent Circuit:

The synchronous motor is connected to two electrical systems; a d.c. source at the rotor terminals and an a.c. system at the stator terminals.

1. Under normal conditions of synchronous motor operation, no voltage is induced in the rotor by the stator field because the rotor winding is rotating at the same speed as the stator field. Only the impressed direct current is present in the rotor winding and ohmic resistance of this winding is the only opposition to it as shown in Fig.(i).
2. In the stator winding, two effects are to be considered, the effect of stator field on the stator winding and the effect of the rotor field cutting the stator conductors at synchronous speed.



i. The effect of stator field on the stator (or armature) conductors is accounted for by including an inductive reactance in the armature winding. This is called synchronous reactance Xs. A resistance Ra must be considered to be in series with this reactance to account for the copper losses in the stator or armature winding. This resistance combines with synchronous reactance and gives the synchronous impedance of the machine.
ii. The second effect is that a voltage is generated in the stator winding by the synchronously-revolving field of the rotor as shown in Fig.(ii).This generated e.m.f. E_b is known as back e.m.f. and opposes the stator voltage V. The magnitude of Eb depends upon rotor speed and rotor fluxΦ per pole. Since rotor speed is constant; the value of Eb depends upon the rotor flux per pole i.e. exciting rotor current I_f.

For synchronous motor

$$V = E_b + I_a Z_s$$
$$V = E_b + I_a(R_a + jX_s)$$
$$E_b = V - I_a R_a - jI_a X_s$$
$$Z_s = \sqrt{R_a^2 + X_s^2}$$

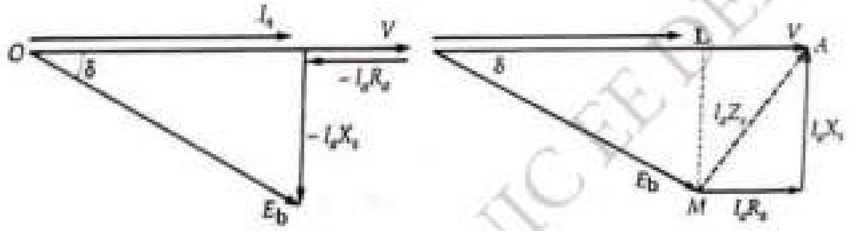
A synchronous motor is said to be normally excited if the field excitation is such that $E_b = V$. If the field excitation is such that $E_b < V$, the motor is said to be under-excited. The motor is said to be over-excited if the field excitation is such that $E_b > V$.

For both normal and under excitation, the motor has lagging power factor. However, for over-excitation, the motor has leading power factor.

Phasor Diagram of a Cylindrical Rotor Synchronous Motor:

Unity power factor:

At unity power factor, the current I, drawn by the motor is in phase with supply voltage V.

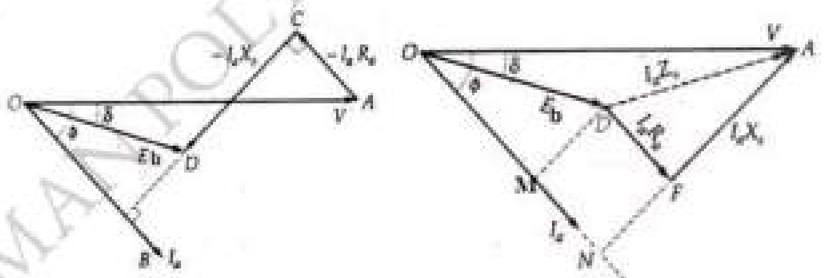


$$OM^2 = OL^2 + LM^2$$

$$E_b^{\,2} = (V - I_aR_a)^2 + (I_aX_s)^2$$

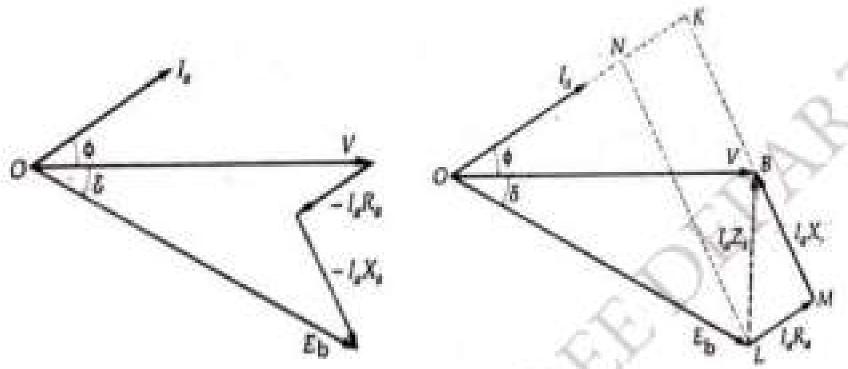
Lagging power factor cosΦ:

Suppose that the synchronous motor is taking a lagging current from the supply. V is taken as reference phasor. For lagging power factor cos Φ, the direction of armature current I, lags behind V by an angle Φ.



$$OD^2 = OM^2 + MD^2 = OM^2 + NF^2$$
$$= (ON - MN)^2 + (NA - FA)^2$$
$$E_b^2 = (VCOS\emptyset - I_aR_a)^2 + (Vsin\emptyset - I_aX_s)^2$$

Leading power factor cosΦ:
When the motor is operating at leading power factor cosΦ, the current I_a drawn by the motor leads the supply voltage V by the phase angle Φ.



$OL^2 = ON^2 + NL^2 = (OK-NK)^2 + (KB+BM)^2$

$$E_b^2 = (VCOS\phi - I_aR_a)^2 + (Vsin\phi + I_aX_s)^2$$

Determination of Eb, by using complex algebra:

Let **V** be taken as reference phasor.

$$\therefore \qquad \mathbf{V} = V\angle 0^\circ = V + j0$$

For lagging power factor cos ϕ

$$\mathbf{I}_a = I_a\angle -\phi = I_a\cos\phi - j\,I_a\sin\phi$$

For unity power factor

$$\mathbf{I}_a = I_a\angle 0^\circ = I_a + j0$$

For leading power factor

$$I_a = I_a\angle +\phi = I_a\cos\phi + j\,I_a\sin\phi$$

The synchronous impedance is given by

$$\mathbf{Z} = R_a + jX_s$$

The Back emf is given by

$$E_b = V - I_a Z_s$$

For lagging power factor $\cos\phi$

$$E_b\angle\delta = V\angle 0^\circ - (I_a\angle -\phi)(R_a + jX_s)$$
$$= V + j0 - (I_a\cos\phi - jI_a\sin\phi)(R_a + jX_s)$$
$$= (V - I_a R_a\cos\phi - I_a X_s\sin\phi) - j(I_a X_s\cos\phi - I_a R_a\sin\phi)$$

$$E_b = \sqrt{(V - I_a R_a\cos\phi - I_a X_s\sin\phi)^2 + (I_a X_s\cos\phi - I_a R_a\sin\phi)^2}$$

$$\delta = \tan^{-1}\frac{I_a R_a\sin\phi - I_a X_s\cos\phi}{V - I_a R_a\cos\phi - I_a X_s\sin\phi}$$

Similarly, *for leading power factor* $\cos\phi$

$$E_b = \sqrt{(V - I_a R_a\cos\phi + I_a X_s\sin\phi)^2 + (I_a X_s\cos\phi + I_a R_a\sin\phi)^2}$$

$$\delta = -\tan^{-1}\left(\frac{I_a X_s\cos\phi + I_a R_a\sin\phi}{V - I_a R_a\cos\phi + I_a X_s\sin\phi}\right)$$

For *unity power factor* $(\cos\phi = 1)$

$$E_b = \sqrt{(V - I_a R_a)^2 + (I_a X_s)^2}$$

$$\delta = -\tan^{-1}\left(\frac{I_a X_s}{V - I_a R_a}\right)$$

Synchronous Motor Torque:

The following torques are considered in the selection of a synchronous motor for a particular application:

1. Locked-rotor torque
2. Running torque
3. Pull-in torque
4. Pull-out torque

Locked Rotor Torque

It is the minimum torque at any angular rotor position that is developed with the rotor locked (i.e., stationary) and rated voltage at rated frequency is applied to the terminals. This torque is provided by the stator windings.

Running Torque

It is the torque developed by the motor under running conditions. It is determined by the power rating and speed of the driven machine.

Pull-in torque

A synchronous motor is started as induction motor till it runs 2 to 5 percent below the synchronous speed. The d.c. excitation is then applied and the rotor pulls into step with the synchronously rotating stator field. The pull-in torque is the maximum constant torque at rated voltage and frequency under which a motor will pull a connected load into synchronism when the d.c. motor excitation is applied.

Pull-out torque

It is the maximum value of torque which a synchronous motor can develop at rated voltage and frequency without losing synchronism.

If T_g is the gross armature torque developed by the motor,

$$T_g \times 2\pi N_s = P_m$$

$$T_g = \frac{P_m}{2\pi N_s} (N_s \ in \ rps)$$

$$T_g = \frac{P_m}{2\pi Ns/_{60}} (N_s \ in \ rpm)$$

$$T_g = \frac{60}{2\pi} \times \frac{P_m}{N_s}$$

Gross torque, $T_g = 9.55 \frac{P_m}{N_s} \ N-m$

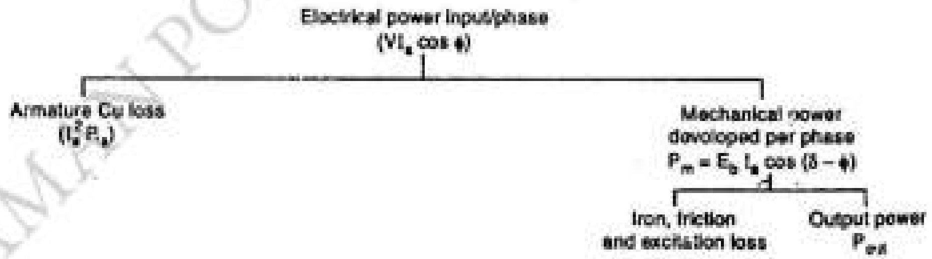
Where P_m =Gross motor output in watts = $E_b I_a cos(\delta - \emptyset)$

N_s = Synchronous speed in r.p.m.

Shaft torque = $T_{sh} = 9.55 \frac{P_{out}}{N_s} \ N-m$

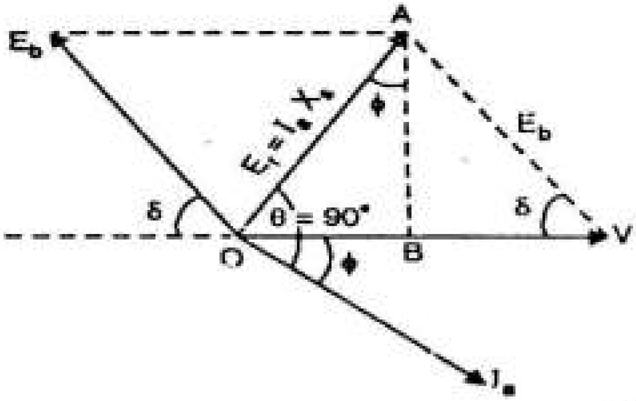
It may be seen that torque is directly proportional to the mechanical power because rotor speed (i.e., Ns) is fixed.

Mechanical Power Developed by Motor:



Power Developed by a Cylindrical rotor Synchronous Motor:

Except for very small machines, the armature resistance of a synchronous motor is negligible as compared to its synchronous reactance. The phasor diagram of an under-excited synchronous motor driving a mechanical load neglecting the armature resistance is shown below.



Since armature resistance Ra is assumed zero. $\tan\theta = \frac{X_s}{R_a} = \infty$

and hence $\theta = 90°$

Input power/phase = $VI_a cos\emptyset$

Since Ra is assumed zero, stator Cu loss $(I_a{}^2R_a)$ will be zero. Hence input power is equal to the mechanical power Pm developed by the motor.

Mechanical power developed/ phase, $P_m = VI_a cos\emptyset$

From the phasor diagram

AB $= E_r cos\emptyset = I_a X_s cos\emptyset$

Also AB $= E_b sin\delta$

$I_a X_s cos\emptyset = E_b sin\delta$

$$I_a\ cos\emptyset = \frac{E_b sin\delta}{X_s}$$

$$P_m = \frac{VE_b sin\delta}{X_s}\ per\ phase$$

$$P_m = \frac{3VE_b sin\delta}{X_s}\ for\ 3\ phase$$

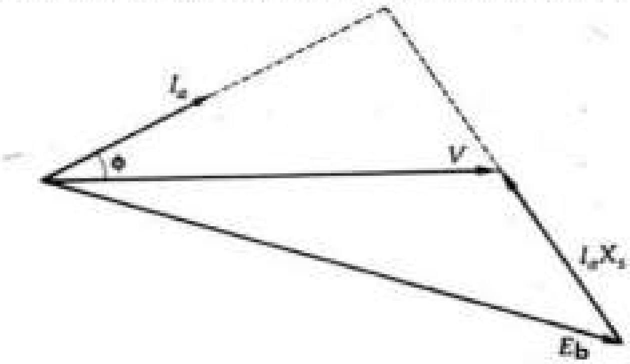
It is clear from the above relation that mechanical power increases with torque angle (in electrical degrees) and its maximum value is reached when d = 90°(electrical).

$$P_{max} = \frac{VE_b}{X_s}$$

Effect of varying load with constant excitation:

A synchronous motor runs at absolutely constant synchronous speed, regardless of the load. Let us examine the effect of load change on the motor.

Consider a synchronous motor operating initially with a leading power factor. The phasor diagram for leading power factor neglecting Ra is shown below.

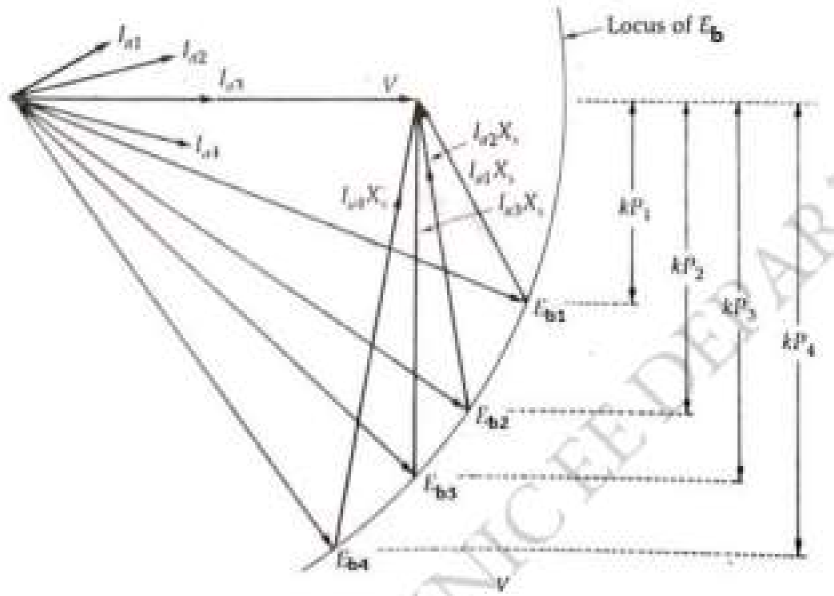


Suppose that the load on the shaft is increased. The rotor slows down momentarily since it takes some time for the motor to take increased power from the line. In other words, although still rotating at synchronous speed, the rotor slips back in space result of increased loading. In this process the torque angle δ becomes larger and therefore the induced torque ($T_{ind} = \frac{VE_b sin\delta}{\omega X_s}$)increases. The increased torque increases the rotor speed and the motor again picks up the synchronous speed but with a larger torque angle δ. Since the excitation voltage(back emf)E_b, is proportional to Φω, it only depends upon the field current and the speed of the motor. Since the motor is moving with a constant synchronous speed, and since the field the field current remains constant. Therefore, the magnitude of excitation voltage E remains constant with the change in load on the shaft.

We have $$P = \frac{VE_b sin\delta}{X_s} = VI_a cos\emptyset$$

$$E_b sin\delta = \frac{X_s}{V}P = KP \text{where} K = \frac{X_s}{V}P = a\ constant$$

These relations show that the increase in P increases $E_b sin\delta$ and $I_a cos\emptyset$. The locus of E, is shown in Fig. below. It is seen from Fig. that with the increase of the load, the quantity jI_aX_s, goes on increasing so that the relation V=$E_b + jI_aX_s$, is satisfied and therefore the armature current I_a, also increases. It is also seen from Fig. that the power factor angle Ø also changes. It becomes less and less leading and then becomes more and more lagging.



$P = \frac{V E_b \sin\delta}{X_s}$, $E_b \sin\delta = \frac{X_s}{V} P = KP$

Thus, when the load on a synchronous motor is increased,

(i) The motor continues to run at synchronous speed
(ii) The torque angle δ increases.
(iii) The excitation voltage remains constant.
(iv) The armature current I_a drawn from the supply increases.
(v) The phase angle Φ increases in the lagging direction.

There is a limit to the mechanical load that can be applied to asynchronous motor. As the load is increased, the torque angle δ also increases till a stage is reached when the rotor is pulled out of synchronism and the motor is stopped.

Effect of varying excitation with constant load:

In a d.c. motor, the armature current I_a is determined by dividing the difference between V and E_b by the armature resistance Ra. Similarly, in a synchronous motor, the stator current(I_a)isdetermined by dividing voltage-phasor resultant (E_r) between V and E_b by the synchronous impedance Z_s.

One of the most important features of a synchronous motor is that by changing the field excitation, it can be made to operate from lagging to leading power factor.

Suppose a synchronous motor is operating with normal excitation (E_b = V) at unity p.f. with a given load shown in fig(a). If R_a is negligible as compared to X_s, then I_a lags E_r by 90°and is in phase with V because p.f. is unity. The armature is drawing a power of VI_a per phase which is enough to meet the mechanical load on the motor .Now let us discuss the effect of decreasing or increasing the field excitation when the load applied to the motor remains constant.

a) Excitation Decreased

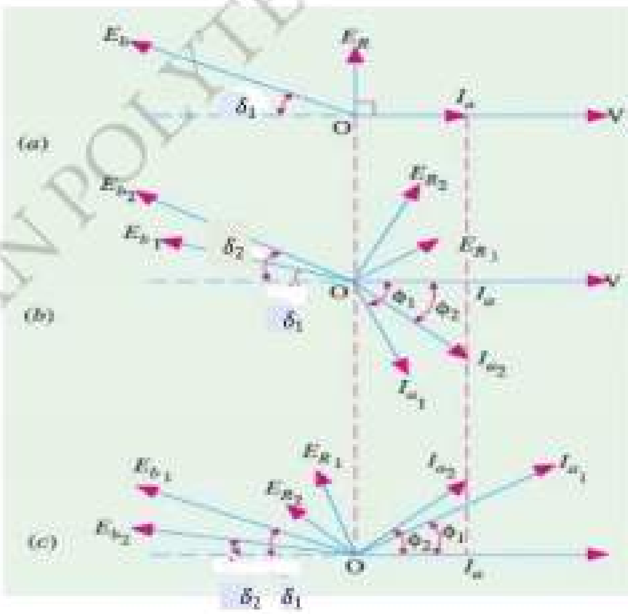
Suppose due to decrease in excitation, back e.m.f. is reduced to E_{b1} at the same load angle δ_1 as shown in fig(b). The resultant voltage E_{r1} causes a lagging armature current I_{a1} to flow. Even though I_{a1} is larger than I_a in magnitude it is incapable of producing necessary power$VI_a$for carrying the constant load because $I_{a1}cos\emptyset_1$component is less than I_a so that$VI_{a1}cos\emptyset_1 <$ VI_a.

Hence, it becomes necessary for load angle to increase from $\delta_1 to\ \delta_2$. It increases back e.m.f. from E_{b1} toE_{b2} which in turn, increases resultant voltage from $E_{r1} to\ E_{r2}$.Consequently, armature current increases to I_{a2} whose in-phase component produces enough power ($VI_{a2}cos\emptyset_2$) to meet the constant load on the motor.

b) Excitation Increased

The effect of increasing field excitation is shown in Fig.(c) where increased E_{b1} is shown at the original load angle δ_1. The resultant voltage E_{r1} causes a leading current I_{a1} whose in-phase component is larger than I_a. Hence, armature develops more power than the load on the motor. Accordingly, load angle decreases from $\delta_1 to\ \delta_2$, which decreases resultant voltage from $E_{r1} to\ E_{r2}$. Consequently, armature current decreases from $I_{a1}$to I_{a2} whose in-phase component $VI_{a2}cos\emptyset_2 = I_a$. The armature develops power sufficient to carry the constant load on the motor.

Hence, we find that variations in the excitation of a synchronous motor running with a given load produce variation in its load angle only.



Power angle characteristics of cylindrical rotor motor:

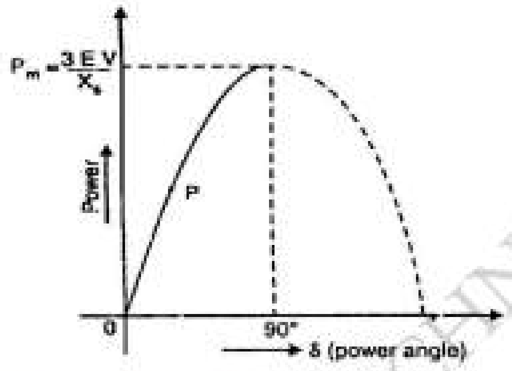
The power output of an alternator is given by:

Power output/phase, $P = \frac{VE_b}{X_s} sin\delta$

Total power output = $\frac{3VE_b}{X_s}$

The power output varies sinusoidally with power angle δ. The synchronous motor delivers maximum power when $\delta = 90°$. If δ becomes greater than 90°, the machine will lose synchronism. The dotted portion of the curve refers to unstable operation, i.e., machine loses synchronism.

Stability of the synchronous motor is determined by the power/power angle characteristic. Suppose the operating position of the alternator is represented by point P on the curve. If unsteadiness occurs due to a transient spike of mechanical input, then load angle δincreases bya small amount. The additional electrical output caused by an increase in δproduces a torque which is not balanced by the driving torque once the spike has passed. This torque causes retardation of the rotor and the synchronous motor returns to the operating point P. The torque causing the return of the synchronous motor to the steady-state position is called the synchronizing torque and the power associated with it is known as synchronizing power.



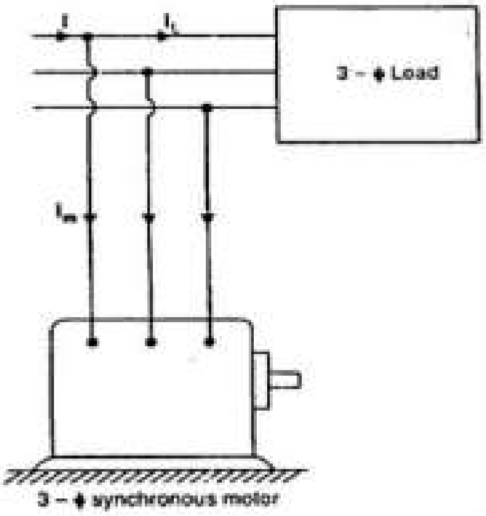
Synchronous Condenser:

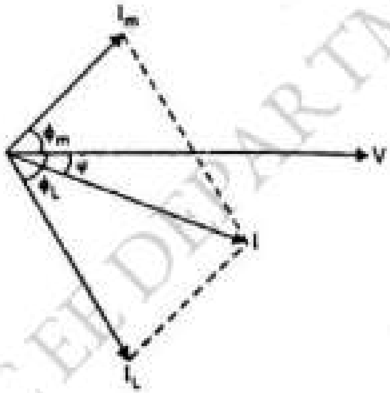
A synchronous motor takes a leading current when over-excited and, therefore, behaves as a capacitor.

An over-excited synchronous motor running on no-load in known as synchronous condenser. It is also known as synchronous capacitor or synchronous compensator or synchronous phase modifier.

When such a machine is connected in parallel with induction motors or other devices that operate at low lagging power factor, the leading kVAR supplied by the synchronous condenser partly neutralizes the lagging reactive kVAR of the loads. Consequently, the power factor of the system is improved.

Figure shown below shows the power factor improvement by synchronous condenser method. The 3 –phase load takes current I_L at low lagging power factor$\cos\phi_L$. The synchronous condenser takes a current $I_m$which leads the voltage by an angle ϕ_m.The resultant current I is the vector sum of $I_m$and I_L and lags behind the voltage by an angle ϕ. It is clear that ϕ is less than ϕ_L so that $\cos\phi$ is greater than $\cos\phi_L$.Thus the power factor is increased from $\cos\phi_L$to $\cos\phi$. Synchronous condensers are generally used at major bulk supply substations for power factor improvement.





Advantages

(i) By varying the field excitation, the magnitude of current drawn by the motor can be changed by any amount. This helps in achieving step less control of power factor.

(ii) The motor windings have high thermal stability to short circuit currents.

(iii) The faults can be removed easily.

Disadvantages

(i) There are considerable losses in the motor.

(ii) The maintenance cost is high.

(iii) It produces noise.

(iv) Except in sizes above 500 KVA, the cost is greater than that of static capacitors of the same rating.

(v) As a synchronous motor has no self-starting torque, then-fore, an auxiliary equipment has to be provided for this purpose.

Hunting in Synchronous Motor:

Sudden changes of load on synchronous motors may sometimes set up oscillations that are superimposed upon the normal rotation, resulting in periodic variations of a very low frequency in speed. This effect is known as hunting or phase-swinging or surging. If the time period of these oscillations happens to be equal to the natural time period of the machine,then mechanical resonance is set up. The amplitude of these oscillations is built up to a large value and may become so great as to throw the machine out of synchronism.

Causes of hunting:

1. Sudden changes of load
2. Faults occurring in the system which the generator supplies
3. Sudden changes in the field current
4. Cyclic variations of the load torque.

Effects of hunting

1. It can lead to loss of synchronism.
2. It can cause variations of the supply voltage producing undesirable lamp flicker.
3. It increases the possibility of resonance. If the frequency of the torque component becomes equal to that of the transient oscillations of the synchronous machine, resonance may take place.
4. Large mechanical stresses may develop in the rotor shaft.
5. The machine losses increase and the temperature of the machine rises.

Of these effects, the first is the most important phenomenon to be avoided.

Reduction of hunting

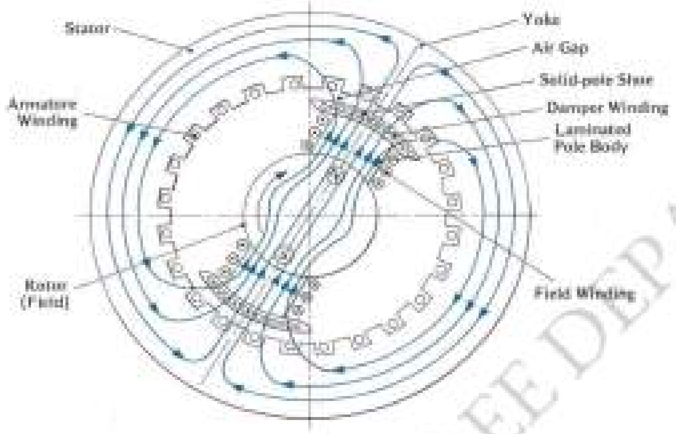
The following are some of the techniques used to reduce hunting:

1. Damper windings
2. Use of flywheels
   The prime mover is provided with a large and heavy flywheel. This increases the inertia of the prime mover and helps in maintaining the rotor speed constant.
3. By designing synchronous machines with suitable synchronizing power coefficients.

Damper winding:

The damper windings consist of short-circuited Cu bars embedded in the faces of the field poles of the motor. The ends of the damper bars are short circuited at the ends by short circuiting rings similar to end rings as in the case of squirrel cage rotors. Under normal running conditions, the damper winding does not carry any current because rotor runs at synchronous speed. Whenever any irregularity takes place in the speed of rotation, however, the polar flux moves from side to side of the pole, this movement causing the flux to move backwards and forwards across the damper bars. Emfs are induced in the damper bars.

These damper windings are serving the function of providing mechanical balance, reduce the effect of over voltages and damp out hunting in case of alternators. In case of synchronous motors, they act as rotor bars and help in self-starting of the motor.



Methods of starting synchronous motor:

A synchronous motor is not self-starting. There are twomethods that are used to start a synchronous motor:

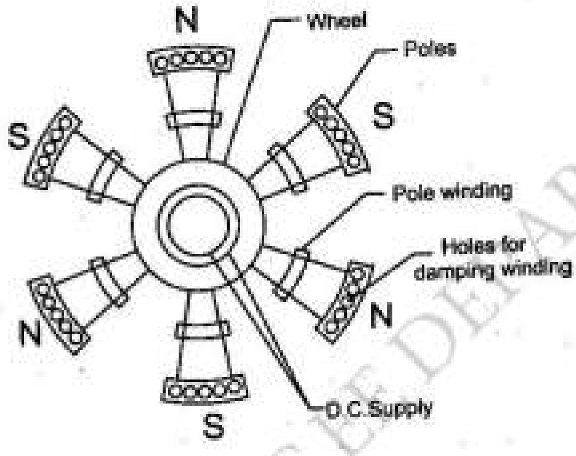
1. Starting with the help of an external prime mover.
2. Starting with the help of damper windings.

Motor Starting with an External Motor:

In this method an external motor drives the synchronous motor and bring it to synchronous speed. The synchronous machine is then synchronized with the bus-bar as a synchronous generator. The prime mover is then disconnected. The synchronous machine will work as a motor. Now the load can be connected to the synchronous motor. Since load is not connected to the synchronous motor before synchronizing, the starting motor has to overcome the inertia of the synchronous motor at no load. Therefore, the rating of the starting motor is much smaller than the rating of the synchronous motor.
Generally, most of the large synchronous motors are provided with brushless excitation systems mounted on their shafts. These exciters are used as the starting motors.

Motor Starting by using damper Winding:

The most widely used method of starting a. synchronous motor is to use damper windings. Most of the large synchronous motors are provided with damper windings, in order to nullify the oscillations of the rotor whenever the synchronous machine is subjected to a periodically varying load. A damper winding consists of heavy copper bars inserted in slots of the pole faces of the rotor. These bars are short circuited by end rings at both ends of the rotor similar to the squirrel cage rotor bars.



When the stator of a synchronous motor is connected to the 3-Phase AC supply, the motor starts as a 3-Phase induction machine due to the presence of the damper bars, just like a squirrel cage induction motor. Once the motor picks up to a speed near about its synchronous speed, the DC supply to its field winding is connected and the synchronous motor pulls into step i.e. it continues to operate as a Synchronous motor running at its synchronous speed.

Applications of Synchronous Motors:

Synchronous motors find extensive application for the following classes of service:

1. Power factor correction
2. Constant-speed, constant-load drives
3. Voltage regulation

Power factor correction

Overexcited synchronous motors having leading power factor are widely used for improving power factor of those power systems which employ a large number of induction motors and other devices having lagging p.f. such as welders and fluorescent lights etc.

Constant-speed applications

Because of their high efficiency and high-speed, synchronous motors (above 600 r.p.m.) are well-suited for loads where constant speed is required such as centrifugal pumps, belt-driven reciprocating compressors, blowers, line shafts, rubber and paper mills etc.

Low-speed synchronous motors (below 600 r.p.m.) are used for drives such as centrifugal and screw-type pumps, ball and tube mills, vacuum pumps, cliippers and metal rolling mills etc.

Voltage regulation

The voltage at the end of a long transmission line varies greatly especially when large inductive loads are present. When an inductive load is disconnected suddenly, voltage tends to rise considerably above its normal value because of the line capacitance. By installing a synchronous motor with a field regulator (for varying its excitation), this voltage rise can be controlled.

When line voltage decreases due to inductive load, motor excitation is increased, thereby raising its p.f. which compensates for the line drop. If line voltage rises due to line capacitive effect, motor excitation is decreased, thereby making its p.f. lagging which helps to maintain the line voltage at its normal value.

Imp 2marks Chapter-2 EC-II

1. what is hunting?
2. What is the function of damper bar?
3. write two application of synchronous motor.
4. what is Damper winding?
5. what are V-curves of synchronous motor?

5 marks

1. Explain how a synchronous motor acts as a synchronous condensor with the help of vector diagram.
2. Explain hunting of synchronous motor.
3. What is the effect of changing excitation on constant load of a synchronous motor!
4. Explain the effect of changing load at a constant excitation of 3-φ synchronous motor.

10 marks

(1) A 3-φ, 400V, synchronous motor takes 52.5 Amp at a power factor of 0.8 leading. calculate the power supplied, the induced emf and the load angle. The motor impedance per phase is $(0.25+j3.2)\Omega$.

2. Explain the principle of operation of a synchronous motor.

3. A, 3φ, 6600 volts, 50Hz star-connected synchronous motor takes 50A current. The resistance and synchronous reactance per phase are 1Ω and 20Ω respectively. Find the power supplied to the motor and induced emf for a power factor of (a) 0.9 lagging (b) 0.9 leading.

4. A 1000KVA, 11kV, 3-φ, Y connected synchronous motor has an armature resistance and reactance per phase of 3.5 Ω & 40Ω respectively. determine the induced emf and load angle or Torque angle of the rotor when fully loaded (a) unit pf (b) 0.8 pf lagging.

5. Details the effect of excitation on armature current & power factor in synchronous motor.

Chapter-3
THREE PHASE INDUCTION MOTOR

An Induction machines is basically ***Asynchronous machines***. If the Induction Machine converts Mechanical energy to Electrical energy, then it is called Induction Generator. If the Induction Machine converts Electrical energy to Mechanical energy, then it is called Induction Motor.

The induction motor may be considered to be a transformer with a rotating secondary and it can, therefore, be described as a "transformer type" a.c. machine in which electrical energy is converted into mechanical energy.

Production of rotating magnetic field:

When a 3-phase winding is energized from a 3-phase supply, a rotating magnetic field is produced. This field is such that its poles do no remain in a fixed position on the stator but go on shifting their positions around the stator. For this reason, it is called a rotating Field.

Consider a 2-pole,3-phase winding placed 120° space apart. The three phases X, Y and Z are energized from a 3-phase source and currents in these phases are indicated as $I_x,\ I_y\ and\ I_z$.The fluxes due to these these currents are $\emptyset_x$, $\emptyset_y$ and $\emptyset_z$.

$$\emptyset_x = \emptyset_m sin\omega t$$
$$\emptyset_y = \emptyset_m\, sin(\omega t - 120°)$$
$$\emptyset_z = \emptyset_m\, sin(\omega t - 240°)$$

Here $\emptyset_m$ is the maximum flux due to any phase. The phasor diagram of the three fluxes is shown in Fig:(i) below.

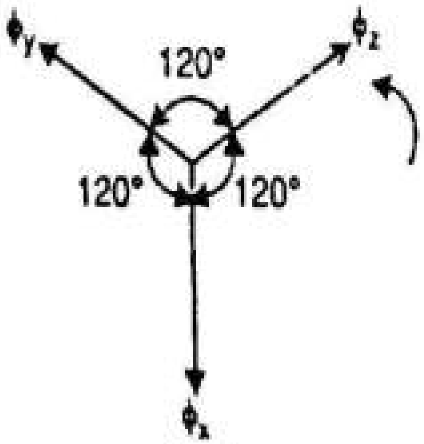


Fig: (i)

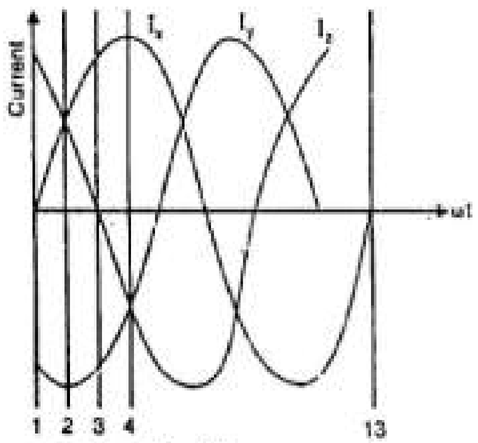


Fig: (ii)

i. At instant 1, From Fig: (ii), the current in phase X is zero and currents in phases Y and Z are equal and opposite. The currents are flowing outward in the top conductors and inward in the bottom conductors. This establishes a resultant flux towards right. The magnitude of the resultant flux is constant and is equal to 1.5 $\emptyset_m$.

At instant 1, $\omega t = 0°$.

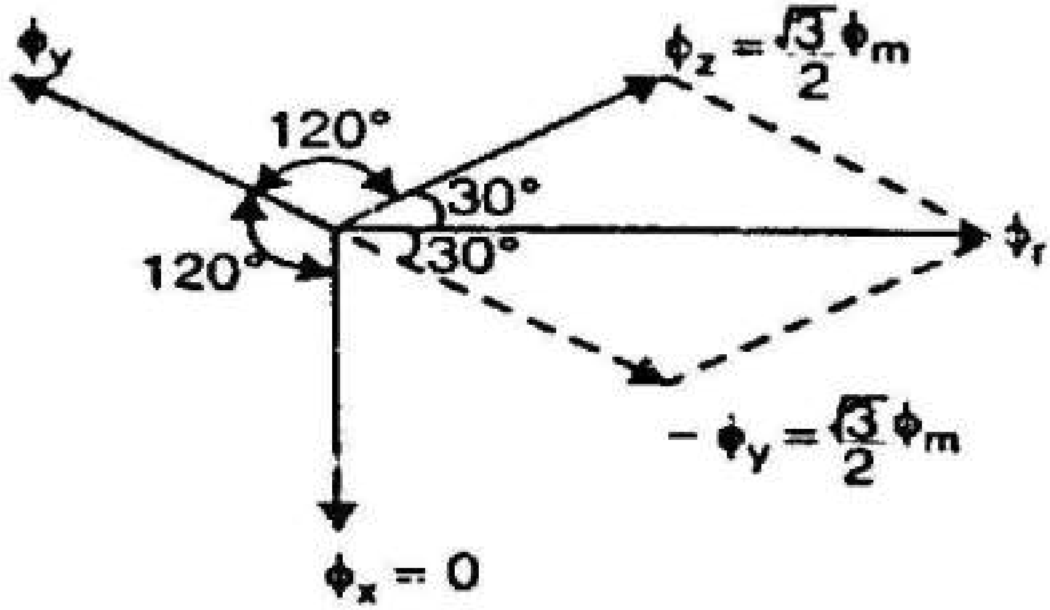
I_x=0 i.e. $\emptyset_x$=$\emptyset_m sin(\omega t) = 0$

$$\emptyset_y = \emptyset_m sin(\omega t - 120°) = \emptyset_m sin(-120°) = \frac{-\sqrt{3}}{2}\emptyset_m$$

$$\emptyset_z = \emptyset_m sin(\omega t - 240°) = \emptyset_m sin(-240°) = \frac{\sqrt{3}}{2}\emptyset_m$$

The phasor sum of $-\emptyset_y$ and $\emptyset_z$ is the resultant flux $\emptyset_r$.

Resultant flux, $\emptyset_r = 2 \times \frac{\sqrt{3}}{2}\emptyset_m cos\left(\frac{60°}{2}\right) = 1.5\ \emptyset_m$



ii. At instant 2, the current is maximum (negative) in $\emptyset_y$ phase Y and 0.5 maximum (positive) in phases X and Y.

At instant 2, $\omega t = 30°$.

$$\emptyset_x = \emptyset_m sin(\omega t) = \emptyset_m sin(30°) = \frac{\emptyset_m}{2}$$

$$\emptyset_y = \emptyset_m sin(\omega t - 120°) = \emptyset_m sin(-90°) = -\emptyset_m$$

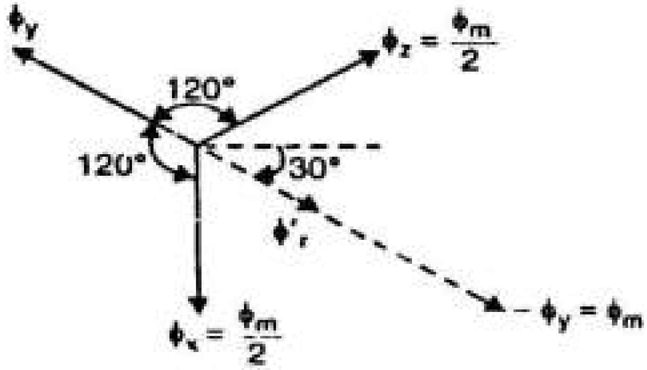
$$\emptyset_z = \emptyset_m sin(\omega t - 240°) = \emptyset_m sin(-210°) = \frac{\emptyset_m}{2}$$

The phasor sum of $\emptyset_x$, $\emptyset_y$ and $\emptyset_z$ is the resultant flux $\emptyset_r$

The phasor sum of ϕ_x and ϕ_z. $\emptyset'_r = 2 \times \frac{\emptyset_m}{2} cos\left(\frac{120°}{2}\right) = \frac{\emptyset_m}{2}$

The phasor sum of $\emptyset'_r$ and $-\emptyset_y$, $\emptyset_r = \frac{\emptyset_m}{2} + \emptyset_m = 1.5\ \emptyset_m$

The resultant flux is displaced 30° clockwise from position 1.



iii. At instant 3, current in phase Z is zero and the currents in phases X and Y are equal and opposite (currents in phases X and Y are 0.866 × max. value).

At instant 3, $\omega t = 60°$.

$$\emptyset_x = \emptyset_m sin(\omega t) = \emptyset_m sin(60°) = \frac{\sqrt{3}}{2}\emptyset_m$$

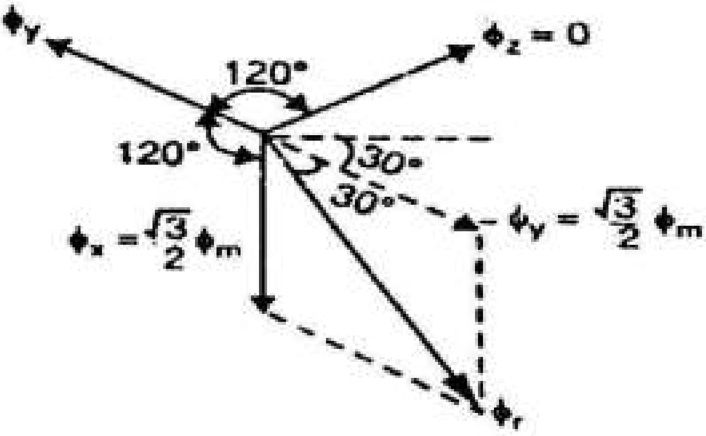
$$\emptyset_y = \emptyset_m sin(\omega t - 120°) = \emptyset_m sin(-60°) = -\frac{\sqrt{3}}{2}\emptyset_m$$

$$\emptyset_z = \emptyset_m sin(\omega t - 240°) = \emptyset_m sin(-180°) = 0$$

The resultant flux $\emptyset_r$ is the phasor sum of $-\emptyset_y$ and $\emptyset_x$

Resultant flux, $\emptyset_r = 2 \times \frac{\sqrt{3}}{2}\emptyset_m cos\left(\frac{60°}{2}\right) = 1.5\ \emptyset_m$

The resultant flux is displaced 60° clockwise from position 1.



iv. At instant 4, the current in phase X is maximum (positive) and the currents in phases Y and Z are equal and negative (currents in phases Y and Z are 0.5 ×max. value). This establishes a resultant flux downward.

At instant 4, $\omega t = 90°$.

$$\emptyset_x = \emptyset_m sin(\omega t) = \emptyset_m sin(90°) = \emptyset_m$$

$$\emptyset_y = \emptyset_m sin(\omega t - 120°) = \emptyset_m sin(-30°) = -\frac{\emptyset_m}{2}$$

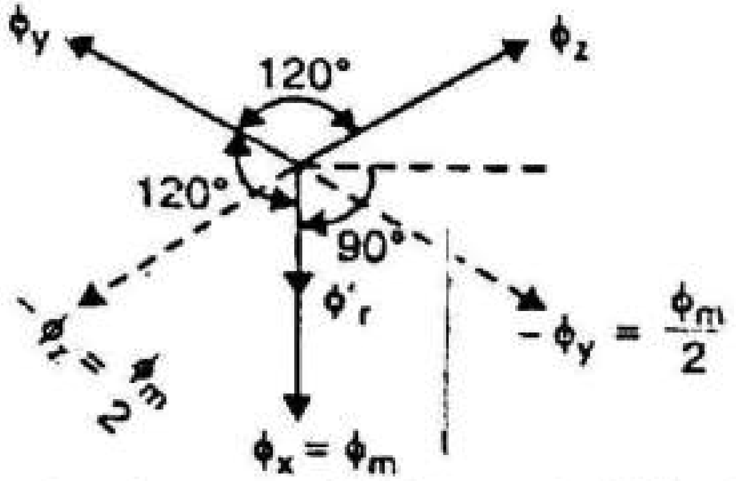
$$\emptyset_z = \emptyset_m sin(\omega t - 240°) = \emptyset_m sin(-150°) = -\frac{\emptyset_m}{2}$$

The phasor sum of $\emptyset_x$, $\emptyset_y$ and $\emptyset_z$ is the resultant flux $\emptyset_r$

The phasor sum of $-\emptyset_y$and$-\emptyset_z$, $\emptyset'_r = 2 \times \frac{\emptyset_m}{2} cos\left(\frac{120°}{2}\right) = \frac{\emptyset_m}{2}$

The phasor sum of $\emptyset'_r$ and$\emptyset_x$, $\emptyset_r = \frac{\emptyset_m}{2} + \emptyset_m = 1.5\ \emptyset_m$

The resultant flux is displaced 90° clockwise from position 1 which is in the downward direction.



Thus a 3-phase supply produces a rotating field of constant value ($=1.5\ \emptyset_m$, where $\emptyset_m$is the maximum flux due to any phase).

Speed of rotating magnetic field:

The speed at which the rotating magnetic field revolves is called the synchronous speed (Ns).

$$N_s = \frac{120f}{P}$$

Where f = frequency in HZ

P= number of poles

Direction of rotating magnetic field:

The phase sequence of the three-phase voltage applied to the stator winding is X-Y-Z. If this sequence is changed to X-Z-Y, it is observed that direction of rotation of the field is reversed i.e., the field rotates counterclockwise rather than clockwise.

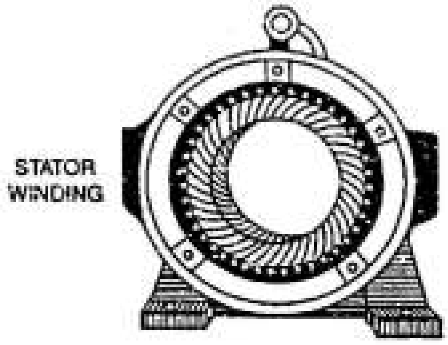
However, the number of poles and the speed at which the magnetic field rotates remain unchanged. Thus it is necessary only to change the phase sequence in order to change the direction of rotation of the magnetic field. For a three-phase supply, this can be done by interchanging any two of the three lines. The rotor in a 3-phase induction motor runs in the same direction as the rotating magnetic field. Therefore, the direction of rotation of a 3-phase induction motor can be reversed by interchanging any two of the three motor supply lines.

Construction:

A 3-phase induction motor has two main parts (i) stator and (ii) rotor. The rotor is separated from the stator by a small air-gap which ranges from 0.4 mm to 4 mm, depending on the power of the motor.

Stator:

- Stator consists of a steel frame which encloses a hollow, cylindrical core made up of thin laminations of silicon steel to reduce eddy current losses. A number of evenly spaced slots is provided on the inner periphery of the laminations.
- Stator carries 3-phase winding and is fed from a 3-phase supply. The 3-phase stator winding is wound for a definite number of poles as per requirement of speed. Greater the number of poles, lesser is the speed of the motor and vice-versa.
- When 3-phase supply is given to the stator winding, a rotating magnetic field of constant magnitude is produced. This rotating field induces currents in the rotor by electromagnetic induction.



Rotor

The rotor, mounted on a shaft, is a hollow laminated core having slots on its outer periphery. The winding placed in these slots (called rotor winding) may be one of the following two types:

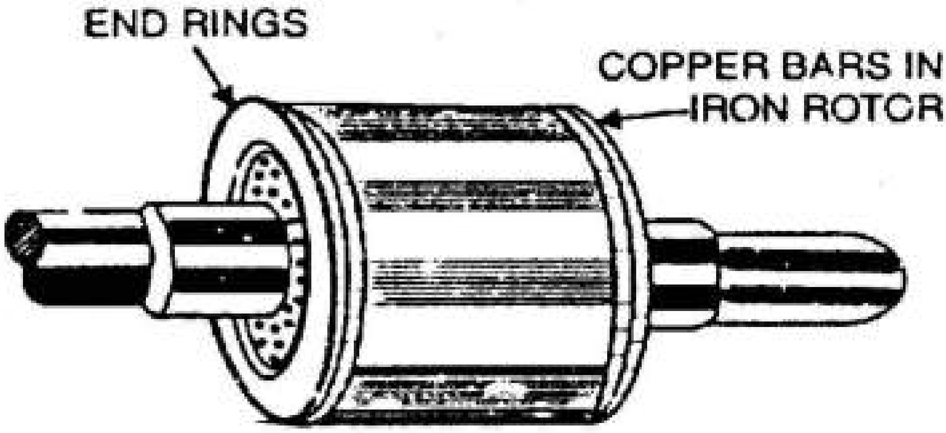
(i) Squirrel cage type (ii) Wound type

Squirrel-cage rotor:

- It consists of a laminated cylindrical core having parallel slots on its outer periphery. One copper or aluminum bar is placed in each slot. All these bars are joined at each end by metal rings called end rings .This forms a permanently short-circuited winding which is indestructible.
- The rotor is not connected electrically to the supply but has current induced in it by transformer action from the stator.
- Those induction motors which employ squirrel cage rotor are called squirrel cage induction motors.
- Most of 3-phase induction motors use squirrel cage rotor as it has a remarkably simple and robust construction enabling it to operate in the most adverse circumstances.
- It suffers from the disadvantage of a low starting torque. It is because the rotor bars are permanently short-circuited and it is not possible to add any external resistance to the rotor circuit to have a large starting torque.

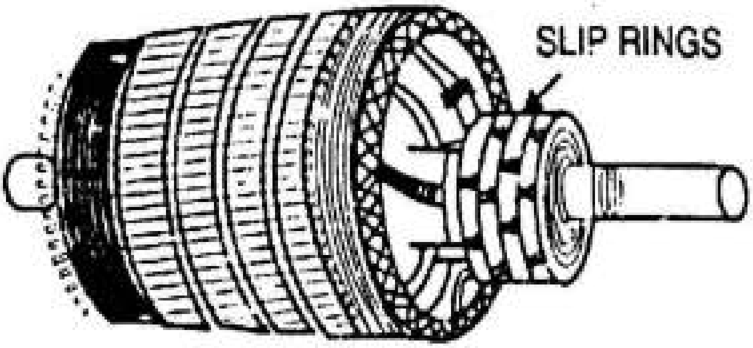
The rotor slots are usually not quite parallel to the shaft but are purposely given a slight skew. This is useful in two ways:

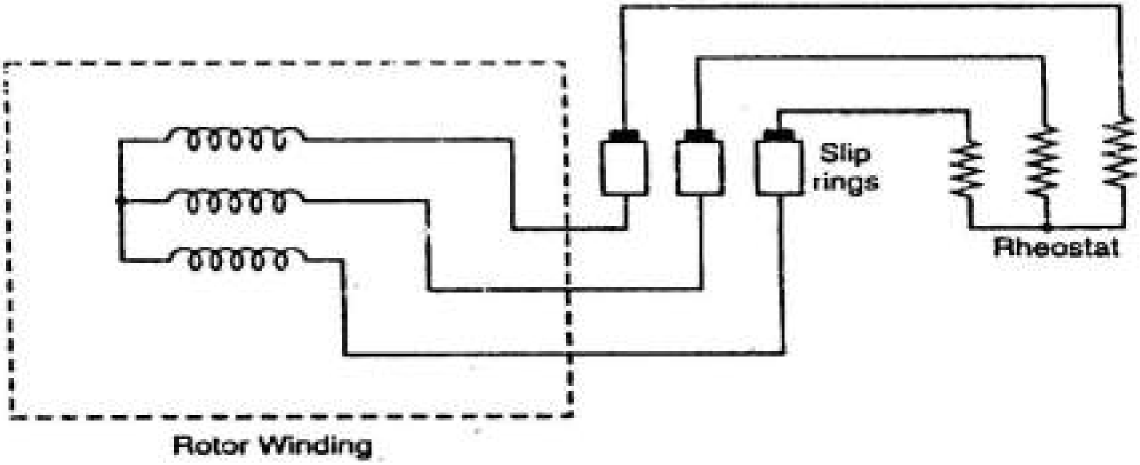
i. It helps to make the motor run quietly by reducing the magnetic hum and
ii. It helps in reducing the locking tendency of the rotor i.e. the tendency of the rotor teeth to remain under the stator teeth due to direct magnetic attraction between the two.



Wound rotor.

- It consists of a laminated cylindrical core and carries a 3- phase winding, similar to the one on the stator.
- The rotor winding is uniformly distributed in the slots and is usually star-connected. The open ends of the rotor winding are brought out and joined to three insulated slip rings mounted on the rotor shaft with one brush resting on each slip ring.
- The three brushes are connected to a 3-phase star-connected rheostat. This makes possible the introduction of additional resistance in the rotor circuit during the starting period for increasing the starting torque of the motor.
- At starting, the external resistances are included in the rotor circuit to give a large starting torque. These resistances are gradually reduced to zero as the motor runs up to speed.
- The external resistances are used during starting period only. When the motor attains normal speed, the three brushes are short-circuited so that the wound rotor runs like a squirrel cage rotor.





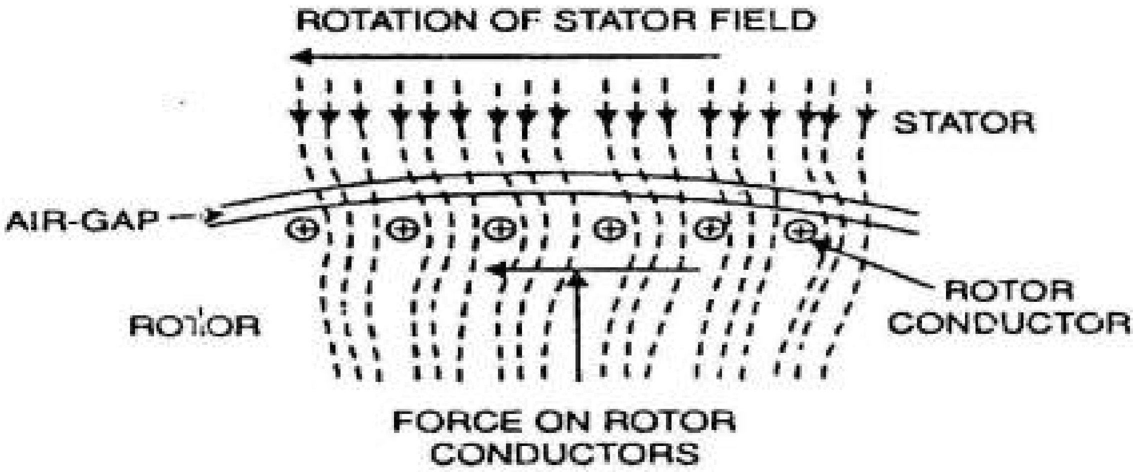
Principle of Operation:

(i) When 3-phase stator winding is energized from a 3-phase supply, a rotating magnetic field is set up which rotates round the stator at synchronous speed Ns (= 120 f/P).

(ii) The rotating field passes through the air gap and cuts the rotor conductors, which are stationary. Due to the relative speed between the rotating flux and the stationary rotor, e.m.f.s are induced in the rotor conductors. Since the rotor circuit is short-circuited, currents start flowing in the rotor conductors.

(iii) The current-carrying rotor conductors are placed in the magnetic field produced by the stator. Consequently, mechanical force acts on the rotor conductors. The sum of the mechanical forces on all the rotor conductors produces a torque which tends to move the rotor in the same direction as the rotating field.

(iv) According to Lenz's law law, the direction of rotor currents will be such that they tend to oppose the cause producing them. The cause producing the rotor currents is the relative speed between the rotating field and the stationary rotor conductors. Hence to reduce this relative speed, the rotor starts running in the same direction as that of stator field and tries to catch it.



Speed and Slip:

The rotor rapidly accelerates in the direction of rotating field. However the rotor can never reach the speed of stator flux. If rotor is rotating at synchronous speed ,then there would be no relative speed between the stator field and rotor conductors,no cutting of flux by the rotor conductors and there would be no generated voltages,no induced rotor currents and, therefore, no torque to drive the rotor. The friction and windage would immediately cause the rotor to slow down. Hence, the rotor speed (N_r) is always less than the suitor field speed (N_s). This difference in speed depends upon load on the motor.

The difference between the synchronous speed N_s of the rotating stator field and the actual rotor speed (N_r) is called slip.

It is usually expressed as a percentage of synchronous speed i.e.,

$$\% \, slip \; s = \frac{N_s - N_r}{N_s} \times 100$$

$$N_r = N_s(1 - s)$$

i. The quantity $N_s - N_r$ is sometimes called slip speed.
ii. When the rotor is stationary (i.e., N_r = 0), slip, s = 1 or 100 %.
iii. In an induction motor, the change in slip from no-load to full-load is hardly 0.1% to 3% so that it is essentially a constant-speed motor.

Frequency of Rotor Current and Voltage:

The frequency of a voltage or current induced due to the relative speed between a vending and a magnetic field is given by

$$\boldsymbol{Frequency \; f = \frac{PN}{120}}$$

where N = Relative speed between magnetic field and the winding
P = Number of poles

For a rotor speed N_r, the relative speed between the rotating flux and the rotor is $N_s - N_r$. Consequently, the rotor current frequency

$$f_r = \frac{(N_s - N_r)P}{120}$$

$$= \frac{sN_sP}{120}$$

$$f_r = sf$$

Rotor current frequency = slip x Supply frequency

i. When the rotor is at standstill or stationary (i.e., s = 1), the frequency of rotor current is the same as that of supply frequency (($f_r = sf = 1 \times f = f$)
ii. As the rotor picks up speed, the relative speed between the rotating flux and the rotor decreases. Consequently, the slip s and hence rotor current frequency decreases.

Rotor EMF and Reactance:

Let E_2 = standstill rotor induced e.m.f./phase

X_2 = standstill rotor reactance/phase.

f = rotor current frequency at standstill

When rotor is stationary i.e. s= 1. the frequency of rotor e.m.f. is the same as that of the stator supply frequency. The value of e.m.f. induced in the rotor at standstill is maximum because the relative speed between the rotor and the revolving stator flux is maximum. In fact, the motor is equivalent to a 3-phase transformer with a short-circuited rotating secondary.

When rotor starts running, the relative speed between rotor and the rotating stator flux is decreased. Hence, the rotor induced e.m.f. which is directly proportional to this relative speed, is also decreased. Hence, for a slip s the rotor induced e.m.f. will be s times the induced e.m.f. at standstill.

Therefore, under running conditions $E_r = sE_2$.

The frequency of the induced e.m.f. will $f_r = sf$

Due to decrease in frequency of the rotor e.m.f.. the rotor reactance will also decrease.

$X_r = sX_2$ where E_r and X_r are rotor e.m.f. and reactance under running conditions

Thus at any slip s,

Rotor e.m.f./phase = sE_2

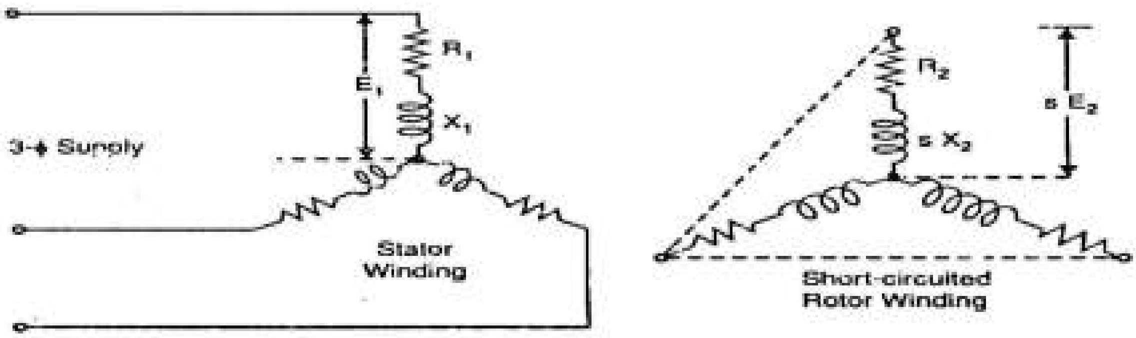
Rotor reactance/phase = sX_2

Rotor frequency = sf

where E_2, X_2 and f are the corresponding values at standstill.

Rotor Current:

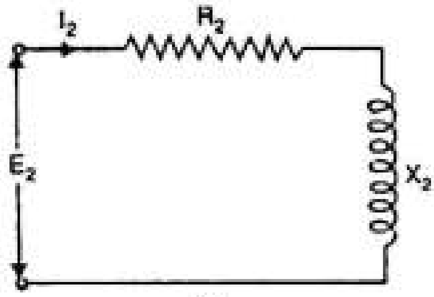
Consider a 3-phase induction motor at any slip s. The rotor is assumed to be of wound type and star connected. Rotor e.m.f./phase and rotor reactance/phase are sE_2 and sX_2 respectively. The rotor resistance/phase is R_2 and is independent of frequency and, therefore, does not depend upon slip. Similarly stator winding values R1 and X1 do not depend upon slip.



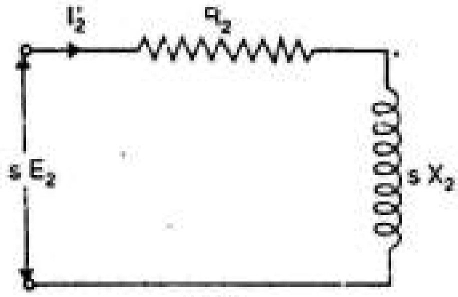
At standstill: One phase of the rotor circuit at standstill is shown in Fig: (i)

$$\text{Rotor current/phase, } I_2 = \frac{E_2}{Z_2} = \frac{E_2}{\sqrt{R_2^2 + X_2^2}}$$

$$\text{Rotor p.f., } \cos\phi_2 = \frac{R_2}{Z_2} = \frac{R_2}{\sqrt{R_2^2 + X_2^2}}$$



(i)



(ii)

When running at slip s: Fig: (ii)) shows one phase of the rotor circuit when the motor is running at slip s.

$$\text{Rotor current, } I'_2 = \frac{sE_2}{Z'_2} = \frac{sE_2}{\sqrt{R_2^2 + (sX_2)^2}}$$

$$\text{Rotor p.f., } \cos\phi'_2 = \frac{R_2}{Z'_2} = \frac{R_2}{\sqrt{R_2^2 + (sX_2)^2}}$$

Rotor Torque:

The torque T developed by the rotor is directly proportional to:

i. rotor current
ii. Rotor e.m.f.
iii. power factor of the rotor circuit

$\therefore \quad T \propto E_2 I_2 \cos\phi_2$

or $\quad T = K E_2 I_2 \cos\phi_2$

where $\quad I_2$ = rotor current at standstill
E_2 = rotor e.m.f. at standstill
$\cos\phi_2$ = rotor p.f. at standstill

Starting Torque (T_{st}):

The torque developed by the motor at the instant of starting is called starting torque.

Let E_2 = rotor e.m.f. per phase at standstill;

R_2 = rotor resistance phase

X_2 = rotor reactance phase at standstill

$$\therefore \quad Z_2 = \sqrt{(R_2^2 + X_2^2)} = \text{rotor impedance/phase at } \textit{standstill}$$

$$\text{Then,} \quad I_2 = \frac{E_2}{Z_2} = \frac{E_2}{\sqrt{(R_2^2 + X_2^2)}}; \quad \cos\phi_2 = \frac{R_2}{Z_2} = \frac{R_2}{\sqrt{(R_2^2 + X_2^2)}}$$

Standstill or starting torque $T_{st} = k_1 E_2 I_2 \cos\phi_2$

$$\text{or} \quad T_{st} = k_1 E_2 \cdot \frac{E_2}{\sqrt{(R_2^2 + X_2^2)}} \times \frac{R_2}{\sqrt{(R_2^2 + X_2^2)}} = \frac{k_1 E_2^2 R_2}{R_2^2 + X_2^2}$$

If supply voltage V is constant, then the flux Φ and hence, E_2 both are constant.

$$\therefore \quad T_{st} = k_2 \frac{R_2}{R_2^2 + X_2^2} = k_2 \frac{R_2}{Z_2^2} \text{ where } k_2 \text{ is some other constant.}$$

$$\text{Now,} \quad k_1 = \frac{3}{2\pi N_s}, \quad \therefore \quad \boxed{T_{st} = \frac{3}{2\pi N_s} \cdot \frac{E_2^2 R_2}{R_2^2 + X_2^2}}$$

Where Ns $\rightarrow$ synchronous speed in rps.

The magnitude of starting torque would depend upon the relative values of R2 and X2 i.e., rotor resistance/phase and standstill rotor reactance/phase.

Starting Torque of a Squirrel-cage Motor:

- The resistance of a squirrel-cage motor is fixed and small as compared to its reactance which is very large especially at the start because at standstill, the frequency of the rotor currents equals the supply frequency. Hence, the starting current I_2 of the rotor, though very large in magnitude, lags by a very large angle behind E_2 with the result that the starting torque per ampere is very poor.
- It is 1.5 times the full-load torque, although the starting current is 5 to 7 times the full-load current. Hence, such motors are not useful where the motor has to start against heavy loads.

Starting Torque of a Slip-ring Motor:

- The starting torque of slip ring motor is increased by improving its power factor by adding external resistance in the rotor circuit from the star-connected rheostat, the rheostat resistance being progressively cut out as the motor gathers speed.
- Addition of external resistance, however, increases the rotor impedance and so reduces the rotor current. At first, the effect of improved power factor predominates the current-decreasing effect of impedance. Hence, starting torque is increased. But after a certain point, the effect of increased impedance predominates the effect of improved power factor and so the torque starts decreasing.

Condition for Maximum Starting Torque:

The starting torque will be maximum when rotor resistance/phase is equal to standstill rotor reactance/phase.

$$T_{st} = \frac{k_2 R_2}{R_2^2 + X_2^2}$$

Differentiating above equation w.r.t. R_2 and equating the result to zero, we get

$$\frac{dT_{st}}{dR_2} = k_2 \left[\frac{1}{R_2^2 + X_2^2} - \frac{R_2\,(2R_2)}{(R_2^2 + X_2^2)^2} \right] = 0$$

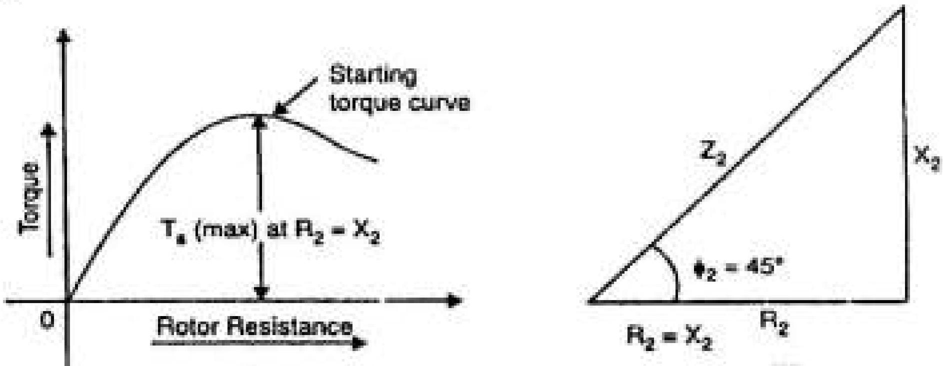
$$R_2^{\,2} + X_2^{\,2} = 2R_2^{\,2}$$

$$\therefore \quad R_2 = X_2$$

Hence starting torque will be maximum when:

Rotor resistance/phase = Standstill rotor reactance/phase

Under the condition of maximum starting torque, ϕ= 45° and rotor power factor is 0.707 lagging.



(*i*) (*ii*)

As the rotor resistance is increased from a low value, the starting torque increases until it becomes maximum when $R_2 = X_2$. If the rotor resistance is increased beyond this optimum value, the starting torque will decrease.

Effect of Change in Supply Voltage on Starting Torque:

$$T_{st} = \frac{k_1 E_2^2\, R_2}{R_2^2 + X_2^2}$$

Since $E_2 \propto$ Supply voltage V

$$T_{st} = \frac{k_3 V^2 R_2}{R_2^2 + X_2^2} = \frac{k_3 V^2 R_2}{Z_2^2}$$

where K_3 is another constant.

$$\text{Hence } T_{st} \propto V^2$$

Therefore, the starting torque is very sensitive to changes in the value of supply voltage. For example, a drop of 10% in supply voltage will decrease the starting torque by about 20%.

Torque Under Running Conditions:

Let the rotor at standstill have per phase induced e.m.f. E_2, reactance X2 and resistance R_2.

$$T \propto E_r I_r \cos\phi_2 \text{ or } T \propto \phi\, I_r \cos\phi_2$$

where E_r = rotor e.m.f./phase under ***running conditions***

I_r = rotor current/phase under ***running conditions***

Now $E_r = sE_2$

$$\therefore \quad I_r = \frac{E_r}{Z_r} = \frac{sE_2}{\sqrt{[R_2^2 + (sX_2)^2]}}$$

$$\cos\phi_2 = \frac{R_2}{\sqrt{[R_2^2 + (sX_2)^2]}}$$

$$\therefore \quad T \propto \frac{s\,\Phi\, E_2 R_2}{R_2^2 + (sX_2)^2} = \frac{k\Phi \,.\, s \,.\, E_2 R_2}{R_2^2 + (sX_2)^2}$$

$$\text{Also } T = \frac{k_1 \,.\, sE_2^2\, R_2}{R_2^2 + (sX_2)^2} \quad (\because E_2 \propto \phi)$$

Where k_1 is another constant. Its value is equal to $\frac{3}{2\pi N_S}$

$$T = \frac{3}{2\pi N_S} \cdot \frac{sE_2^2\, R_2}{R_2^2 + (sX_2)^2} = \frac{3}{2\pi N_S} \cdot \frac{sE_2^2\, R_2}{Zr^2}$$

At standstill when s=1,

$$T_{st} = \frac{k_1 E_2^2\, R_2}{R_2^2 + X_2^2} \left(\text{or} = \frac{3}{2\pi N_S} \cdot \frac{E_2^2 R_2}{R_2^2 + X_2^2} \right)$$

It may be seen that running torque is:

i. Directly proportional to slip i.e., if slip increases (i.e., motor speed decreases), the torque will increase and vice-versa.
ii. Directly proportional to square of supply voltage ($E_2 \propto V$)

Maximum Torque under Running Conditions:

The torque of a rotor under running conditions is

$$T = \frac{k\Phi s E_2 R_2}{R_2^2 + (sX_2)^2} = k_1 \frac{sE_2^2\, R_2}{R_2^2 + (sX_2)^2}$$

The condition for maximum torque may be obtained by differentiating the above expression with respect to slip s and then putting it equal to zero.

$$\frac{dT}{ds} = \frac{K_1 \left[R_2 \left(R_2^2 + s^2\, X_2^2 \right) - 2sX_2^2 (s\, R_2) \right]}{\left(R_2^2 + s^2\, X_2^2 \right)^2} = 0$$

$$\left(R_2^2 + s^2 X_2^2\right) - 2sX_2^2 = 0$$
$$R_2^2 = s^2 X_2^2$$
$$R_2 = s X_2$$

Thus for maximum torque (Tm) under running conditions:
Rotor resistance/phase = Fractional slip ×Standstill rotor reactance/phase

Slip corresponding to maximum torque is $s = R_2/X_2$

Putting $R_2 = sX_2$ and Substituting value of $s = R_2/X_2$ in the torque equation

$$T_{max} = k_1 \frac{(R_2/X_2) \cdot E_2^2 \cdot R_2}{R_2^2 + (R_2/X_2)^2 \cdot X_2^2} = k_1 \frac{E_2^2}{2X_2}$$

$$T_{max} = \frac{3}{2\pi N_s} \cdot \frac{E_2^2}{2X_2} \text{ N-m}$$

From the above, it is found that

i. The maximum torque is independent of rotor resistance.
ii. However, the speed or slip at which maximum torque occurs is determined by the rotor resistance. torque becomes maximum when rotor reactance equals its resistance. Hence, by varying rotor resistance (possible only with slip-ring motors) maximum torque can be made to occur at any desired slip (or motor speed),
iii. Maximum torque varies inversely as standstill reactance. Hence, it should be kept as small as possible.
iv. Maximum torque varies directly as the square of the applied voltage.
v. For obtaining maximum torque at starting (s =1), rotor resistance must be equal to rotor reactance.

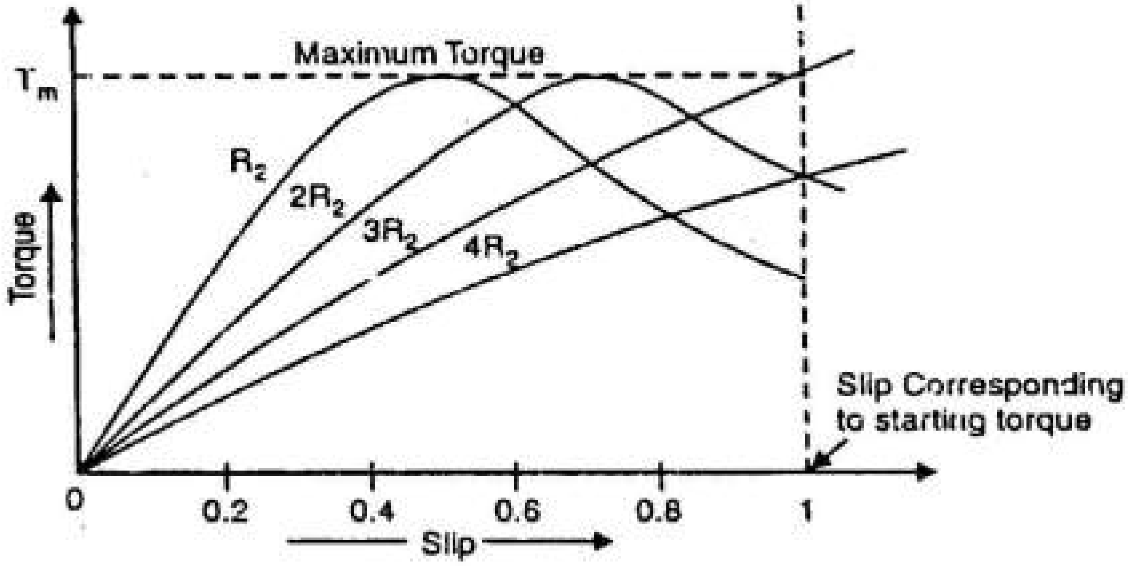
Torque-Slip Characteristics:

The graph drawn between the torque and slip for a particular value of rotor resistance R_2, is called torque-slip characteristic. A family of torque-slip characteristics for a slip-range from s = 0 to s = 1 for various values of rotor resistance is shown below.

The motor torque under running conditions is given by

$$T = \frac{k \Phi s E_2 R_2}{R_2^2 + (sX_2)^2}$$

$$T \propto \frac{sR_2}{R_2^2 + s^2 X_2^2}$$



(i) At s = 0, T = 0 so that torque-slip curve starts from the origin.

(ii) At normal speed, slip is small so that $s\,X_2$ is negligible as compared to R_2.

$$T \propto \frac{s}{R_2}$$

$\propto s$ ... as R_2 is constant

Hence torque slip curve is a straight line from zero slip to a slip that corresponds to full-load.

(iii) As slip increases beyond full-load slip, the torque increases and becomes maximum at $= \frac{R_2}{X_2}$. This maximum torque in an induction motor is called pull-out torque or break-down torque. Its value is at least twice the full-load value when the motor is operated at rated voltage and frequency.

(iv) When slip increases beyond that corresponding to maximum torque, the term $s^2{X_2}^2$ increases very rapidly so that ${R_2}^2$ may be neglected as compared to $s^2{X_2}^2$.

$$T \propto \frac{s}{s^2{X_2}^2}$$

$$\propto \frac{1}{s} \quad \text{.... as } X_2 \text{ is constant}$$

Thus the torque is now inversely proportional to slip. Hence torque-slip curve is a rectangular hyperbola.

(v) The maximum torque remains the same and is independent of the value of rotor resistance. Therefore, the addition of resistance to the rotor circuit does not change the value of maximum torque but it only changes the value of slip at which maximum torque occurs.

Full-Load and Maximum Torque:

Let s_f be the slip corresponding to full-load Torque

$$T_f \propto \frac{s_f R_2}{R_2^2 + (s_f X_2)^2}$$

$$T_{max} \propto \frac{1}{2 X_2}$$

$$\frac{T_f}{T_{max}} = \frac{2 s_f R_2 X_2}{R_2^2 + (s_f X_2)^2}$$

Dividing the numerator and denominator on R.H.S. by $\boldsymbol{X_2}^2$, we get,

$$\frac{T_f}{T_{max}} = \frac{2 s_f \cdot R_2 / X_2}{(R_2 / X_2)^2 + s_f^2} = \frac{2 a s_f}{a^2 + s_f^2}$$

$$where\ \ a = \frac{R_2}{X_2} = \frac{\text{Rotor resistance/phase}}{\text{Standstill rotor reactance/phase}}$$

Starting Torque Maximum Torque:

$$T_{st} \propto \frac{R_2}{R_2^2 + X_2^2}$$

$$T_{max} \propto \frac{1}{2 X_2}$$

Dividing the numerator and denominator on R.H.S. by $\boldsymbol{X_2}^2$, we get,

$$\frac{T_{st}}{T_{max}} = \frac{2 R_2 X_2}{R_2^2 + X_2^2} = \frac{2 R_2 / X_2}{1 + (R_2 / X_2)^2} = \frac{2a}{1 + a^2}$$

$$where\ \ a = \frac{R_2}{X_2} = \frac{\text{Rotor resistance/phase}}{\text{Standstill rotor reactance/phase}}$$

Power Stages in an Induction Motor:

The input electric power fed to the stator of the motor is converted into mechanical power at the shaft of the motor. The various losses during the energy conversion are:

1. Fixed losses
   (i) Stator iron loss
   (ii) Friction and windage loss

The rotor iron loss is negligible because the frequency of rotor currents under normal running condition is small.

2. Variable losses
   (i) Stator copper loss
   (ii) Rotor copper loss

Fig. shown below shows electric power fed to the stator of an induction motor suffers losses and finally converted into mechanical power.

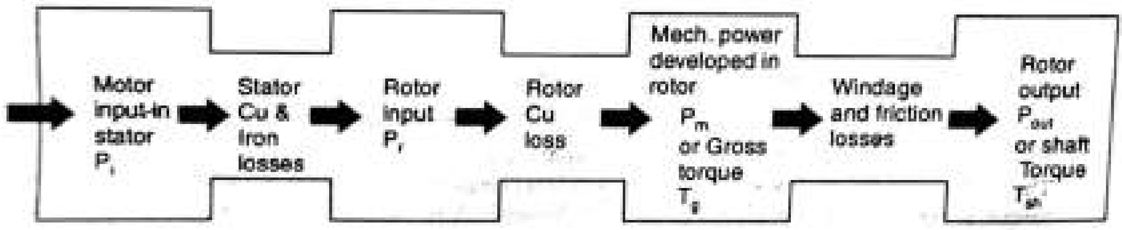
From the figure the following points may be noted:

(i) Stator input, P_i = Stator output + Stator losses
= Stator output + Stator Iron loss + Stator Cu loss

(ii) Rotor input, P_r = Stator output
It is because stator output is entirely transferred to the rotor through air-gap by electromagnetic induction.

(iii) Mechanical power available, $P_m = P_r$ − Rotor Cu loss
This mechanical power available is the gross rotor output and will produce a gross torque T_g.

(iv) Mechanical power at shaft, $P_{out} = P_m$ − Friction and windage loss
Mechanical power available at the shaft produces a shaft torque T_{sh}.
Clearly, $P_m - P_{out}$ = Friction and windage loss



Induction Motor Torque:

The mechanical power P available from any electric motor can be expressed as:

$P = \frac{2\pi NT}{60}$ watts

Where N= speed of the motor in r.p.m.

T= torque developed in N-m

If the gross output of the rotor of an induction motor is Pm and its speed is N r.p.m., then gross torque T_g developed is given by:

$$T_g = 9.55 \frac{P_m}{N} \ N - m$$

Similarly

$$T_{sh} = 9.55 \frac{P_{out}}{N} \ N - m$$

Rotor Output:

If T_g newton-metre is the gross torque developed and N r.p.m. is the speed of the rotor, then,

Gross rotor output = $P = \frac{2\pi NT_g}{60}$ watts

If there were no copper losses in the rotor, the output would equal rotor input and the rotor would run at synchronous speed N_s.

$$\therefore \quad \text{Rotor input} = \frac{2\pi N_s T_g}{60} \quad \text{watts}$$

$$\therefore \quad \text{Rotor Cu loss} = \text{Rotor input} - \text{Rotor output}$$

$$= \frac{2\pi T_g}{60}(N_s - N)$$

(i) $$\frac{\text{Rotor Cu loss}}{\text{Rotor input}} = \frac{N_s - N}{N_s} = s$$

$$\therefore \quad \text{Rotor Cu loss} = s \times \text{Rotor input}$$

(ii) $$\text{Gross rotor output, } P_m = \text{Rotor input} - \text{Rotor Cu loss}$$
$$= \text{Rotor input} - s \times \text{Rotor input}$$
$$\therefore \quad P_m = \text{Rotor input } (1 - s)$$

(iii) $$\frac{\text{Gross rotor output}}{\text{Rotor input}} = 1 - s = \frac{N}{N_s}$$

(iv) $$\frac{\text{Rotor Cu loss}}{\text{Gross rotor output}} = \frac{s}{1-s}$$

It is clear that if the input power to rotor is P_r then sP_r is lost as rotor Cu loss and the remaining (1 -s)P_r is converted into mechanical power. Consequently, induction motor operating at high slip has poor efficiency.

Note: Rotor input: Rotor Cu loss: Gross rotor output = 1: s: (1-s)

$$\frac{Gross\ rotor\ output(P_m)}{Rotor\ input(P_r)} = 1 - s = \frac{N}{N_S}$$

If the stator losses as well as friction and windage losses are neglected, then,

$$\text{Gross rotor output} = \text{Useful output}$$
$$\text{Rotor input} = \text{Stator input}$$
$$\therefore \quad \frac{\text{Useful output}}{\text{Stator output}} = 1 - s = \text{Efficiency}$$

Starting of Three Phase Induction Motor:

When the supply is connected to the stator of a three-phase induction motor, a rotating magnetic field is produced and the rotor starts rotating. Thus a three phase Induction motor is self-starting.

The induction motor is fundamentally a transformer in which the stator is the primary and the rotor is short-circuited secondary. At starting, the voltage induced in the induction motor rotor is maximum (s = 1). Since the rotor impedance is low, the rotor current is very large. This large rotor current is reflected in the stator because of transformer action. This results in high starting current (4 to 10 times the full-load current) in the stator at low power factor and consequently the value of starting torque is low. Because of the short duration, this value of large current does not harm the motor if the motor accelerates normally.

However, this large starting current will produce large line-voltage drop. This will affect the operation of other electrical equipment connected to the same lines. Therefore, it is desirable and necessary to reduce the magnitude of stator current at starting. Thus the purpose of a starter is not to start the motor but to limit the heavy starting current of the motor at the time of starting.

Methods of Starting Three Phase Induction Motors:

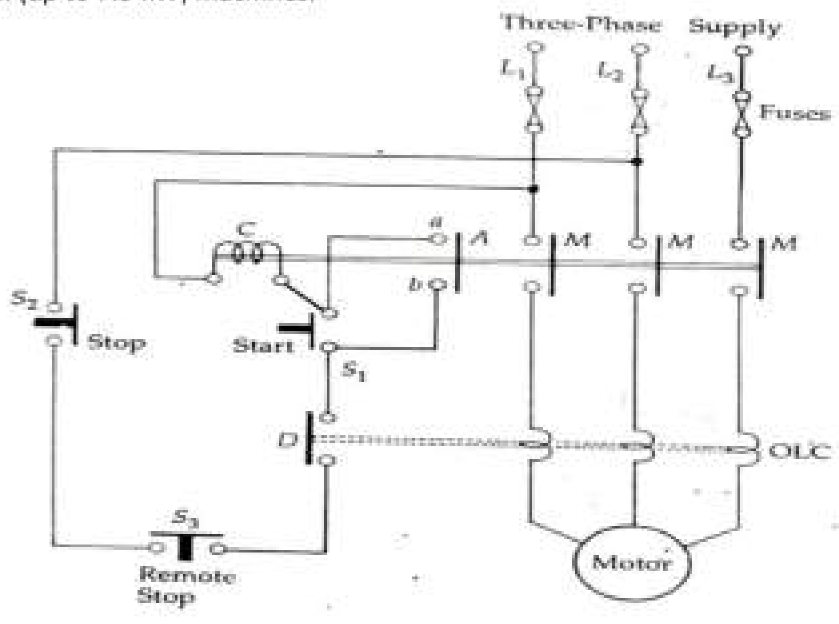
The method to be employed in starting a given induction motor depends upon the size of the motor and the type of the motor. The methods used to start induction motors are:

(i) Direct-on-line starting
(ii) Stator resistance starting
(iii) Autotransformer starting
(iv) Star-delta starting
(v) Rotor resistance starting

Methods (i) to (iv) are applicable to both squirrel-cage and slip ring motors. However, method (v) is applicable only to slip ring motors.
Except direct-on-line starting, all other methods of starting squirrel-cage motors employ reduced voltage across motor terminals at starting.

Direct-on-line starting:

In this method of starting the motor is started by connecting it directly to 3-phase supply. The impedance of the motor at standstill is relatively low and when it is directly connected to the supply system, the starting current will be high (4 to 10 times the full- load current) and at a low power factor. Consequently, this method of starting is suitable for relatively small (up to 7.5 kW) machines.



D.O.L starter consists of a coil-operated contactor C controlled by start and stop push buttons which may be installed at convenient places remote from the starter. On pressing the START push button S_1, (which is normally held open by a spring) the contactor coil C is energised from two line conductors L_1 and L_2. The three main contacts M and the auxiliary contact A close and the terminals a and b are short-circuited. The motor is thus connected to the supply. When the pressure on S_1 is released, it moves back under spring action.Even then the coil C remains energised through ab. Thus, the main contacts M remain closed and the motor continues to get supply. For this reason, contact A is called hold-on-contact.

When the STOP push button S_2 (which is normally held closed by spring) is pressed, the supply through the contactor coil Cis disconnected. Since the coil C is de energised, the main contacts M and auxiliary contact A are opened. The supply to motor is disconnected and the motor stops.

- When the voltage falls below a certain value, or in the event of failure of supply during motor operation, the col C is de-energised. The motor is then disconnected from the supply.
- In case of an overload on the motor, one or all the overload coils (O.LC) are energised. The normally closed contact D is opened and the contactor coil C is de-energised to disconnect the supply to the motor.

Fuses are provided in the circuit for short-circuit protection.

Direct-on-line starting is a simple and cheap method. The starting current be as large as 10 times the full load current and the starting torque is equal to full-load torque. Such a large starting current produces excessive voltage droop in the line supplying the motor. Small motors up to 5kW rating may be started by D.O.L. starters to avoid supply voltage fluctuations.

Relation between starling and F.L. torques. We know that:

$$\text{Rotor input} = 2\pi N_s T = kT$$

But $$\text{Rotor Cu loss} = s \times \text{Rotor input}$$

$$\therefore \quad 3(I_2)^2 R_2 = s \times kT$$

or $$T \propto (I_2)^2/s$$

or $$T \propto I_1^2/s \qquad (\because I_2 \propto I_1)$$

If I_{st} is the starting current, then starting torque (T_{st}) is

$$T \propto I_{st}^2 \qquad (\because \text{ at starting } s = 1)$$

If I_f is the full-load current and s_f is the full-load slip, then,

$$T_f \propto I_f^2/s_f$$

$$\therefore \quad \frac{T_{st}}{T_f} = \left(\frac{I_{st}}{I_f}\right)^2 \times s_f$$

When the motor is started direct-on-line, the starting current is the short-circuit (blocked-rotor) current I_{sc}.

$$\therefore \quad \frac{T_{st}}{T_f} = \left(\frac{I_{sc}}{I_f}\right)^2 \times s_f$$

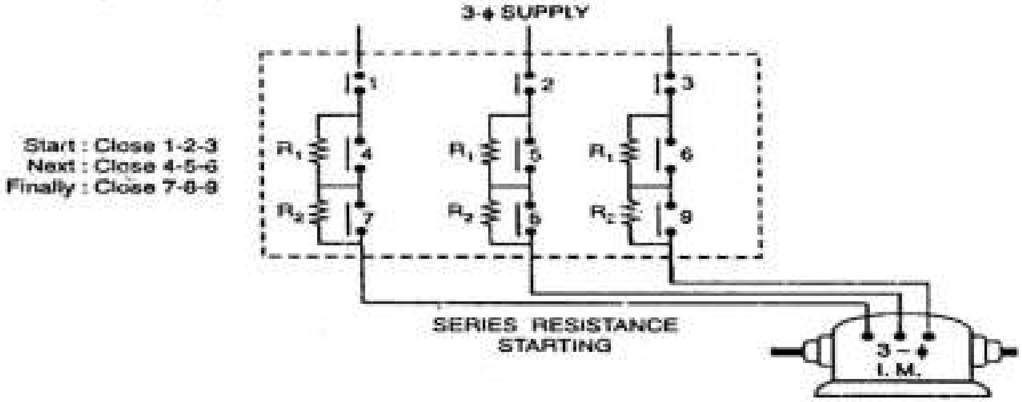
Note that starting current is as large as five times the full-load current but starting torque is just equal to the full-load torque. Therefore, starting current is very high and the starting torque is comparatively low. If this large starting current flows for a long time, it may overheat the motor and damage the insulation.

Stator resistance starting:

In this method, external resistances are connected in series with each phase of stator winding during starting. This causes voltage drop across the resistances so that voltage available across motor terminals is reduced and hence the starting current. The starting resistances are gradually cut out in steps (two or more steps) from the stator circuit as the motor picks up speed. When the motor attains rated speed, the resistances are completely cut out and full line voltage is applied to the rotor.

Drawback:

- First, the reduced voltage applied to the motor during the starting period lowers the starting torque and hence increases the accelerating time.
- Secondly, a lot of power is wasted in the starting resistances.



Relation between starting and F.L. torques.

Let V be the rated voltage/phase. If the voltage is reduced by a fraction x by the insertion of resistors in the line, then voltage applied to the motor per phase will be xV.

So,

$$I_{st} = x\, I_{sc}$$

Now $$\frac{T_{st}}{T_f} = \left(\frac{I_{st}}{I_f}\right)^2 \times s_f$$

or $$\frac{T_{st}}{T_f} = x^2 \left(\frac{I_{sc}}{I_f}\right)^2 \times s_f$$

Thus while the starting current reduces by a fraction x of the rated-voltage starting current (I_{sc}), the starting torque is reduced by a fraction x^2 of that obtained by direct switching. The reduced voltage applied to the motor during the starting period lowers the starting current but at the same time increases the accelerating time because of the reduced value of the starting torque. Therefore, this method is used for starting small motors only.

Autotransformer starting:

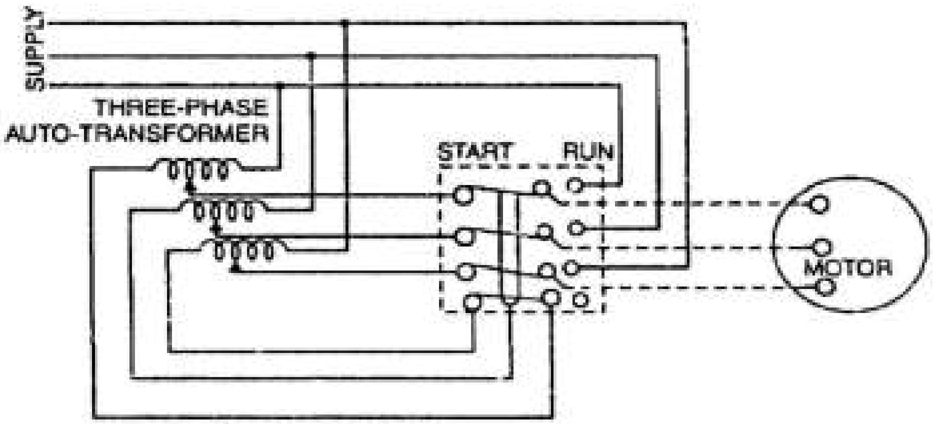
This method also aims at connecting the induction motor to a reduced supply at starting and then connecting it to the full voltage as the motor picks up sufficient speed. The tapping on the autotransformer is so set that when it is in the circuit, 65% to 80% of line voltage is applied to the motor.

At the instant of starting, the change-over switch is thrown to "start" position. This puts the autotransformer in the circuit and thus reduced voltage is applied to the circuit. Consequently, starting current is limited to safe value. When the motor attains about 80% of normal speed, the changeover switch is thrown to "run" position. This takes out the autotransformer from the circuit and puts the motor to full line voltage.

Advantages of Autotransformer starting:

(i) low power loss,
(ii) low starting current and
(iii) less radiated heat.

For large machines (over 25 H.P.), this method of starting is often used. This method can be used for both star and delta connected motors.



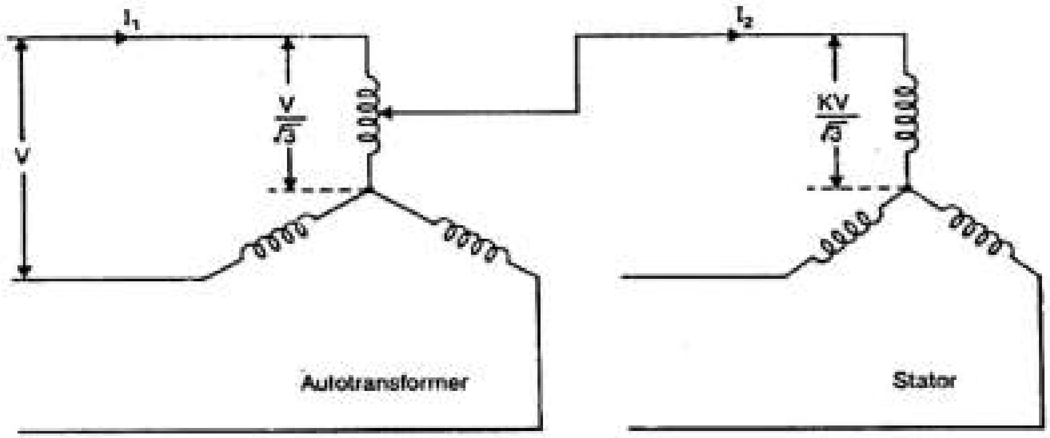
Relation between starting And F.L. torques. Consider a star-connected squirrel-cage induction motor. If V is the line voltage, then voltage across motor phase on direct switching is $V/\sqrt{3}$ and starting current is $I_{st} = I_{sc}$. In case of autotransformer, if a tapping of transformation ratio K (a fraction) is used, then phase voltage across motor is $KV/\sqrt{3}$ and $I_{st} = K\,I_{sc}$.

Now $$\frac{T_{st}}{T_f} = \left(\frac{I_{st}}{I_f}\right)^2 \times s_f = \left(\frac{K\,I_{sc}}{I_f}\right)^2 \times s_f = K^2\left(\frac{I_{sc}}{I_f}\right)^2 \times s_f$$

$$\therefore \quad \frac{T_{st}}{T_f} = K^2\left(\frac{I_{sc}}{I_f}\right)^2 \times s_f$$

The current taken from the supply or by autotransformer is $I_1 = KI_2 = K^2I_{sc}$.

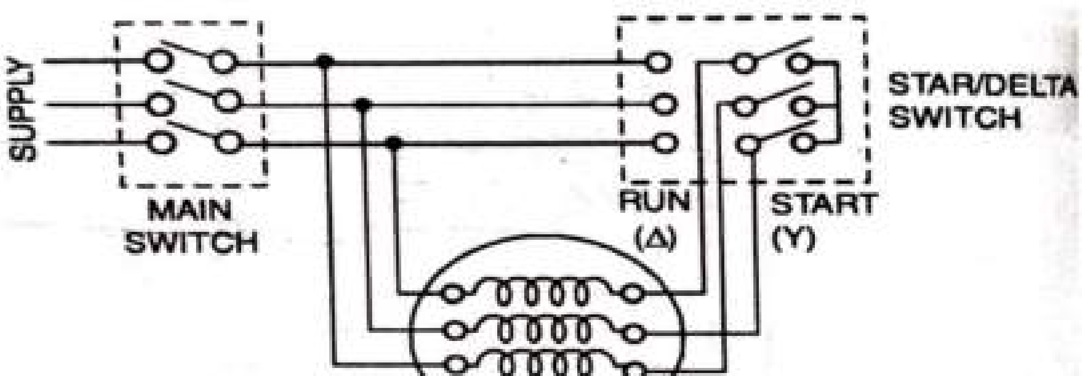
The motor current is K times, the supply line current is K^2 times and the starting torque is K^2 times the value it would have been on direct-on-line starting.



Star-delta starting:

The stator winding of the motor is designed for delta operation and is connected in star during the starting period. When the machine is up to speed, the connections are changed to delta.

The six leads of the stator windings are connected to the changeover switch as shown in figure below. At the instant of starting, the changeover switch is thrown to "Start" position which connects the stator windings in star. Therefore, each stator phase gets V/√3 volts where V is the line voltage. This reduces the starting current. When the motor picks up speed, the changeover switch is thrown to "Run" position which connects the stator windings in delta. Now each stator phase gets full line voltage V.



Disadvantages of this method are:

a) With star-connection during starting, stator phase voltage is $1/\sqrt{3}$ times the line voltage. Consequently, starting torque is $\left(1/\sqrt{3}\right)^2$ or $1/3$ times the value it would have with Delta- connection. This is a large reduction in starting torque.

b) The reduction in voltage is fixed.

This method of starting is used for medium-size machines (up to about 25 H.P)

Relation between starting and F.L. torques. In direct delta starting,

Starting current/phase, $I_{sc} = V/Z_{sc}$ where V = line voltage

Starting line current = $\sqrt{3}\ I_{sc}$

In star starting, we have,

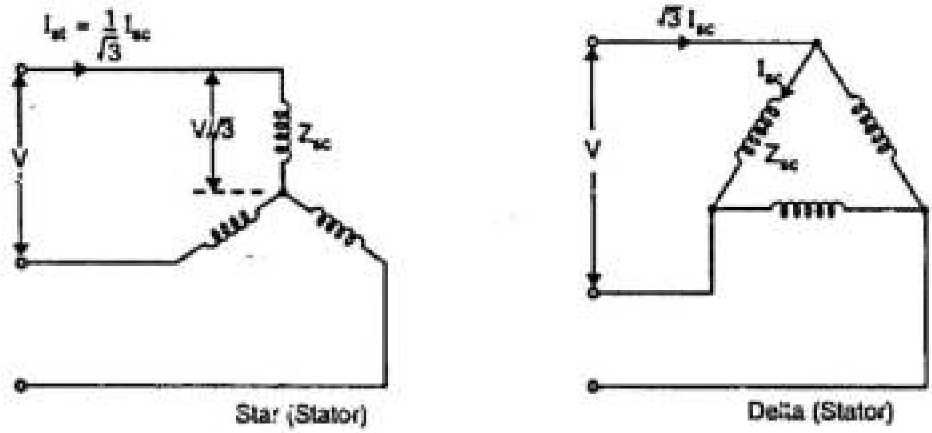
Starting current/phase, $I_{st} = \dfrac{V/\sqrt{3}}{Z_{sc}} = \dfrac{1}{\sqrt{3}} I_{sc}$

Now $$\frac{T_{st}}{T_f} = \left(\frac{I_{st}}{I_f}\right)^2 \times s_f = \left(\frac{I_{sc}}{\sqrt{3} \times I_f}\right)^2 \times s_f$$

or $$\frac{T_{st}}{T_f} = \frac{1}{3}\left(\frac{I_{sc}}{I_f}\right)^2 \times s_f$$

where I_{sc} = starting phase current (delta)

I_f = F.L. phase current (delta)



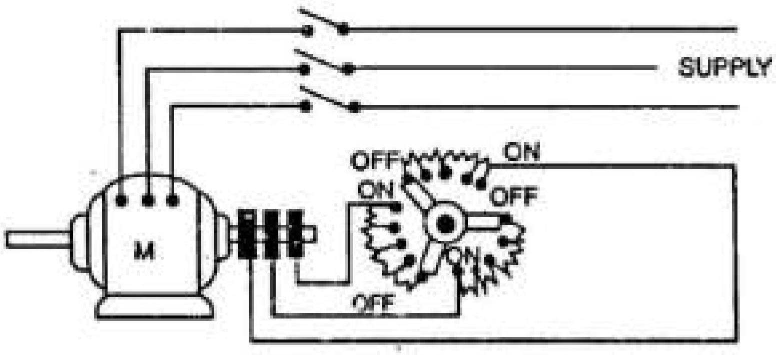
In star-delta starting, the starting line current is reduced to one-third as compared to starting with the winding delta connected. Further, starting torque is reduced to one-third of that obtainable by direct delta starting. This method is cheap but limited to applications where high starting torque is not necessary e.g., machine tools, pumps etc.

Rotor resistance starting:

Slip-ring motors are invariably started by rotor resistance starting. In this method, a variable star- connected rheostat is connected in the rotor circuit through slip rings and full voltage is applied to the stator winding as shown in Fig.

i. At starting, the handle of rheostat is set in the OFF position so that maximum resistance is placed in each phase of the rotor circuit. This reduces the starting current and at the same time starting torque is increased.

ii. As the motor picks up speed, the handle of rheostat is gradually moved in clockwise direction and cuts out the external resistance in each phase of the rotor circuit. When the motor attains normal speed, the change-over switch is in the ON position and the whole external resistance is cut out from the rotor circuit.



Speed Control of Induction Motors:

The slip of an induction motor is very small (< 3%) so that it is essentially a "constant-speed motor. Therefore, it is suitable for use in essentially constant-speed drive systems. The speed of an induction motor can be changed by the following methods:

1. By changing the number of stator poles (P).
2. By changing the line frequency
3. By changing the applied voltage.
4. By changing resistance in the rotor circuit.

Speed Control by changing number of stator poles:

We know that synchronous speed of induction motor $N_s = \frac{120f}{P}$. Therefore, by changing the number of stator poles (P), the synchronous speed and hence the rotor speed (N) can be changed. This method is easily applicable to squirrel cage motors but is not practicable for wound rotor motors. Squirrel cage motors designed for pole-changing control are commonly called multispeed motors.

Speed Control by changing Line frequency:

We know that synchronous speed of an induction motor is given by $N_s = \frac{120f}{P}$. Therefore, by changing the line frequency f, the synchronous speed (N_s) of the motor and hence the running speed (N) can be changed.

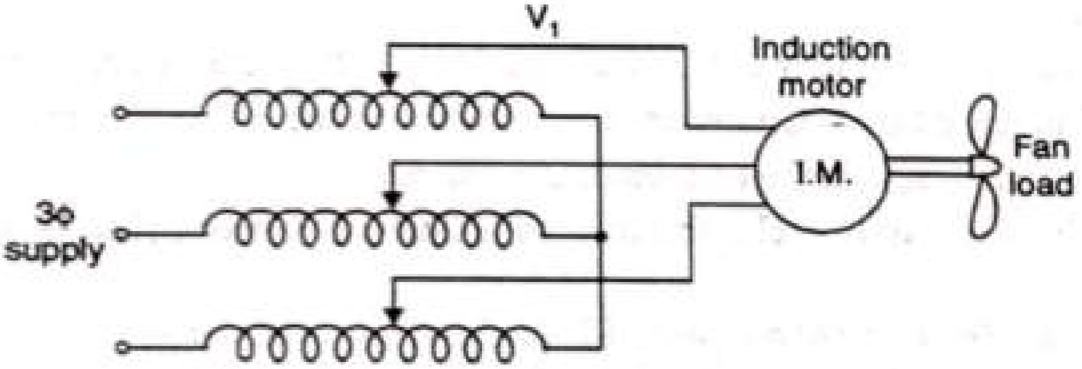
When employing line-frequency control, the applied line voltage should be changed in direct proportion to the frequency i.e. if frequency is increased, the supply voltage must also be increased and if the frequency is decreased, the supply voltage must also be decreased proportionately. This is necessary to maintain an approximately constant flux in the air-gap of the machine, otherwise the motor performance will not be satisfactory. Under these conditions, the maximum developed torque will remain approximately constant and the output power will vary approximately in direct proportion to the speed of the motor.

Disadvantages:

It involves the use of 3-phase variable frequency power supply. The auxiliary equipment required for this purpose results in a high first cost, increased maintenance and lowering of the overall efficiency.

Speed Control by changing applied Voltage:

We know that torque developed (T) by an induction motor is directly proportional to the square of applied voltage (V) i.e $T \propto V^2$. Therefore, by changing the applied voltage, the torque and hence speed (or slip) of the motor can be changed. Fig. shown below shows the arrangement to control the speed of induction motor (squirrel cage or wound rotor motor) by changing the applied voltage.



The motor is supplied from 3-phase Supply through a 3-phase autotransformer. The motor drives fan load. The voltage applied to the motor can be changed by the autotransformer and hence desired motor speed can be obtained. when we change the applied voltage, the slip (s) of the motor is changed i.e. motor speed changes.

Limitations: The stator voltage control method is the cheapest and the easiest method of speed control of induction motors. However, it is rarely used because of the following drawbacks

i. A large change in voltage is required for a relatively small change in speed.
ii. The large change in voltage results in large change in the flux density. This affects the magnetic conditions and hence performance of the motor.

Speed Control by changing Rotor circuit Resistance

This method of speed control is suitable only for slip- ring motors. The speed of the motor can be decreased by adding external resistance to the rotor. Under normal running condition, the relation between torque (T) and slip (s) of an induction motor is given by:

$$T \propto \frac{s}{R_2}$$

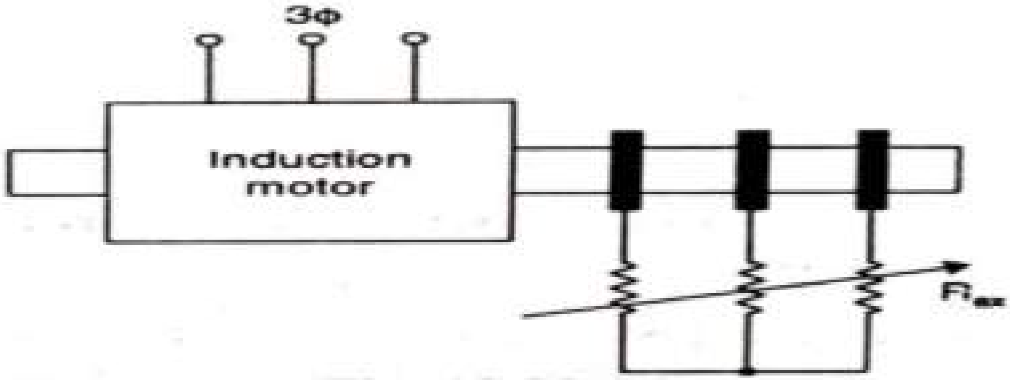
where R, is the rotor resistance/phase.

From the above relation, for a given torque, $s \propto R_2$.Therefore slip can be increased (i.e. motor speed can be decreased) by increasing the rotor resistance.

Drawbacks:

i. There is an increase in the rotor Cu losses due to the increased rotor circuit resistance.
ii. Due to increased rotor Cu losses, the efficiency of the motor is decreased.
iii. There is an increase in the temperature of the motor.

Because of the above drawbacks, this method is used where speed changes are required for short periods only.



Plugging of an Induction motor:

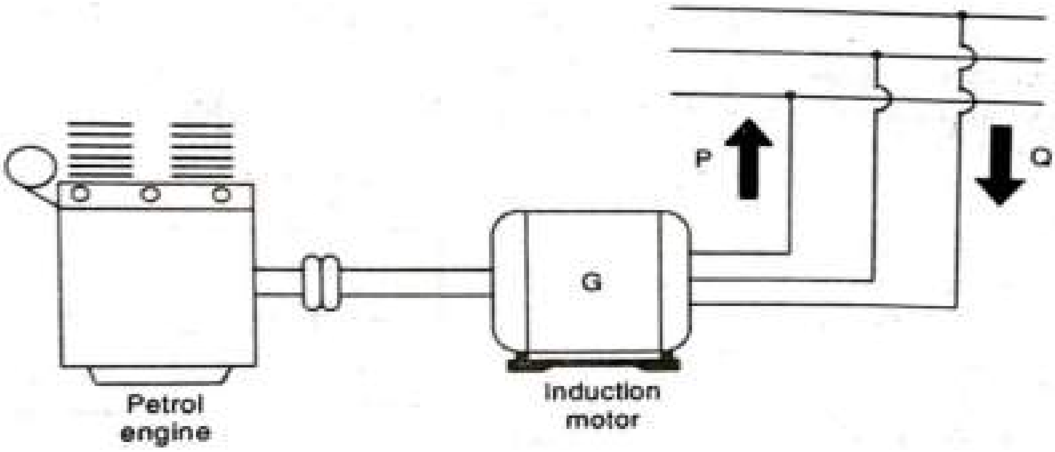
- To bring the running Induction motor to a rapid stop, the two stator leads can be simply interchanged. This process is called plugging.
- When we interchange two stator leads, the revolving field suddenly turns in the opposite direction to the rotor. During the plugging period, the motor acts as a brake. It absorbs kinetic energy from the still-revolving field, causing its speed to fall.
- The mechanical power associated with the rotor is entirely dissipated as heat in the rotor. At the same time rotor also continues to receive power from the stator which is also dissipated as heat. Consequently, plugging produces I^2R losses in the rotor which even exceed those when the rotor is locked.
- Motors should not be plugged too frequently because high rotor temperatures may melt the rotor bars or overheat the stator winding. When very high inertia loads have to be brought to a stop, wound-rotor motors are recommended because most of the thermal energy absorbed by the rotor is dissipated by the external resistors. Furthermore, we can maintain a consistently high torque by gradually varying the rotor resistance during deceleration period.

Induction Generator:

If an induction motor whose stator windings are connected to a 3-phase line is driven by a mover prime- at a speed higher than synchronous speed, it acts as a generator. It converts the mechanical energy it receives from the prime-mover into electrical energy and this electrical energy is supplied to the mains. Such a machine is called an induction generator or asynchronous generator.

When of speed the induction motor exceeds the synchronous speed, the slip (s) becomes negative. Therefore, the relative motion between rotor conductors and the rotating flux is reversed and as a result, the directions of rotor e.m.f. and the rotor currents will also be reversed. However, as soon as this takes place, the motor develops a counter torque which opposes the increase in speed. Thus generator operation occurs and mechanical energy of the prime-mover is converted into electrical energy which is supplied to the mains.

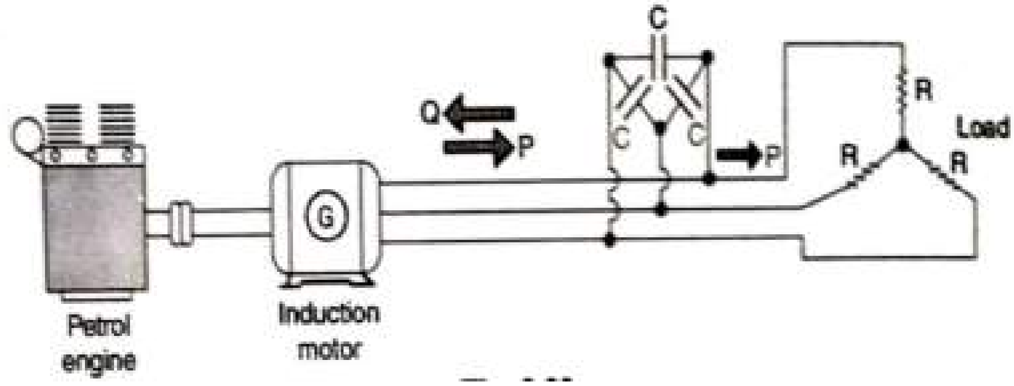
Figure shown below shows an induction generator connected to a 3-phase line. The petrol engine is the prime-mover. As the engine speed exceeds the synchronous speed, the motor becomes a generator, delivering active power P (kW) to the electrical systems (i.e. 3-phase which line in this case) to it is connected. However, to create its magnetic field, the motor has to absorb reactive power Q (kVAR). This power can only come from the supply lines. Consequently, the reactive power Q flows in the opposite direction to the active power P.

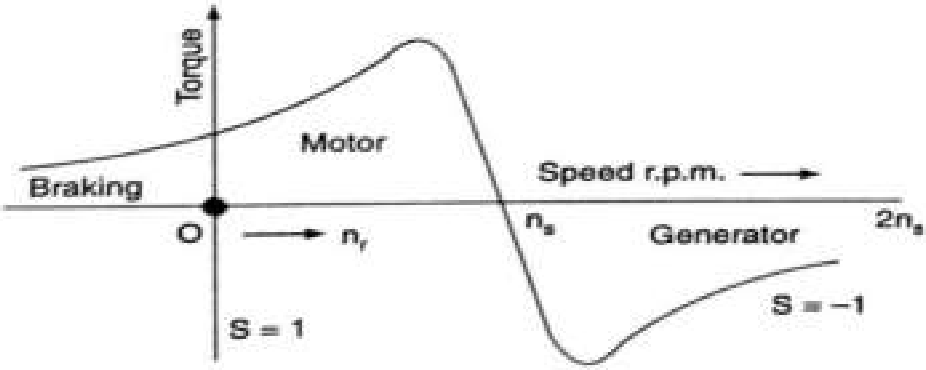


The active power P (kW) delivered is directly proportional to the slip above synchronous speed. Thus, a higher engine speed produces a greater output. However, the rated output is reached at small slip, generally less than 3%.

An Induction generator will deliver power only if it is supplied with proper reactive power to create its magnetic field. For this reason, an induction generator is generally connected to a 3-phase line. The reactive power may be supplied by a group of capacitors connected to the terminals of the motor.

The terminal voltage increases with the capacitance, but its magnitude is limited by saturation in the iron. If the capacitance is insufficient, the generator voltage will not build up. The capacitor bank must be large enough to supply the reactive power the machine normally absorbs when operating as a motor.





Torque-speed curve of induction machine showing braking, motoring and generating regions.

Applications of Induction Generators:

The induction generator is not a self-excited generator. It is necessary to excite the stator with an external polyphase source at its rated voltage and frequency. It will generate only when it is connected to a source of fixed voltage and frequency and if it is then driven at a speed above the synchronous speed.

Thus the induction or asynchronous generator has limited applications. The most important use of the principle of the Induction generator lies in automatic dynamic braking. For example, in a lift or crane driven by an induction motor, when the laden cage or hook is descending, the load torque on the motor acts in the direction of rotation. As a result, the motor speed exceeds the synchronous speed and the machine automatically becomes an induction generator and produces a braking torque, returning the energy of the descending load to the supply.

Cogging in 3-phase Induction Motor:

A squirrel-cage rotor may show a peculiar behaviour in starting for certain relationship between the number of stator slots (S_1) and rotor slots (S_2). If S_1, is equal to or an integral multiple of S_2, the motor may refuse to start. This phenomenon is known as cogging and is due to the magnetic locking between the stator and rotor teeth.

The reluctance of the magnetic path depends upon the positions of rotor teeth w.r.t. stator teeth. The reluctance of the magnetic path is minimum when the rotor and stator teeth face each other. In such positions of minimum reluctance, there exists a strong alignment force between the stator and the rotor at standstill. The alignment force at the instant of start may become stronger than the starting torque. Consequently, the motor fails to start. To avoid cogging, the number of stator and rotor slots are never made to be equal or have an integral ratio.

Crawling in 3-phase induction Motor:

Induction motors, particularly the squirrel-cage type, sometimes show a tendency to run at speeds as low as one-seventh ($1/7^{th}$) of their synchronous speed Ns. This peculiar behaviour of the cage motor at starting is known as crawling of an induction motor. This happens due to harmonic induction torques.

Crawling signifies running of motor at almost one seventh of the rated speed due to interference of seventh harmonics, crawling usually occurs when the motor is started with a coupled mechanical load. This action is due to the fact that flux wave produced by a stator winding is not purely sine wave instead it is a complex wave consisting a fundamental wave and odd harmonics like 3rd, 5th, 7th etc.

COMPARISON BETWEEN INDUCTION MOTOR AND TRANSFORMER:

An induction motor may be considered to be a transformer with a rotating short-circuited secondary The stator winding corresponds to transformer primary and rotor winding to transformer secondary. The differences between the two are:

(i) Unlike a transformer, the magnetic circuit of a 3-phase induction motor has an air gap. Therefore, the magnetizing current in a 3-phase induction motor is much larger than that of the transformer. For example, in an induction motor, it may be as high as 30-50% of rated current whereas it is only 1 - 5% of rated current in a transformer.

(ii) In an induction motor, there is an air gap and the stator and rotor windings are distributed along the periphery of the air gap rather than concentrated on a core as in a transformer. Therefore, the leakage reactances of stator and rotor windings are quite large compared to that of a transformer.

(iii) In an induction motor, the inputs to the stator and rotor are electrical but the output from the rotor is mechanical. However, in a transformer, input as well as output is electrical.

(iv) The main difference between the induction motor and transformer lies in the fact that the rotor voltage and its frequency are both proportional to slip s. If f is the stator frequency, E_2 is the per phase rotor e.m.f. at standstill and X_2 is the standstill rotor reactance/phase, then at any slip s, these values are:

Rotor e.m.f./phase, $E_2{}' = sE_2$,

Rotor reactance/phase, $X_2{}' = sX_2$

Rotor frequency, $f' = sf$

Comparison between Squirrel Cage and Slipring Induction Motors:

Sl. No.	Characteristics	Squirrel-cage motor	Slip-ring motor
1.	Speed	Almost constant but decreases slight with increased load	Speed decrease more rapidly than in cage motor
2.	Torque	Starting torque is less but running torque is good.	Starting torque is about three times the full load torque.
3.	Current	Starting current is about 5-6 times the full load current	Stating current is about two times the full load current.
4.	Speed control	Done by changing poles.	Done by changing resistance of rotor circuit.
5.	Power factor	Low (about 0.7 to 0.8)	High (about 0.8 to 0.9)
6.	Cost of fabrication	Low	Higher
7.	Maintenance cost	Very low	High (due to presence of brushes, brush gears, extra resistance etc.)
8.	Brushes	Absence of brushes reduces the risk of sparking	More chances of sparking
9.	Efficiency	Higher efficiency	Less efficiency
10.	Applications	Lathe, drills, printing machines, blowers etc.	Lifts, cranes, etc. where high starting torque is needed.

CHAPTER-4

SINGLE PHASE INDUCTION MOTOR

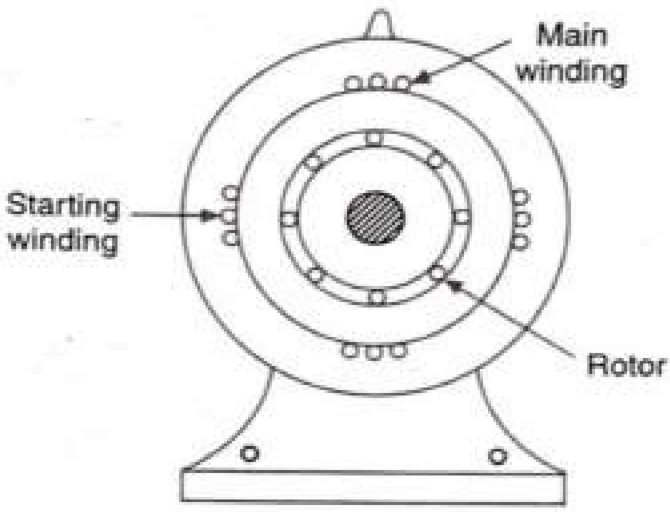
Single phase Induction motor is a popular type of a.c. electrical motor which is used widely in many areas. Single phase Induction motors perform a great variety of useful services in domestic, commercial as well as industrial purposes such as fans, refrigerators, washing machines, vacuum cleaner, kitchen equipment and farming appliance etc.

Single phase motors are generally manufactured in fractional HP ratings below 1 HP for economic reasons. Hence, those motors are generally referred to as fractional horsepower motors with a rating of less than 1 HP.

The characteristics of single phase induction motors are identical to 3-phase induction motors except that single phase induction motor has no inherent starting torque and some special arrangements have to be made for making itself starting.

Construction:

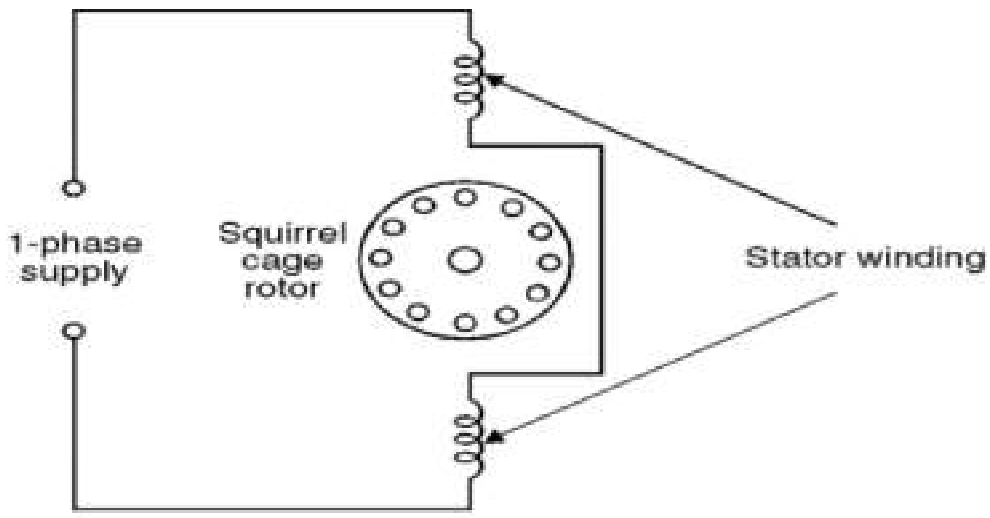
- The construction of a single phase induction motor is a similar to that a 3-phase induction motor. The rotor is cylindrical in shape and always in squirrel cage while the stator carries a single phase winding.
- The stator winding placed in slots around the inner periphery of a laminated ring. In addition the stator also carries an auxiliary winding for providing the starting torque, so that motor becomes self starting.
- The slots of rotor are not made parallel to each other but skewed to prevent magnetic locking of stator and rotor teeth.
- The squirrel cage rotor consists of aluminium bars. These aluminium bars are called rotor conductors and are placed in the slots on the periphery of the rotor.
- The rotor conductors are permanently shorted by the aluminium rings. It is not possible to add external resistance as the bars are permanently shorted. The absence of the sliprings and brushes make the construction of single phase induction motor very simple and robust.



Construction of single phase induction motor

Working:

- When single phase a.c. supply is given to stator winding of single phase induction motor, the alternating current produces an alternating flux called main flux.
- This magnetic field is pulsating in nature which means that field builds up in one direction falls to zero and again builds up in another direction.
- This pulsating current is incapable of producing a rotating torque in stationary rotor. But if the rotor is rotate by some external mechanical force in either direction rotor start to rotate in that direction continuously.
- So single phase induction motor is not self starting. In order to obtain a rotating field, that stator is provided with two windings the main winding and a starting winding. Starting winding is also called auxiliary winding.
- The phase difference of 90° between two windings is obtained by spliting the phase.
- So there are two fluxes one is main flux and another is called rotor flux. These two fluxes produce the desired torque which is required by the motor to rotate.
- When motor pick up 75% of rated speed, starting Winding is generally disconnected from supply and motor continuously run.



Double revolving field Theory:

Statement: The double field revolving theory states that any alternating quantity can be resolved into two components having magnitude half of the maximum magnitude of the alternating quantity and both these components rotating in opposite direction.

Theory:

In double field revolving theory an alternating sinusoidal flux ($\emptyset = \emptyset_m cos\omega t$) can be represented by two revolving fluxes, each equal to one-half of the maximum value of alternating flux (i.e., $\emptyset_m/_2$) and each rotating at synchronous speed ($N_s = \frac{120f}{P}$, $\omega = 2\pi f$) in opposite directions.

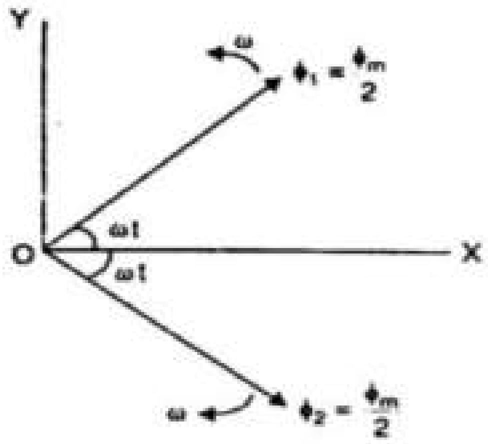
Consider two rotating magnetic fluxes $\emptyset_1$and $\emptyset_2$ each of magnitude $\emptyset_m/_2$ and rotating in opposite directions with angular velocity ω. The two fluxes start rotating from OX axis at t = 0. After time t seconds, the angle through which the flux vectors have rotated is ωt. By resolving the flux vectors along-X-axis and Y-axis,

Total X-component = $\frac{\emptyset_m}{2} cos\omega t + \frac{\emptyset_m}{2} cos\omega t = \emptyset_m cos\omega t$

Total Y-component = $\frac{\emptyset_m}{2} sin\omega t - \frac{\emptyset_m}{2} sin\omega t = 0$

Resultant flux, $\emptyset$ =$\sqrt{(\emptyset_m cos\omega t^2 + 0^2)}$ =$\emptyset_m cos\omega t$

Thus the resultant flux vector is $\emptyset = \emptyset_m cos\omega t$ along X-axis. Therefore, an alternating field can be replaced by two relating fields of half its amplitude rotating in opposite directions at synchronous speed.



When the rotating flux vectors are in phase, the resultant vector is $\emptyset = \emptyset_m$,when out of phase by 180°, the resultant vector $\emptyset = 0$.

Rotor at standstill

Consider the rotor is stationary and the stator winding is connected to a single-phase supply. The alternating flux produced by the stator winding can be presented as the sum of two rotating fluxes $\emptyset_1$and $\emptyset_2$, each equal to one half of the maximum value of alternating flux and each rotating at synchronous speed $N_s = \frac{120f}{P}$ in opposite directions. Let the flux $\emptyset_1$ rotate in anti clockwise direction and flux $\emptyset_2$, in clockwise direction. The flux $\emptyset_1$ will result in the production of torque T_1 in the anti clockwise direction and flux $\emptyset_2$ will result in the production of torque T_2 In the clockwise direction. At standstill, these two torques are equal and opposite and the net torque developed is zero. Therefore, single-phase induction motor is not self-starting.

Rotor running:

The flux rotating in the clockwise direction is the forward rotating flux ($\emptyset_f$) and that in the other direction is the backward rotating flux ($\emptyset_b$).

The slip w.r.t. the forward flux will be

$$s_f = \frac{N_s - N}{N_s} = s$$

Where N_s=synchronous speed

N = speed of rotor in the direction of forward flux

The slip w.r.t. the backward flux will be

$$S_b = \frac{N_s - (-N)}{N_s} = 2 - s$$

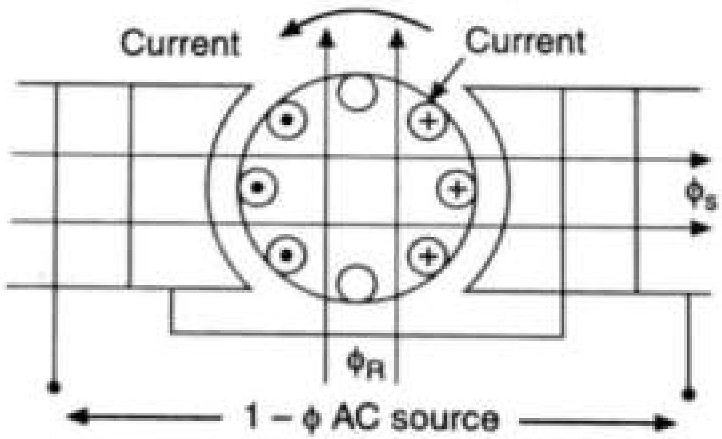
$$s_b = 2 - s$$

Thus for forward rotating flux, slip is s (less than unity) and for backward rotating flux, the slip is 2 - s (greater than unity).

Cross-Field Theory:

As soon as the rotor begins to tum a speed an emf E is induced in the rotor conductors, as they cut the stator flux. Thus voltage increases as the rotor speed increases. It causes current I_R to flow in the rotor bars facing the stator poles.

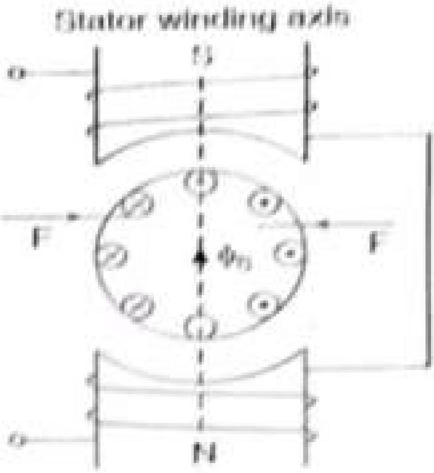
This currents produce an ac flux $\emptyset_R$ which act at right angle to the stator flux $\emptyset_s$.$\emptyset_R$ lags almost 90° behind $\emptyset_s$ owing to the inductance of the rotor. The combined action of $\emptyset_s$ and $\emptyset_R$ produces a revolving magnetic field, similar to that in three-phase motor. The value of $\emptyset_R$ increases with increasing speed, becoming almost equal to $\emptyset_s$ at synchronous speed and nearly perfect revolving field is produced.



Current induced in the rotor bars due to rotation

Rotor at standstill

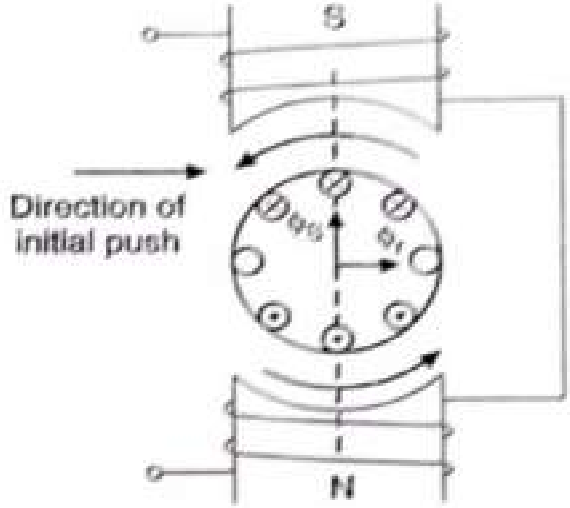
The stator winding in excited by the single phase a.c. supply. The supply produces an alternating flux $\emptyset_s$ which acts along the axis of stator winding. Due to this flux, emf gets induced in the rotor conductors due to transformer action. This emf circulates current through the rotor conductors. The direction of rotor current is so as to opposed the cause producing it, which is stator flux $\emptyset_s$.Now the rotor conductors experience force whose direction is found by Fleming's left hand rule shown in figure below. Thus overall, the force experienced by the rotor is zero. Hence no torque exists on the rotor and rotor cannot start rotating.



Rotor running:

Assume now that an initial push is given to the rotor in anticlockwise direction. Due to the rotation, the rotor physically cuts the stator flux and emf gets induced in the rotor. This is called rotational emf or speed emf and this emf is in phase with the stator flux $\emptyset_S$ donated as E_2. This emf circulates current through rotor which is I_2.This current produces its own flux called rotor flux $\emptyset_r$. The axis of $\emptyset_r$, is at 90°. The axis of stator flux hence the rotor flux is called cross field.

Thus $\emptyset_r$, is in quadrature with $\emptyset_s$, in space and lags, $\emptyset_s$ by 90° in time phase. Such two fluxes produce the rolating magnetic field. The direction of this rotating magnetic field will be same as the direction of intial push given. Thus rotor experience a torque in the same direction as that of rotating magnetic field i.e., the direction of initial push.



Why Single-phase Induction Motor is not self starting?

According to double field revolving theory, any alternating quantity can be resolved into two components, each component have magnitude equal to the half of the maximum magnitude of the alternating quantity and both these components rotate in opposite direction to each other.

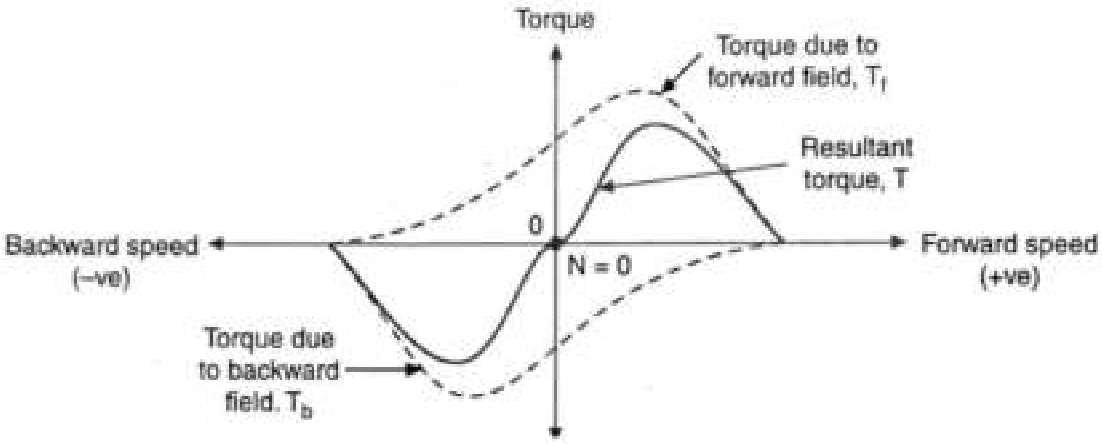
When a single phase ac supply is given to the stator winding of single phase induction motor, it produces its flux of magnitude$\emptyset_m$. According to the double field revolving theory, this alternating flux, $\emptyset_m$, is divided into two components of magnitude $\frac{\emptyset_m}{2}$. Each of these components will rotate in opposite direction, with the synchronous speed, Ns.

Let these two components of flux are forward component of flux, $\emptyset_f$ and backward component of flux$\emptyset_b$.The resultant of these two components of flux at any instant of time, gives the value of instantaneous stator flux at that particular instant.

i.e. $\emptyset_r = \frac{\emptyset_m}{2} + \frac{\emptyset_m}{2}$ or $\emptyset_r = \emptyset_f + \emptyset_b$

At starting, both the forward and backward components of flux are exactly opposite to each other Also both of these components of flux are equal in magnitude. So, they cancel each other and hence the net torque experienced by the rotor at starting is zero. So, the single phase induction motors are not self starting motors.

Torque-speed characteristics:



Torque-speed characteristic

At start N=0 and at that point resultant torque is zero. So single phase induction motors are not self starting. However if the rotor is given an initial rotation in any direction, the resultant average torque increase in the direction in which the rotor initially rotated and motor starts rotating in that direction .

Making Single-Phase Induction Motor Self-Starting:

The single-phase induction motor is not self starting. However if the rotor is rotate by some external mechanical force in either direction rotor start to rotate in that direction continuously, but in practice it is not possible to give initial torque to rotor externally. Hence some modifications are done in the construction of single phase induction motor to make them self starting.

To make a single-phase induction motor self-starting, a revolving stator magnetic field is produced. This may be achieved by providing an auxiliary winding (starting winding) in addition to the main winding for producing the starting torque, so that motor becomes self starting. When the motor attains sufficient speed, the starting means (i.e., additional winding) may be removed depending upon the type of the motor.

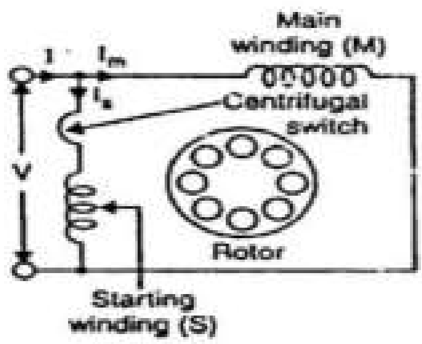
Types of Single Phase Induction Motors:

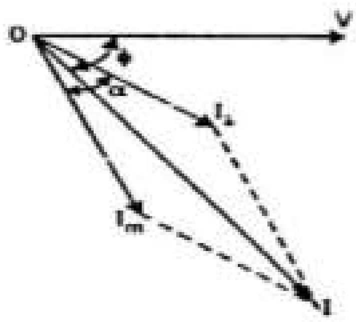
Single-phase induction motors are classified and named according to the method employed to make them self-starting.

1. **Split-phase motors**-started by two phase motor action through the use of an auxiliary or starting winding.
2. **Capacitor motors**-started by two-phase motor action through the use of an auxiliary winding and a capacitor.
3. **Shaded-pole motors**-started by the motion of the magnetic field produced by means of a shading coil around a portion of the pole structure.

Split-Phase Induction Motor:

- The stator of a split-phase induction motor is provided with an auxiliary or starting winding S in addition to the main or running winding M.
- The starting winding is located 90° electrical from the main winding and operates only during the period when the motor starts up.
- The two windings are so designed that the starting winding S has a high resistance and relatively small reactance while the main winding M has relatively low resistance and large reactance. Consequently, the currents flowing in the two windings have reasonable phase difference α (25° to 30°).





Main Parts of Split Phase Induction Motor:

1. Stator
2. Stator winding
3. Rotor
4. Centrifugal switch
5. End shield

1. **Stator:** Stator consists of steel sheet stampings having slots in its inner periphery. It serves the purpose to carry to stator winding and to cover, support and covering to other parts of the machine.
2. **Stator winding:** Split phase induction motor has two stator windings at a phase displacement of 90°. The running winding is always lower than the starting winding. The starting winding has more resistance. The split phase motors are usually wound to give $\frac{1}{2}\ to\ \frac{1}{3}$ horse power.
3. **Rotor:** The rotor of a split phase motor is very similar to the squirrel cage rotor of 3-phase induction motor. The core consists of steel sheet laminations having slots on the rotor periphery. The slots carry a number of copper, aluminium bars. The ends of the conductors in slot are connected and permanently short circuited by means of copper end rings.
4. **Centrifugal switch:** Centrifugal is a mechanical device which is used in split phase induction motor to disconnect the winding when starting the motor attains 75-80% of the synchronous speed. When the rotor of the motor pick up speed about 75% of synchronous speed, switch opens circuit of the starting winding. The centrifugal switch also prevents the motor from putting the drawing excessive current from main by starting winding out of the circuit.
5. **End Shield:** End shields are the end covers of the motor. It protects the motor from the dust and moisture etc. The entire weight of the rotor comes on the end bearings of the motor.

Operation:

(i) When the two stator windings are energized from a single-phase supply, the main winding carries current I_m while the starting winding carries current I_s .

(ii) Since main winding is made highly inductive while the starting winding highly resistive, the currents I_m and I_s have a reasonable phase angle α(25° to 30°) between them. Consequently, a weak revolving field approximating to that of a 2-phase machine is produced which starts the motor. The starting torque is given by;

$$T_s = kI_mI_s sin\alpha$$

where k is a constant whose magnitude depends upon the design of the motor.

(iii) When the motor reaches about 75% of synchronous speed, the centrifugal switch opens the circuit of the starting winding. The motor then operates as a single-phase induction motor and continues to accelerate till it reaches the normal speed. The normal speed of the motor is below the synchronous speed and depends upon the load on the motor.

Performance Characteristics:

(i) The starting torque is 1.5 to 2 times the full-loud torque mid (lie starting current is 6 to 8 times the full-load current.

(ii) Due to their low cost, split-phase induction motors are most popular single phase motors in the market.

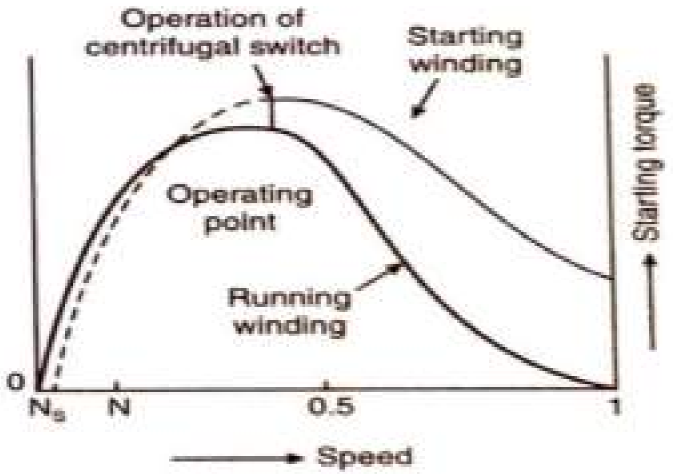
(iii) Since the starting winding is made of fine wire, the current density is high and the winding heats up quickly. If the starting period exceeds 5 seconds, the winding may burn out unless the motor is protected by built-in-thermal relay. This motor is, therefore, suitable where starting periods are not frequent.

(iv) These motors are essentially constant-speed motors. The speed variation is 2-5% from no-load to full load.

(v) These motors are suitable where a moderate starting torque is required and where starting periods are infrequent to drive.

Torque-speed characteristics of Split Phase Motor:

The high starting torque is obtained in a split phase induction motor due to high resistance in the starting winding. Such motors are available in sizes 30 to 200 watts. They gives fairly constant speed.



Reversal of direction of rotation: The direction of rotation of a 1-phase (split phase) induction motor can be reversed by reversing (inter-changing) the connections of either starting winding or running winding.

Applications:

- As starting torque is not so high so this machine is not used where large starting torque is required. It is used for smaller sizes about 0.25 H.P.
- It is used in washing machines, blowers, wood working tools, grinders and various other low starting torque applications.

Capacitors Motors:

The stator of the capacitor motors have two windings like split-phase induction motor i.e., starting winding and running winding, But in this motor phase angle between the currents of main and starting winding is obtained by using capacitors. Moreover, the phase splitting is achieved by using a capacitor is placed in series with the starting winding. The capacitor induces necessary phase shift.

Advantages of use of capacitor:

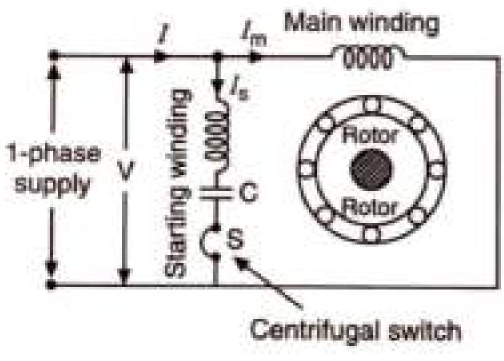
1. The starting torque is higher as compared to split phase motor.
2. Power factor of the motors gets improved.
3. Starting current is low.

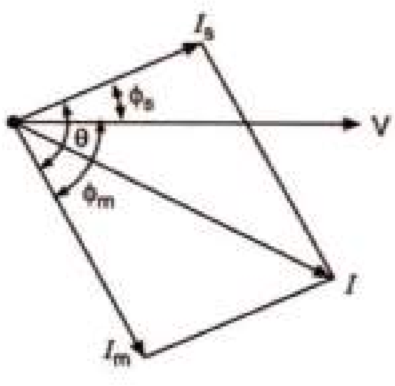
The capacitor may be connected in series with the starting winding in three different way therefore capacitor motor may be:

(i) Capacitor start motor
(ii) Capacitor run motor
(iii) Capacitor start and capacitor run motor

Capacitor start motor:

- In these types of motors, the necessary splitting of phase for starting is provided using capacitor.
- The capacitor generally used of electrolyte type and designed for short duty period. Electrolyte capacitor is connected in series with the starting winding along with centrifugal switch S.
- This switch disconnects the capacitor as soon as motor reaches 75% of full speed. The motor is not operated on running winding only. It is used where high starting is required.





Performance Characteristics:

(i) The starting characteristics of a capacitor-start motor are better than those of a split-phase motor, both machines possess the same running characteristics because the main windings are identical.

(ii) The phase angle between the two currents is about 80° compared to about 25° in a split-phase motor. Consequently, for the same starting torque, the current in the starting winding is only about half that in a split-phase motor. Therefore, the starting winding of a capacitor start motor heats up less quickly

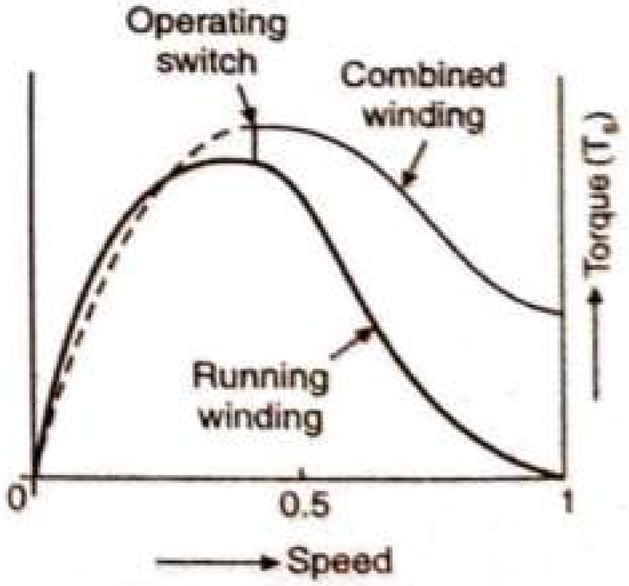
(iii) It is well suited to applications involving either frequent or prolonged starting periods.

(iv) Its full load efficiency is about 65%.

(v) It is a constant speed motor as there is a very small fall in speed with load.

Torque-speed Characteristics of Capacitor Start Motor:

Capacitor Start Motor is having a high starting torque as compared to an ordinary split phase motor. The power factor is also improved.



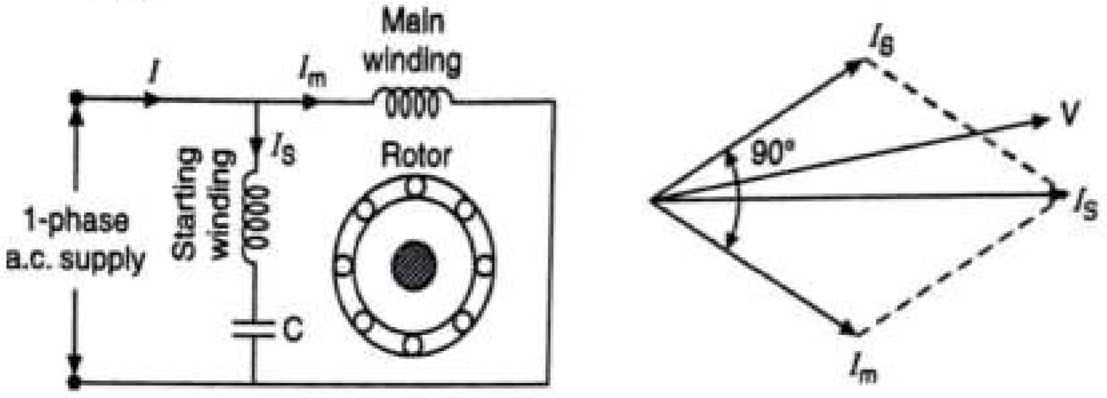
The **direction of rotation** of such motors can be **reversed** simple by interchanging the leads of either running or starting winding.

Applications:

- Capacitor-start motors are used where high starting torque is required and where the starting period may be long to drive.
- Hence these motors find their applications in pumps, compressor, conveyer and refrigerators etc. Such motors are available between 0.5 H.P to 1 H.P.

Capacitor run motor:

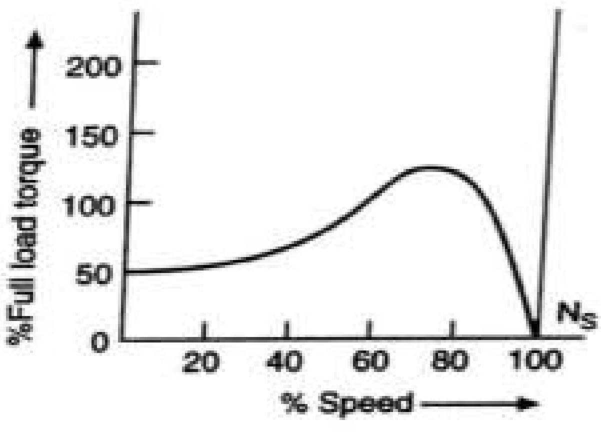
- In these motors, a paper capacitor is permanently connected in the starting winding. In this case electrolytic capacitor cannot be used since this type of capacitor is designed only for short time rating and hence cannot be permanently connected in the winding.
- Both main as well as starting winding is of equal rating and similar.
- No centrifugal switch or other such device has been used for disconnecting the starting winding. The rotor is squirrel cage.
- In this motor the phase difference between two current is 90° .so starting torque is high.



Performance Characteristics:

(i) The capacitor remains in circuit so resultant line current is low.
(ii) Power factor is improved may be about unity.
(iii) Its full load efficiency is higher about 75%.

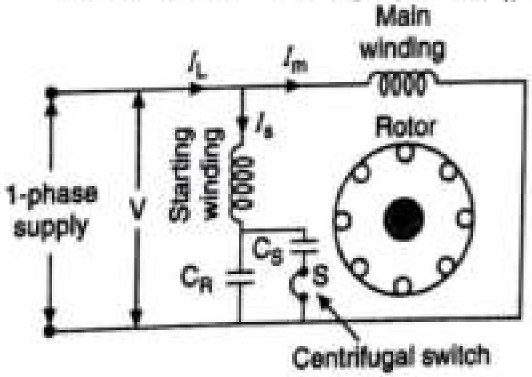
Torque-speed Characteristics:

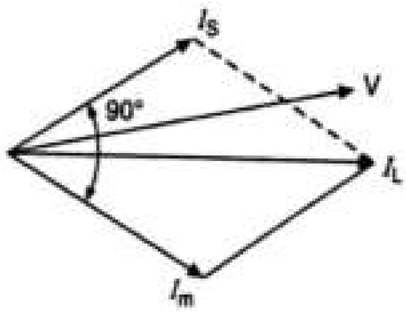


Applications: This motor finds application in fans, room coolers, portable tools and other domestic and commercial appliances.

Capacitor start and capacitor run motor:

- In this case, two capacitors are used one for starting purpose and other for running purpose.
- The capacitors used for starting purpose C_S is of electrolytic type and is disconnected from the supply when the motors attain 75% of synchronous speed with the help of centrifugal switch S.
- Whereas, the other capacitor C_R which remains in the circuit of starting winding during operation is a paper capacitor. Starting capacitor C_s which is of higher value than the value of running capacitor C_R.



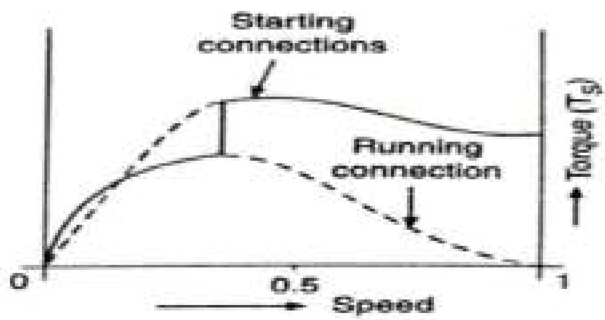


Performance Characteristics:

(i) The starting winding and the capacitor can be designed for perfect 2-phase operation at any load. The motor then produces a constant torque and not a pulsating torque as in other single-phase motors.
(ii) It improves the overload capacity of the motor.
(iii) It increases the efficiency of the motor.
(iv) It improves the power factor.
(v) It reduces the noise of the motor.
(vi) This type of motor gives best running and starting operation.

Torque-speed Characteristics:

Such motors operate as two phase motors giving best performance and noiseless operation. Starting torque is high, starting current is low and gives better efficiency and higher power factor.



Applications:

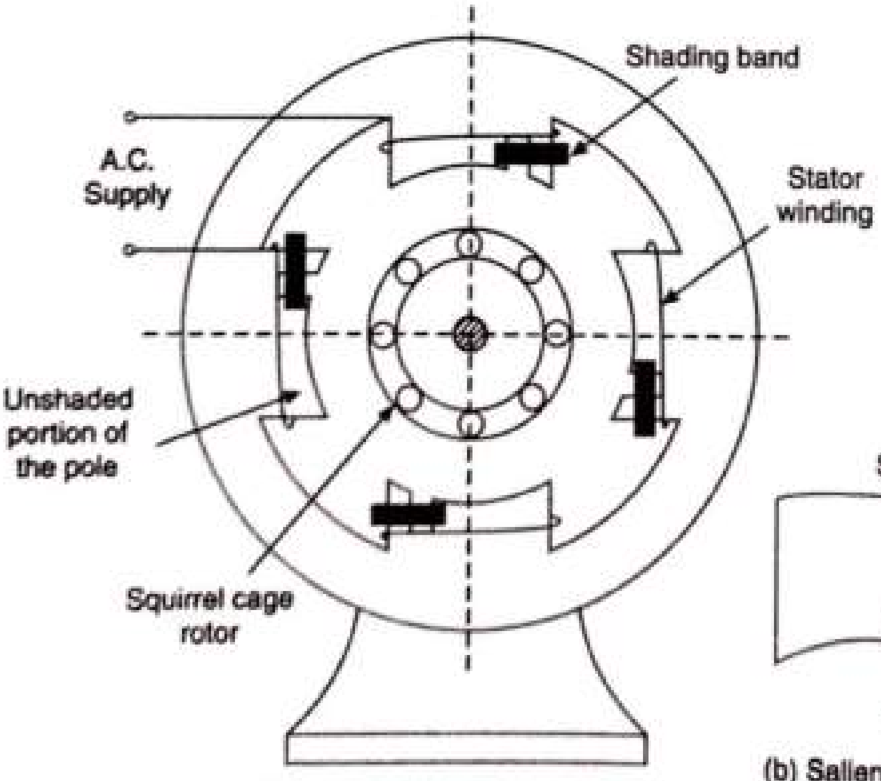
Because of constant torque, the motor is vibration free and can be used in: (a) hospitals (b) studios and (c) other places where silence is important.

Shaded-pole Motors:

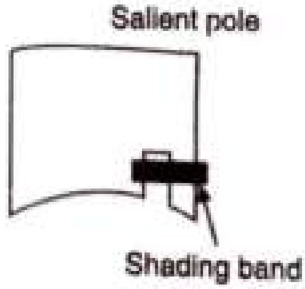
A shaded-pole motor may be defined as a single phase induction motor provided with short circuited auxiliary winding displaced in magnetic position from the main winding. The shaded pole motor has small output not exceeding 30 watts. Starting torque of shaded pole is very small. It is suitable in low power domestic appliances.

Construction:

- The stator of shaded pole motors have salient pole and rotor is squirrel cage. Each stator pole carries a magnetising coil.
- One third portion of each pole of stator is short circuited using copper band or ring known as Shading band/coil (shaded portion of the pole), because it causes the flux in that portion of the pole sourrounded by it to lag behind the flux in the rest of the pole.
- Basically, the pole is split in two parts at its face, shaded part and unshaded part.
- The rotor is also made of laminations. Along the circular surface, there are number of holes in which copper bars are fitted. The ends of these bars are soldered to copper end plate at each end.



(a) Schematic diagram



(b) Salient pole with shading band

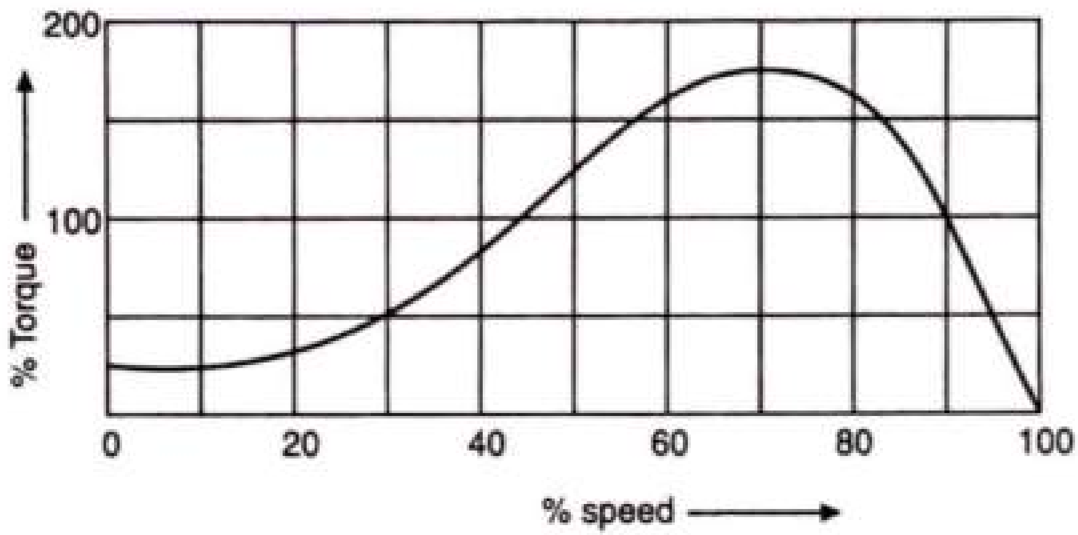
Operation:

i. When single phase ac. supply is given to the stator of shaded pole induction motor an alternating flux is produced.
ii. This changing flux induces emf in the shaded coil. Since this shaded portion is short circuited, the current is produced in shaded portion in such a direction to oppose the main flux.
iii. The flux in shaded pole lags behind the flux in the unshaded pole. The phase difference between these two fluxes produces resultant rotating flux.
iv. Thus due to this resultant rotating field emf is induced in the rotor, the rotor starts rotating due to single phase induction motor action additional torque is produced and rotor rotates continuously with the speed less than synchronous speed.
v. The direction of rotating field(flux) is from unshaded to shaded portion of the pole.

The reversal of direction of rotation in shaded pole motor is not possible.

Torque-speed characteristic:

The starting torque is small typically only 30 to 50 percent of the rated torque.



Torque-speed characteristic curve of a shaded pole motor.

Advantages:

1. It has rugged construction.
2. Small in size.
3. Cheaper in cost.
4. Low maintenance is required.
5. It is more reliable
6. There is no commutator, switch, contacts or brushes to give any trouble during operation.

Disadvantages:

1. Starting torque is very low about 8 to 15 percentage.
2. Low Power factor.
3. Small power rating.
4. The shaded-pole motors are inefficient because of the losses in the permanently shorted winding.

Applications:

As starting torque is very low, these motors are mainly used in record players, tape recorders, slide projectors, photo copying machine, starting of electric clocks, hair dryers, toys, gramophones.

CHAPTER-5

COMMUTATOR MOTORS

The commutator motors are so called because the wound rotor of this kind of motor is equipped with a commutator and brushes. This group consists of the following two classes:

1. Those operating on the principle of the series motor in which the energy is conductively carried both to the rotor armature and its series-connected single phase stator field.
2. Those operating on 'repulsion principle' (repulsion motors) in which energy is inductively transferred from the single phase stator field winding to the rotor.

A.C. SERIES MOTOR:

The series motor due to its desirable speed-torque characteristics is almost exclusively use in railway service. It is more convenient and more economical to transmit power and to transform voltages in A.C. systems than with direct currents has lead to the development of the A.C. series motor for use on some of the important electrifications.

Construction:

The construction of an a.c. series motor is very similar to a d.c. series motor but some modifications are necessary in d.c series motor that is to operate satisfactorily on a.c.

Modifications and improvement in design of D.C. series motor to operate on A.C. supply

In order to get satisfactory operation following modifications are to be done

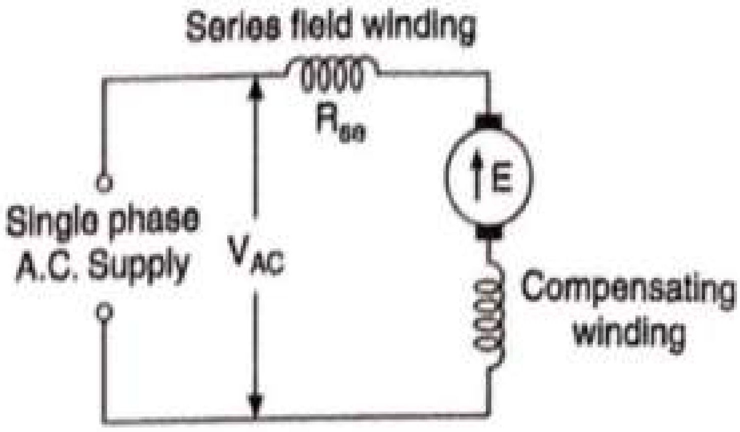
(i) The yoke and the poles should be made from laminations in order to reduce the eddy currents.

(ii) In order to reduce the effect of armature reaction, motor is provided with additional compensating winding in series field and armature winding.

(iii) In order to reduce inductive reactance, motor is built with a few turns. This reduces the voltage drop across the field winding.

(iv) In order to obtain the required torque, armature turns are increased.

(v) There is considerable sparking between the brushes and the commutator when the motor is used on a.c. supply. This can be eliminated by using high-resistance leads to connect the coils to the commutator segments.



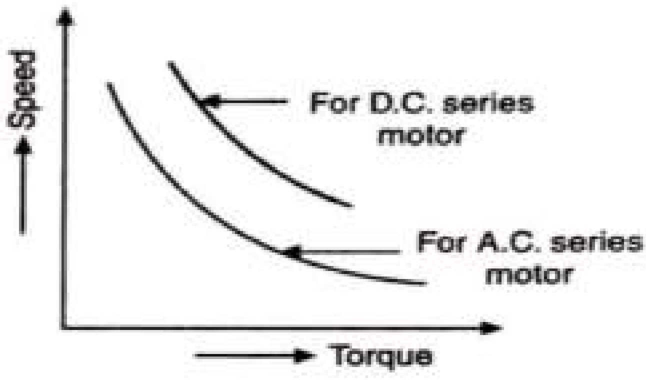
Working Principle:

The working principle of an A.C. series motor is the same as that of that D.C. series motor. The armature and field are wound and interconnected in the same manner as the D.C. series motor.

When the motor is connected to an a.c. supply, the same alternating current flows through the field and armature windings. The field winding produces an alternating flux that reacts with the current flowing in the armature to produce a torque. The field flux and armature current reverse simultaneously every half cycle, but the direction of the torque remains unchanged. The rotor, therefore, continuously rotate in the same direction.

Torque-speed Characteristic:

The torque speed characteristic of an a.c. series motor is similar to that of a dc. series motor. The torque varies as square of the current and speed varies inversely as the current. The efficiency of a.c. series motor is not good as compared to d.c. series motor due to greater eddy current loss and effect of power factor.



Advantages:

1. It is a constant speed motor.
2. The motor is very useful where constant speed is required such as electric clock etc.

Disadvantages:

To make a.c. series motor from d.c. series motor special structural changes must be needed to make in the motor to make it a practical and reasonable efficient machine.

Applications:

1. The most important application of a.c. series motor in electric traction.
2. For driving electric clocks and phonographs.

UNIVERSAL MOTOR:

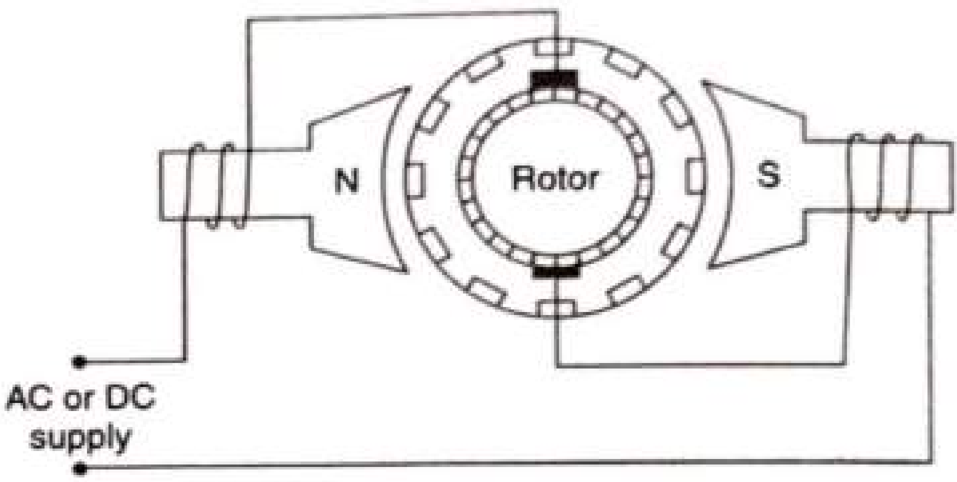
- Fractional-horsepower series motors that are adapted for use on either D.C. or A.C. circuits of a given voltage are called universal motors.
- These motors are generally series wound (armature and field winding are in series), and hence produce high starting torque.
- They run at lower speed on AC supply than they run on DC supply of same voltage, due to the reactance voltage drop which is present in AC and not in DC.

There are two basic types of universal motor: (i) compensated type and (ii) uncompensated type

Construction of Universal Motor:

The construction of a universal motor is very similar to construction of a d.c. machine.

- It consists of a stator on which field poles are mounted. Field coils are wound on the field poles.
- However, the whole magnetic path (stator field) circuit and also armature is laminated. Lamination is necessary to minimize the eddy currents which induce while operating on AC.
- The rotary armature is of wound type having straight or skewed slots and commutator with brushes resting on it.
- The commutation on AC is poorer than the for DC, because of the current induced in the armature coils. For that reason brushes used are having high resistance.



Working of Universal Motor:

A universal motor works on either DC or single phase AC supply. When the universal motor is fed with a DC supply. it works as a DC series motor. When current flows in field winding, it produces an electromagnetic field. The same current also flows from the armature conductors. When a current carrying conductor is placed in an electromagnetic field, it experiences a mechanical force. Due to this mechanical force, or torque, the rotor starts to rotate. The direction of this force is given by Fleming left hand rule.

When fed with AC supply, it still produces unidirectional torque. Because, armature winding and field winding are connected in series, they are in same phase. Hence as polarity of AC changes periodically, the direction of current in armature and field winding reverses at the same time. Thus, direction of magnetic field and the direction of armature current reverses in such a way that the direction of force experienced by armature conductors remains same. Thus, regardless of AC or DC supply, universal motor works on the same principle that DC series motor.

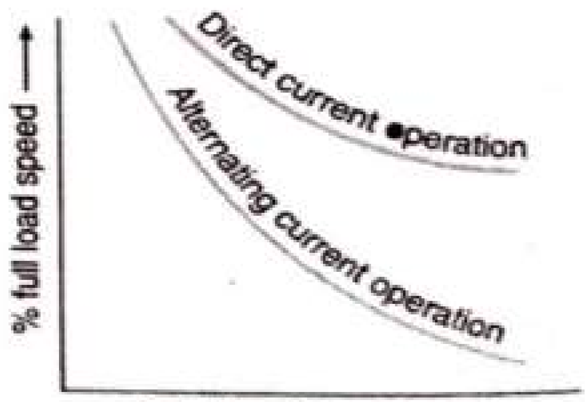
Reversal of Direction of Rotation:

The direction of rotation can be changed by interchanging connections to the field with respect to the armature as in a d.c. series motor.

Speed-Torque Characteristics:

Speed/torque characteristics of a universal motor is similar to that of DC series motor.

(i) The speed of universal motor is low at full load and very high at no load.
(ii) The motor torque is high for large armature current giving high starting torque.
(iii) At Full load, the PF is about 90%
(iv) Most of the universal motors are designed to operate at higher speeds, exceeding 3500 RPM.
(v) Universal motor may be built to operate satisfactorily either 50 Hz a.c. or direct current, at 115 or 230 volts d.c.



Advantages of Universal Motor:

1. It is small in size.
2. Less expensive.
3. High speed from 3600 rpm to 25000 rpm
4. High torque at low and intermediate speeds.
5. Higher power output.

Disadvantages:

1. Poor commutation on a.c operation.
2. Motor become noisy at high speeds.
3. Requirement for careful balancing to avoid vibrations.

Applications:

Due to the good starting torque, high efficiency and speed, these motors suitable tor following applications.

1. Universal motors find their use in various home appliances like vacuum cleaners, drink and food mixtures, domestic sewing machine and hair dryers.
2. The higher rating universal motors used in portable drills, blenders etc.
3. Used in portable toys, hand tools, electric typewriters, cameras and electric shavers etc.

REPULSION MOTOR:

A repulsion motor is similar to an a.c. series motor except that

(i) Brushes are not connected to supply but are short-circuited. Consequently, currents are induced in the armature conductors by transformer action.

(ii) The field structure has non-salient pole construction.

By adjusting the position of short-circuited brushes on the commutator, the starting torque can be developed in the motor.

Construction:

- The field of stator winding is wound like the main winding of a split-phase motor and is connected directly to a single-phase source.
- The armature or rotor is similar to a d. c. motor armature with drum type winding connected to a commutator.
- The brushes are not connected to supply but are connected to each other or short-circuited. Short-circuiting the brushes effectively makes the rotor into a type of squirrel cage.
- By using a commutator motor with brushes short-circuited, it is possible to vary the starting torque by changing the brush axis. It has also better power factor than the conventional single-phase motor.

Principle of operation:

Let us consider a two-pole repulsion motor with its two short-circuited brushes shown in figure below.

i. In Fig.(i), the brush axis is parallel to the stator field. When the stator winding is energized from single-phase supply, e.m.f. is induced in the armature conductors (rotor) by induction. By Lenz's law, the direction of the e.m.f. is such that the magnetic effect of the resulting armature currents will oppose the increase in flux. With the brush axis in the position, current will flow from brush B to brush A where it enters the armature and flows back to brush B through the two paths ACB and ADB. With brushes set in this position, half of the armature conductors under the N-pole carry current inward and half carry current outward and similar under S-pole. Therefore, as much torque is developed in one direction as in the other and the armature remains stationary. The armature will also remain stationary if the brush axis is perpendicular to the stator field axis. It is because even then net torque is zero.

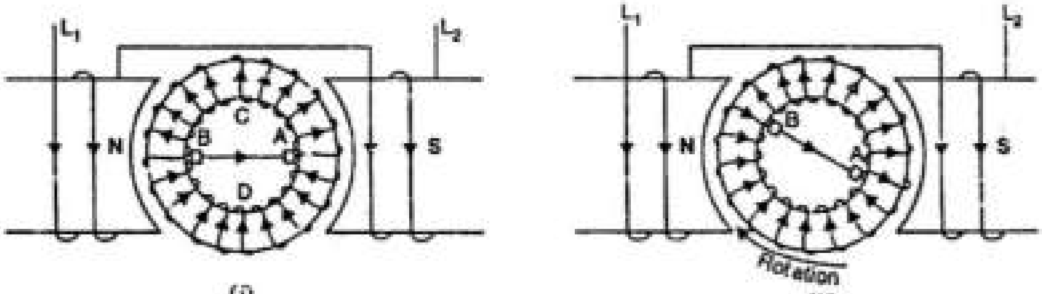
ii. If the brush axis is at some angle other than 0° or 90° to the axis of the stator field, a net torque is developed on the rotor and the rotor accelerates to its final speed shown in Fig.(ii). The brushes have been shifted clockwise through some angle from the stator field axis. Now e.m.f. is still induced in the direction and current flows through the two paths of the armature winding from brush B to brush A. Because of the new brush positions, the greater part of the conductors under the N pole carry current in one direction while the greater part of conductors under S-pole carry current in the opposite direction. With brushes in the position torque is developed in the clockwise direction and the rotor quickly attains the final speed.

iii. The total armature torque in a repulsion motor can be

$$T_a \propto sin2\alpha$$

where α= angle between brush axis and stator field axis

For maximum torque, 2α= 90° or α = 45°



(i) (ii)

Reversal of Direction of Rotation:

- The direction of rotation of the rotor depends upon the direction in which the brushes are shifted. If the brushes are shifted in clockwise direction from the stator field axis, the net torque acts in the clockwise direction and the rotor accelerates in the clockwise direction.
- If the brushes are shifted in anti-clockwise direction the armature current under the pole faces is reversed and the net torque is developed in the anti-clockwise direction.

Thus a repulsion motor may be made to rotate in either direction depending upon the direction in which the brushes are shifted.

Characteristics:

(i) The repulsion motor has characteristics very similar to those of an a.c. series motor i.e., it has a high starting torque and a high speed at no load.

(ii) The speed which the repulsion motor develops for any given load will depend upon the position of the brushes.

(iii) In comparison with other single-phase motors, the repulsion motor has a high starring torque and relatively low starting current.

REPULSION-START INDUCTION-RUN MOTOR:

The action of a repulsion motor is combined with that of a single phase induction motor to produce repulsion-start induction-run motor. The machine is started as a repulsion motor with a corresponding high starting torque but after it reaches 75% of its full speed, a centrifugal device short-circuits the commutator so that the machine then operates as a single-phase induction motor.

The repulsion-start induction-run motor has the same general construction of a repulsion motor. The only difference is that in addition to the basic repulsion motor construction, it is equipped with a centrifugal device fitted on the armature shaft. When the motor reaches 75% of its full speed, the centrifugal device forces a short-circuiting ring to come in contact with the inner surface of the commutator. This short-circuits all the commutator bars. The rotor then resembles squirrel-cage type and the motor runs as a single-phase induction motor. At the same time, the centrifugal device raises the brushes from the commutator which reduces the wear of the brushes and commutator as well as makes the operation quiet.

Characteristics:

(i) The starting torque is 2.5 to 4.5 times the full-load torque and the starting current is 3.75 times the full-load value.

(ii) Due to their high starting torque, repulsion-motors were used to operate devices such as refrigerators, pumps, compressors, grinding devices,floor-polishing etc.

REPULSION-INDUCTION MOTOR:

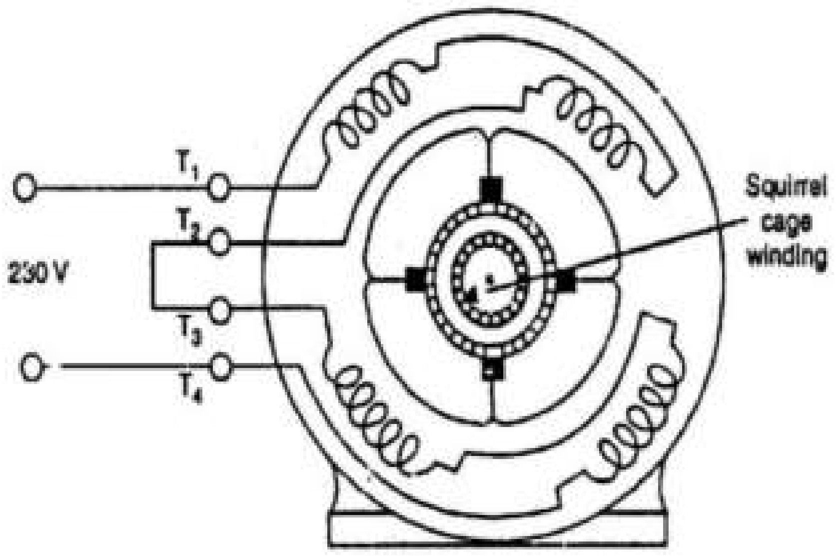
The repulsion-induction motor produces a high starting torque entirely due to repulsion motor action. When running, it functions through a combination of induction-motor and repulsion motor action.

Construction:

It consists of a stator and a rotor (or armature).

(i) The stator carries a single distributed winding fed from single-phase supply.

(ii) The rotor is provided with two independent windings placed one inside the other. The inner winding is a squirrel-cage winding with rotor bars permanently short-circuited. Placed over the squirrel cage winding is a repulsion commutator armature winding. The repulsion winding is connected to a commutator on which ride short-circuited brushes. There is no centrifugal device and the repulsion winding functions at all times.



Operation:

(i) When single-phase supply is given to the stator winding, the repulsion winding (i.e., outer winding) is active. Consequently, the motor starts as a repulsion motor with a corresponding high starting torque.

(ii) As the motor speed increases, the current shifts from the outer to inner winding due to the decreasing impedance of the inner winding with increasing speed. Consequently, at running speed, the squirrel cage winding carries the greater part of rotor current. This shifting of repulsion motor action to induction-motor action is thus achieved without any switching arrangement.

(iii) The motor starts as a repulsion motor. When running, it functions through a combination of principle of induction and repulsion; the former being predominant.

Characteristics:

(i) The no-load speed of a repulsion-induction motor is somewhat above the synchronous speed because of the effect of repulsion winding. However, the speed at full-load is slightly less than the synchronous speed as in an induction motor.

(ii) The speed regulation of the motor is about 6%.

(iii) The starting torque is 2.25 to 3 times the full-load torque; the lower value being for large motors. The starting current is 3 to 4 times the full-load current.

Applications:

This type of motor is used for applications requiring a high starting torque with essentially a constant running speed. Its field of application includes house-hold refrigerators, garage air pumps, petrol pumps, compressors, machine tools, mixing machines, lifts and hoists etc. The common sizes are 0.25 to 5 H.P.

CHAPTER-6
SPECIAL ELECTRICAL MACHINE

Stepper Motor:

These motors are also called stepping motors or step motors. The name stepper is used because this motor rotates through a fixed angular step in response to each input current pulse received by its controller. they can be controlled directly by computers, microprocessors and programmable controllers.

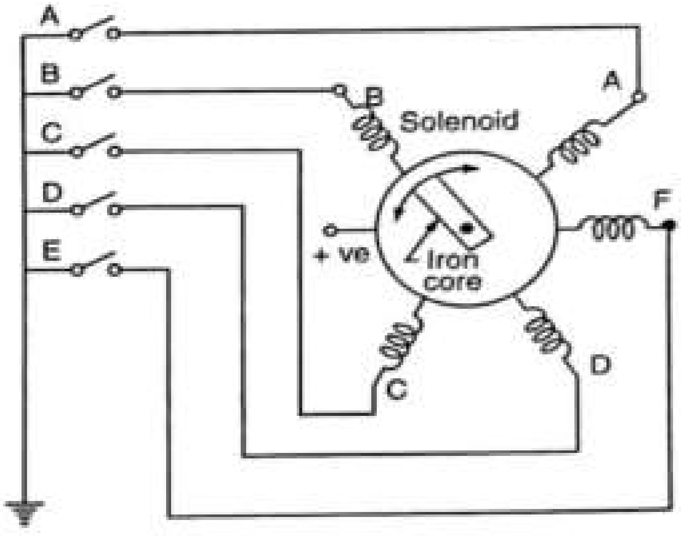
The stepper motor rotates in discrete step angles. Its output shaft rotates in a series of discrete angular intervals or steps, one step being taken each time a command pulse is received. When a definite number of pulses are supplied, the shaft turns through a definite known angle. This makes the motor well-suited for open-loop position control because no feedback need be taken from the output shaft.

Stepping motors are ideally suited for situations where either precise positioning or precise speed control or both are required in automation systems. Such motors develop torques ranging from 1 μN-m (in a tiny wrist watch motor of 3 mm diameter) up to 40 N-m in a motor of 15 cm diameter suitable for machine tool applications. Their power output ranges from about 1 W to a maximum of 2500 W.

The only moving part in a stepping motor is its rotor which has no windings, commutator or brushes. This makes the motor quite robust and reliable. Absence of brushes and commutator makes the operation of stepper motor free from noise.

Principle of Operation:

Steeper motors work on the principle of electro-magnetism. A series of electromagnets arranged in a circle are energised in sequence by the train of pulses. The magneto-motive force developed in them and interact with the rotor (iron piece) and cause it to turn in clockwise or anticlockwise direction depending upon the energised electromagnet position.



Advantages:

1. Low cost.
2. Small in size.
3. It is available in wide range of step angles i.e. from 1.8° to 90°.
4. Excellent torque at low speeds.
5. Low maintenance (brushless).
6. The starting current is low.
7. Excellent for precise positioning control.
8. It has low speed without reduction gears.

Disadvantages:

1. Overall efficiency is low
2. Limited size available
3. Torque decreases with speed

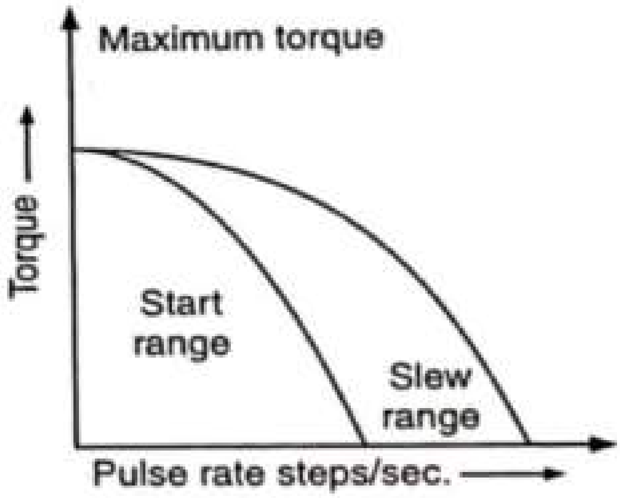
Applications of Stepper Motor:

Such motors are used for

1. Operation control in computer peripherals.
2. In textile industry
3. IC fabrications and robotics etc
4. For incremental motion such as typewriter, line printers, tape drives, floppy disk drivers.
5. For numerical controlled machine tools, process controls system and X-Y plotters.
6. It is also used in commercial, military and medical purpose. In such cases it performs the function like mixing, cutting, striking etc.
7. They also take part in the manufacture of packed food stuffs etc.
8. As the motor speed is proportional to rate of common pulses, it can be used for speed control.

Characteristics of Stepper Motor:

- As the stepping rate is increased, the motor can provide less torque because the rotor has less time to drive the load from one position to the next position.
- The start range is that in which load position follows the pulse without losing steps. Slew range is that in which the load velocity follows the pulse rate without losing steps but cannot start or reverse on signal. The maximum torque point is the point at which the torque is maximum.
- If the stepping rate is increased too quickly, the motor loses synchronism and stops. If when the motor is slewing, command pulses are suddenly stopped instead of being progressively slowed.
- When the pulse rate is high, the shaft rotation seems continuous. Operation at high speeds is called 'slewing'.



Torque pulse rate characteristics of stepper motor

Definition related to Stepper Motor:

1. Step Angle:

The angle through which the motor shaft rotates for each command pulse is called the step angle. Smaller the step angle, greater the number of steps per revolution and higher the resolution or accuracy of positioning obtained. The step angles can be as small as 0.72° or as large as 90°. But the most common step sizes are 1.8°. 2.5°. 7.5° and 15°. Step angle can be measured in terms of angular displacement of rotor shaft. It is denoted by β.

The value of step angle can be expressed either in terms of the rotor and stator poles (teeth) N_r and N_s respectively or in terms of the number of stator phases (m) and the number of rotor pole (teeth).

$$\beta = \frac{N_s - N_r}{N_s N_r} \times 360°$$

Or $$\beta = \frac{360°}{m \times N_r} = \frac{360°}{No.of\ Stator\ phases \times No.of\ rotor\ poles}$$

2. Resolution:

Resolution is defined as the number of steps needed to complete one revolution of the rotor shaft. Higher the resolution, greater the accuracy of positioning of objects by the motor.

Resolution= Number of steps per revolution = $\frac{360°}{\beta}$

3. Pulse frequency resolution:

If f is the stepping frequency (or pulse rate) in pulses per second (pps) and β is the step angle, then motor shaft speed is given by

$$n = \frac{\beta \times f}{360°}\ rps\ = pulse\ frequency\ resolution$$

Types of Stepper Motors:

The stepper motor can be classified depending upon the type of rotor. The following are main types of stepper motor.

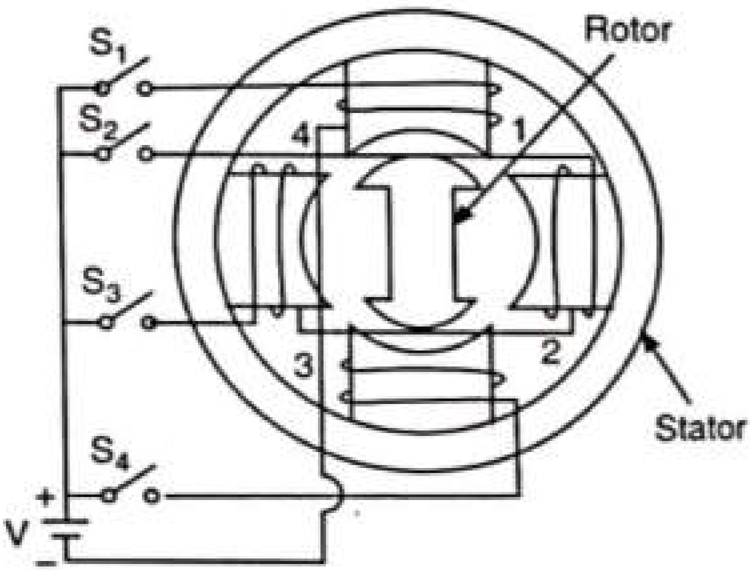
1. Variable Reluctance (VR) stepper motor
2. Permanent magnet (PM) stepper motor
3. Hybrid stepper motor.

Variable Reluctance (VR) stepper motor:

Construction: A variable reluctance stepper motor has no permanent magnet on the rotor. The rotor is made of ferromagnetic materials having teeth (pole) on the outer periphery to obtain variable reluctance is called variable reluctance motor.

A variable reluctance stepper motor has salient pole on the stator. The stator having slots in which multiple multiphase winding is placed.

The rotor is made of soft iron material and carries no windings.



Four phase 4/2 pole variable reluctance motor

Working: When the stator windings are excited in a proper sequence from d.c. supply with the help of switches, a magnetic field is produced. It occupies the position where the reluctance is minimum. Therefore the rotor axis aligns itself to the stator field axis.

When winding no.1 excited, the rotor aligns with the axis of phase 1. The rotor is stable in this position, untill phase no.1 is de-energised. Next phase no. 2 excited and no. 1 is disconnected. The rotor moves through one step 90° in the clockwise direction.

Further phase 3 is excited and phase 2 is disconnected. The rotor is again moves through 90° in clockwise direction.

Thus on exciting the phases in sequence 1,2,3,4 & 1. The rotor moves through a step of 90° in clockwise direction at each transition. Therefore the rotor completes one revolution in four steps. The direction of rotation can be reverse by reversing the sequence of switching i.e., 1,4,3,2,1. The direction of rotation is also independent of direction of current through the phases.

Summary: Variable stepper motor

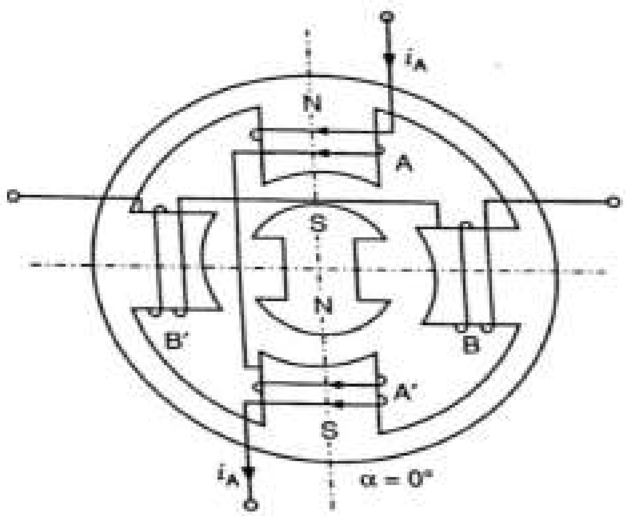
1. The rotor is a soft iron cylinder with salient poles.
2. This the most in expensive stepper motor.
3. Large step angle.
4. A lead screw is often mounted to the shaft for linear stepping motion.

Permanent magnet (PM) stepper motor:

Construction: In Permanent stepper motor the stator is similar to variable reluctance motor but the rotor is made of permanent magnet of ferrite having even number of poles. The stator has projecting poles but rotor is cylindrical and radially magnetized permanent magnets.

The end connections of the winding are taken out to the terminal box for d.c. excitations. The rotor is cylindrical consisting of even number of poles made of high retentivity.

The rotor poles align with the stator poles depending on the excitation of the winding.



Two phase 4/2 pole permanent magnet stepper motor

Working: The two coils A-A' are connected in series to form phase A winding the two coils B-B' connected in series form phase B winding. When winding B is energized by the exciting current and A does not carry any current the rotor moves by step of 90° in clockwise direction. Now if winding A is energised and B does not carry any current, the rotor moves further by step of 90° in clockwise direction. For further movement of 90° the winding A is energised and so on.

To get rotation in anticlockwise direction the sequence of the stator winding in changed. Winding, A is energised first and then winding B and so on.

Truth table Phase

Cycle	A	B	Position $\alpha°$
+	1	0	0
	0	1	90°
-	1	0	180°
	0	1	270°
+	1	0	360°

Advantages of Permanent Magnet Stepper Motor:

1. Permanent magnet stepper motor do not require any external exciting current.
2. Power consumption is low.
3. It has high starting torque as compared to variable reluctance stepper motor.

Disadvantages:

1. It has slower acceleration.
2. It is difficult to manufacture small permanent stepper motor with large number of poles.
3. It has high inertia.
4. Step size of such motors is relatively large ranging from 30° to 90°

Summary of Permanent Stepper Motor

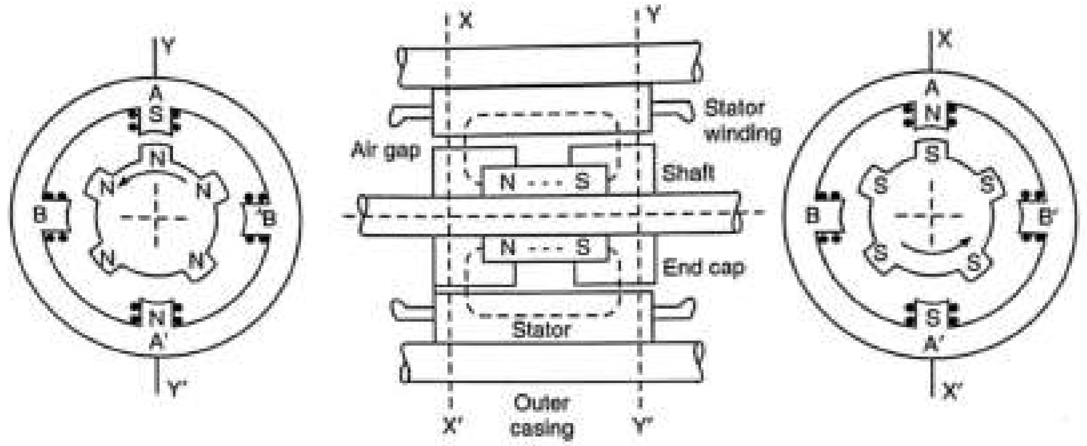
1. The rotor is a permanent magnet, often ferrite magnetized with number of poles.
2. Large to moderate step angle
3. Often used in computer printer to advance paper.

HYBRID STEPPER MOTORS:

A hybrid stepper motor combines the features of variable reluctance motor and permanent magnet stepper motors. The direction of its torque also depends upon the polarity of the stator current. The rotor of such type motor consists of a permanent magnet.

Construction: It is the combination of permanent magnet stepper motor and variable reluctance stepper motor. The rotor consists of a permanent magnet which is magnetized axially to make N and S pole.

Two end-caps are fitted at both ends of this axial magnet. These end-caps consist of equal number of teeth which are magnetized with polarities by the axial magnet.



(a)Cross-section YY′ (b)Axial view (c)Cross-section XX′

Working: Phase A is excited in such a fashion that the top portion of stator pole is a S-pole so that it attracts the N-pole of the rotor and brings it in line with the A - A' axis. Further to turn to rotor phase A is de-energized and phase B is excited positively. The rotor will turn in clockwise (CW) direction by a full step of 18° $\left((5-4)\times\frac{360°}{5\times4}\right)$.

Next, phase A and B are energized negatively one after the other to produce further rotation of 18° each in the same direction.

The hybrid stepping motors are built with more rotor poles than shown in order to give higher angular resolution.

As compared to variable reluctance motor, hybrid motor requires less excitation to achieve a given torque.

Advantages of Hybrid Stepper Motors:

The main advantages of hybrid stepper motors as compared with variable reluctance stepper motors are:

1. It is used where stepping is small (e.g., 1.5°, 2.5°)
2. Higher efficiency at lower speeds.

Disadvantages of Hybrid Stepper Motors:

1. More weight due to the presence of rotor magnet.
2. More costly than variable reluctance stepper motors.

Summary of Hybrid Stepper Motor:

1. The step angle smaller than variable reluctance or permanent magnet steppers motor.
2. The rotor is permanent magnet with fine teeth.
3. The stator windings are divided into not less than two phases.

Comparison between permanent magnet, variable reluctance and hybrid stepper motor:

Sl. No.	Characteristic	Permanent Magnet	Variable Reluctance	Hybrid
1.	Cost	Cheapest	Moderate	Most expensive
2.	Resolution	30° - 3°/step	1.8°/per step	1.8°/per step and smaller
3.	Noise	Quiet	Noisy	Quiet
4.	Design	Moderately complex	Simple	Complex
5.	Stepping	Run in full half and microstepping	Run in full step only	Run in full half and microstepping

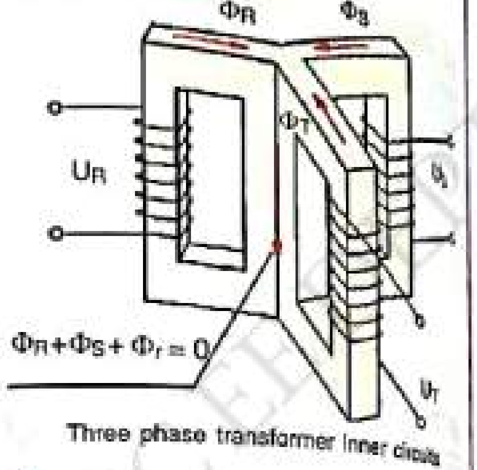
Due to the manufacturing process for the permanent magnet motor it is cheaper. Hybrid and variable reluctance motors are more expensive due to the geared rotor.

Permanent magnet rotors are physically limited by the number of pole pairs. Hybrid and variable reluctance motor have very fine resolution due to the geared construction of the rotor.

However noise of the motor is also taken into consideration. Variable reluctance motors are typically noiser than their permanent magnet or hybrid motor.

33.1. Three-Phase Transformer

Large scale generation of electric power is usually 3-phase at generated voltages of 13.2 kV or somewhat higher. Transmission is generally accomplished at higher voltages of 110, 132, 275, 400 and 750 kV for which purpose 3-phase transformers are necessary to step up the generated voltage to that of the transmission line. Next, at load centres, the transmission voltages are reduced to distribution voltages of 6,600, 4,600 and 2,300 volts. Further, at most of the consumers, the distribution voltages are still reduced to utilization voltages of 440, 220 or 110 volts. Years ago, it was a common practice to use suitably interconnected three single-phase transformers instead of a single 3-phase transformer. But these days, the latter is gaining popularity because of improvement in design and manufacture but principally because of better acquaintance of operating men with the three-phase type. As compared to a bank of single-phase transformers, the main advantages of a 3-phase transformer are that it occupies less floor space for equal rating, weighs less, costs about 15% less and further, that only one unit is to be handled and connected.



Three phase transformer Inner circuits

Like single-phase transformers, the three-phase transformers are also of the core type or shell type. The basic principle of a 3-phase transformer is illustrated in Fig. 33.1 in which only primary windings have been shown interconnected in star and put across 3-phase supply. The three cores are 120° apart and their empty legs are shown in

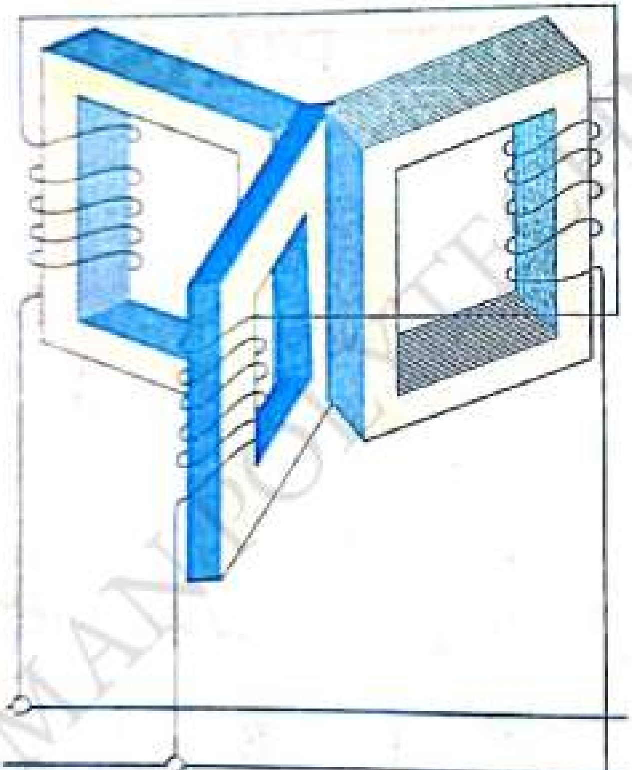


Fig. 33.1

contact with each other. The centre leg, formed by these three, carries the flux produced by the three-phase currents I_R, I_Y and I_B. As at any instant $I_R + I_Y + I_B = 0$, hence the sum of three fluxes is also zero. Therefore, it will make no difference if the common leg is removed. In that case any two legs will act as the return for the third just as in a 3-phase system any two conductors act as the return for the current

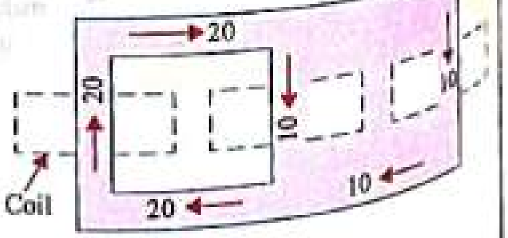


Fig. 33.2 (a)

in the third conductor. This improved design is shown in Fig. 33.2 (*a*) where dotted rectangles indicate the three windings and numbers in the cores and yokes represent the directions and magnitudes of fluxes at a particular instant. It will be seen that at any instant, the amount of 'up' flux in any leg is equal to the sum of 'down' fluxes in the other two legs. The core type transformers are usually wound with circular cylindrical coils.

In a similar way, three single-phase shell type transformers can be combined together to form a 3-phase shell type unit as shown in Fig. 33.2(*b*). But some saving in iron can be achieved in constructing a single 3-phase transformer as shown in Fig. 33.3. It does not differ from three single-phase transformers put side by side. Saving in iron is due to the joint use of the magnetic paths between the coils. The three phases, in this case, are more independent than they are in the core type transformers, because each phase has a magnetic circuit independent of the other.

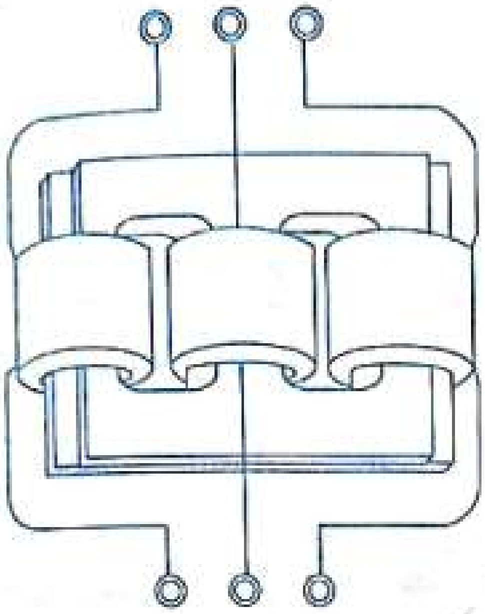


Fig. 33.2 (*b*)

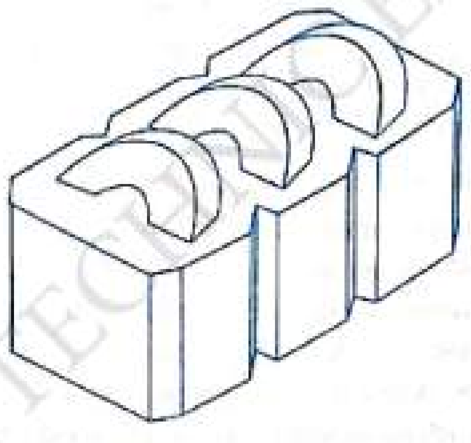
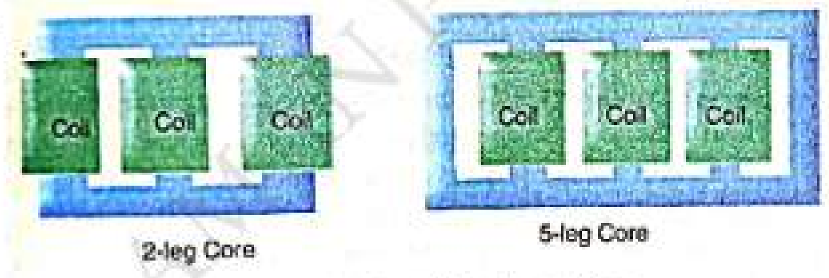
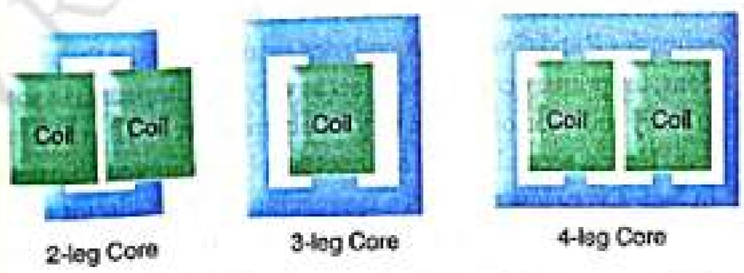


Fig. 33.3



Three-Phase Transformer Cores



Single-Phase Transformer Cores

One main drawback in a 3-phase transformer is that if any one phase becomes disabled, then the whole transformer has to be ordinarily removed from service for repairs (the shell type may be operated open

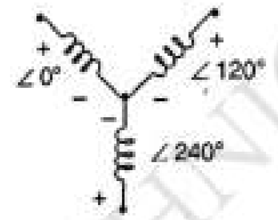
Δ or Vee but this is not always feasible). However, in the case of a 3-phase bank of single-phase transformers, if one transformer goes out of order, the system can still be run open-Δ at reduced capacity or the transformer can be readily replaced by a single spare.

33.2. Three-phase Transformer Connections

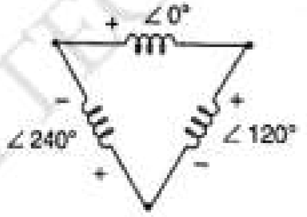
There are various methods available for transforming 3-phase voltages to higher or lower 3-phase voltages *i.e.* for handling a considerable amount of power. The most common connections are (*i*) $Y - Y$ (*ii*) $\Delta - \Delta$ (*iii*) $Y - \Delta$ (*iv*) $\Delta - Y$ (*v*) open-delta or $V - V$ (*vi*) Scott connection or $T - T$ connection.

33.3. Star/Star or Y/Y Connection

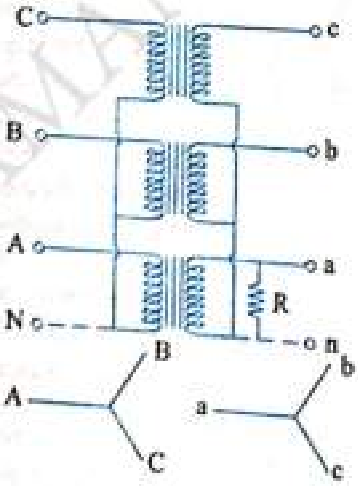
This connection is most economical for small, high-voltage transformers because the number of turns/phase and the amount of insulation required is minimum (as phase voltage is only $1/\sqrt{3}$ of line voltage). In Fig. 33.4 a bank of 3 transformers connected in Y on both the primary and the secondary sides is shown. The ratio of line voltages on the primary and secondary sides is the same as the transformation ratio of each transformer. However, there is a phase shift of 30° between the phase voltages and line voltages both on the primary and secondary sides. Of course, line voltages on both sides as well as primary voltages are respectively in phase with each other. ***This connection works satisfactorily only if the load is balanced.*** With the unbalanced load to the neutral, the neutral point shifts thereby making the three line-to-neutral (*i.e.* phase) voltages unequal. The effect of unbalanced loads can be illustrated by placing a single load between phase (or coil) a and the neutral on the secondary side. The power to the load has to be supplied by primary phase (or coil) A. This primary coil A cannot supply the required power because it is in series with primaries B and C whose secondaries are open. Under these conditions, the primary coils B and C act as very high impedances so that primary coil A can obtain but very little current through them from the line. Hence, secondary coil a cannot supply any appreciable power. In fact, a very low resistance approaching a short-circuit may be connected between point a and the neutral and only a very small amount of current will flow. This, as said above, is due to the reduction of voltage E_{an} because of neutral shift. In other words, under short-circuit conditions, the neutral is pulled too much towards a. This reduces E_{an} but increases E_{bn} and E_{cn} (however line voltages E_{AB}, E_{BC} and E_{CA} are unaffected). On the primary side, E_{A} ...



With these phase angles, the center points of the Y must tie either all "–" or all "+" winding ends together.



With these phase angles, the winding polarities must stack together in a complementary manner (+ to –).



0° Angular Displacement

Fig. 33.4

practically reduced to zero whereas E_{BN} and E_{CN} will rise to nearly full primary line voltage. This difficulty of shifting (or floating) neutral can be obviated by connecting the primary neutral (shown dotted in the figure) back to the generator so that primary coil A can take its required power from between its line and the neutral. It should be noted that if a single phase load is connected between the lines a and b, there will be a similar but less pronounced neutral shift which results in an overvoltage on one or more transformers.

Another advantage of stabilizing the primary neutral by connecting it to neutral of the generator is that it eliminates distortion in the secondary phase voltages. This is explained as follows. For delivering a sine wave of voltage, it is necessary to have a sine wave of flux in the core, but on account of the characteristics of iron, a sine wave of flux requires a third harmonic component in the exciting current. As the frequency of this component is thrice the frequency of the circuit, at any given instant, it tends to flow either towards or away from the neutral point in all the three transformers. If the primary neutral is isolated, the triple frequency current cannot flow. Hence, the flux in the core cannot be a sine wave and so the voltages are distorted. But if the primary neutral is earthed *i.e.* joined to the generator neutral, then this provides a path for the triple-frequency currents and e.m.fs. and the difficulty is overcome. Another way of avoiding this trouble of oscillating neutral is to provide each of the transformers with a third or tertiary winding of relatively low kVA rating. This tertiary winding is connected in Δ and provides a circuit in which the triple-frequency component of the magnetising current can flow (with an isolated neutral, it could not). In that case, a sine wave of voltage applied to the primary will result in a sine wave of phase voltage in the secondary. As said above, the advantage of this connection is that insulation is stressed only to the extent of line to neutral voltage *i.e.* 58% of the line voltage.

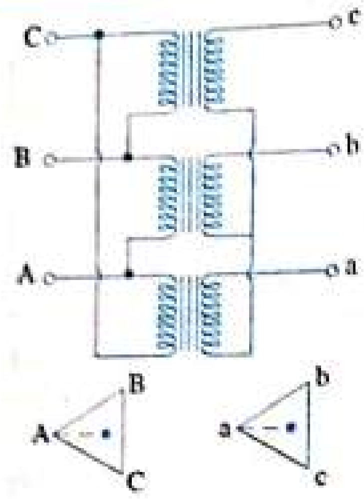
33.4. Delta-Delta or $\Delta - \Delta$ Connection

This connection is economical for large, low-voltage transformers in which insulation problem is not so urgent, because it increases the number of turns/phase. The transformer connections and voltage triangles are shown in Fig. 33.5. The ratio of transformation between primary and secondary line voltage is exactly the same as that of each transformer. Further, the secondary voltage triangle *abc* occupies the same relative position as the primary voltage triangle *ABC* *i.e.* there is no angular displacement between the two. Moreover, there is no internal phase shift between phase and line voltages on either side as was the case in $Y - Y$ connection. This connection has the following advantages :

1. As explained above, in order that the output voltage be sinusoidal, it is necessary that the magnetising current of the transformer must contain a third harmonic component. In this case, the third harmonic component of the magnetising current can flow in the Δ-connected transformer primaries without flowing in the line wires. The three phases are 120° apart which is $3 \times 120 = 360°$ with respect to the third harmonic, hence it merely circulates in the Δ. Therefore, the flux is sinusoidal which results in sinusoidal voltages.

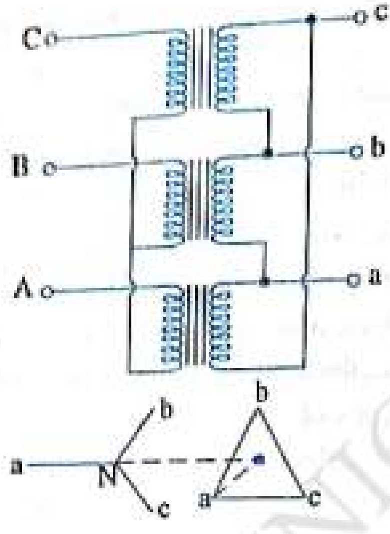
2. No difficulty is experienced from unbalanced loading as was the case in $Y - Y$ connection. The three-phase voltages remain practically constant regardless of load imbalance.

3. An added advantage of this connection is that if one transformer becomes disabled, the system can continue to operate in open-delta or in $V - V$ although with reduced available capacity. The reduced capacity is 58% and not 66.7% of the normal value, as explained in Art. 33.7.



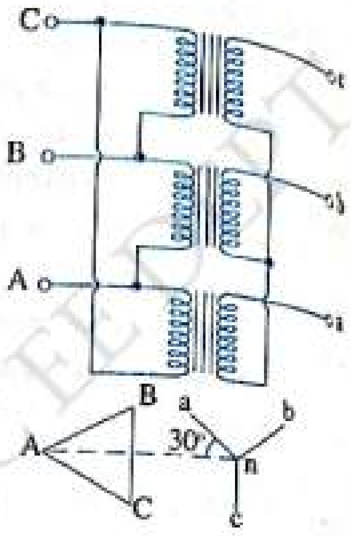
0° Angular Displacement

Fig. 33.5



30° Angular Displacement

Fig. 33.6



30° Angular Displacement

Fig. 33.7

33.5. Wye/Delta or Y/Δ Connection

The main use of this connection is at the substation end of the transmission line where the voltage is to be stepped down. The primary winding is Y-connected with grounded neutral as shown in Fig. 33.6. The ratio between the secondary and primary line voltage is $1/\sqrt{3}$ times the transformation ratio of each transformer. There is a 30° shift between the primary and secondary line voltages which means that a $Y-\Delta$ transformer bank cannot be paralleled with either a $Y-Y$ or a $\Delta-\Delta$ bank. Also, third harmonic currents flows in the Δ to provide a sinusoidal flux.

33.6. Delta/Wye or Δ/Y Connection

This connection is generally employed where it is necessary to step up the voltage as for example, at the beginning of high tension transmission system. The connection is shown in Fig. 33.7. The neutral of the secondary is grounded for providing 3-phase 4-wire service. In recent years, this connection has gained considerable popularity because it can be used to serve both the 3-phase power equipment and single-phase lighting circuits.

This connection is not open to the objection of a floating neutral and voltage distortion because the existence of a Δ-connection allows a path for the third-harmonic currents. It would be observed that the primary and secondary line voltages and line currents are out of phase with each other by 30°. Because of this 30° shift, it is impossible to parallel such a bank with a $\Delta - \Delta$ or $Y - Y$ bank of transformers even though the voltage ratios are correctly adjusted. The ratio of secondary to primary voltage is $\sqrt{3}$ times the transformation ratio of each transformer.

33.11. Parallel Operation of 3-phase Transformers

All the conditions which apply to the parallel operation of single-phase transformers also apply to the parallel running of 3-phase transformers but with the following additions :

1. The voltage ratio must refer to the terminal *voltage of primary and secondary*. It is obvious that this ratio may not be equal to the ratio of the number of turns per phase. For example, if V_1, V_2 are the primary and secondary terminal voltages, then for Y/Δ connection, the turn ratio is $V_2/(V_1/\sqrt{3}) = \sqrt{3}V_2/V_1$.

2. The phase displacement between primary and secondary voltages must be the same for all transformers which are to be connected for parallel operation.

3. The phase sequence must be the same.

4. All three transformers in the 3-phase transformer bank will be of the same construction either core or shell.

Note. (*i*) In dealing with 3-phase transformers, calculations are made for one phase only. The value of equivalent impedance used is the equivalent impedance per phase referred to secondary.

(*ii*) In case the impedances of primary and secondary windings are given separately, then primary impedance must be referred to secondary by multiplying it with (transformation ratio)^2.

(*iii*) For Y/Δ or Δ/Y transformers, it should be remembered that the voltage ratios as given in the questions, refer to terminal voltages and are quite different from turn ratio.

TRANSFORMER TAP CHANGER

A tap changer is a device fitted to power transformers for regulation of the output voltage to required levels. This is normally achieved by changing the ratios of the transformers on the system by altering the number of turns in one winding of the appropriate transformer/s. Supply authorities are under obligation to their customers to maintain the supply voltage between certain limits. Tap changers offer variable control to keep the supply voltage within these limits. About 96% of all power transformers today above 10MVA incorporate on load tap changers as a means of voltage regulation.

Tap changers can be on load or off load. On load tap changers generally consist of a diverter switch and a selector switch operating as a unit to effect transfer current from one voltage tap to the next. It was more than 60 years ago on load tap changers were introduced to power transformers as a means of on load voltage control.

Tap changers possess two fundamental features:

(a) Some form of impedance is present to prevent short circuiting of the tapped section,

(b) A duplicate circuit is provided so that the load current can be carried by one circuit whilst switching is being carried out on the other.

The impedance mentioned above can either be resistive or reactive. The tap changer with a resistive type of impedance uses high speed switching, whereas the reactive type uses slow moving switching. High speed resistor switching is now the most popular method used worldwide, and hence it is the method that is reviewed in this report.

The tapped portion of the winding may be located at one of the following locations, depending upon the type of winding:

(a) At the line end of the winding;

(b) In the middle of the winding;

(c) At the star point.

The most common type of arrangements is the last two. This is because they give the least electrical stress between the tap changer and earth; along with subjecting the tapings to less physical and electrical stress from fault currents entering the line terminals. At lower voltages the tap changer may be located at either the low voltage or high voltage windings.

Tap changers can be connected to the primary or secondary side windings of the transformer depending on:

- Current rating of the transformer
- Insulation levels present

- Type of winding within the transformer (eg. Star, delta or autotransformer)
- Position of tap changer in the winding
- Losses associated with different tap changer configurations eg. Coarse tap or reverse winding
- Step voltage and circulating currents
- Cost
- Physical size on-load tap changer

The Consequences Of Transformer Failure

Transformers are one of the more expensive pieces of equipment used in a power system, and the potential consequences of failure can be quite damaging. This has been shown in the past with the political and media attention surrounding blackouts at various locations around the world. Within Australia and New Zealand, the largest cost transformer failures have occurred due to internal winding faults, faulty load tap changers, and failed winding accessories respectively.

Failure of winding accessories includes loose coil clamping bolts, together with internal winding faults and faulty tap changers. These failures affected on average ten transformers per year during the period 1975 to 1995, incurring repair costs of at least $600,000 per year, together with other associated costs. For example, with several elements drawn from an Australian case study and through discussion with engineers at Pacific Power's Advanced Technical Center, the cost of a generator unit transformer failing has been conservatively estimated at $5.4M. This figure was considered conservative because there are many other factors that could be added on to this figure that are difficult to determine. It is interesting to note the root of these failures appear to have been predominantly design and manufacturing flaws.

Current Maintenance Strategies of Transformer Tap Changers

During the past years and after a number of visits, meetings, lectures and training courses, the conclusion has been reached that proper organization and execution of OLTC maintenance is found only in very few cases.

The frequency of maintenance to on load tap changers is dependent on the condition of the diverter switch and the necessity to maintain the motor drive unit. Maintenance of the diverter switch should be carried out on a cyclic basis, but on transformers where frequency of tap change is high, maintenance may be necessary before the cyclic maintenance becomes due. A certain period should not be exceeded between inspections. When considering inspection periods, serious consideration should be given to the breaking of circulating current which in some cases may exceed the load current.

The diverter switch and tap selector is the only internal moving parts in a transformer. The diverter switch does the entire on load making and breaking of currents, whereas the tap selector preselects the tap to which the diverter switch will transfer the load current. The tap selector operates off load and therefore needs no maintenance. However experience has shown that in some circumstances inspection of selector switches becomes necessary where contacts become misaligned or contact braids in fact fatigueandbreak.

The next segment is a list taken from on what should be carried out during tap changer maintenance;

- Replace contacts in older type tap changers. Modern tap changers rarely require contact replacement; this depends on the characteristics of the tap changer in question. The frequency of diverter switch and motor drive unit inspections can usually be obtained from manufacturer manuals or previous maintenance experience.

- Measuring and recording contact consumption during inspection will give a reasonably accurate life expectancy of the contacts at that present load condition. Therefore this should be done on a regular basis.

- Transition resistors should be checked for continuity and value as an open circuited resistor can result in excessive contact wear.

- Need to equalize rotation lag between the diverter switch and the motor drive unit to ensure minimum spring energisation in the energy accumulator springs.

- The function of relays, interlocks, limit switches and switches should be checked as well as remote indication of tap position.

- Drive shafts and gearboxes must be inspected for radial and axial wear. A large percentage of tap change failures are as a result of drive shaft faults.

- Replace transformer oil with clean, dry oil. Cleaning is only carried out with transformer oil not solvents. Carbon and copper deposits are generally found on horizontal surfaces of the diverter switch as small convection currents in the oil are established each tap change. This results in the carbon being deposited on top of the diverter.

Source: http://mediatoget.blogspot.in/2012/01/transformer-tap-changer.html

MAINTENANCE INSTRUCTIONS FOR POWER TRANSFORMERS

Maintenance Schedule

Sl No	Inspection frequency	Items to be inspected	To be checked	Action required if inspection shows unsatisfactory conditions
1	Hourly	Ambient temperature		
2	Hourly	Winding temperature	Ensure that temperature rise is within specified limits.	
3	Hourly	Oil temperature		
4	Hourly	Load (amps)	Check against rated figures given on the name plate	
5	Hourly	Voltage		
6	Daily	Oil level in transformer	Check oil level gauge	If low, top with dry oil find whether there is any leak.
7	Daily	Oil level in bushing	--	--
8	Daily	Dehydrating breather	Check that air passages are free. Check colour of active agent	If silicagel is pink, change by new charge. The old charge may be reactivated for using again.
9	Daily	Oil level in OLTC conservator	Check oil sight window or oil level gauge	If low, top with new dry oil

Sl No	Inspection frequency	Items to be inspected	To be checked	Action required if inspection shows unsatisfactory conditions
10	Daily	Relief diaphragm of OLTC explosion vent	--	Replace if cracked or broken
11	Daily	Cooler fan, bearing motor & operating mechanism	Check the bearings. Examine contacts, check manual control and interlock	Lubricate the bearing. Replace burnt or worn contacts.
12	Quarterly	Bushings	Examine for cracks and dirt deposit	Clean the dirt. If cracked or broken replace the bushing.
13	Quarterly	Oil in transformer	Check for dielectric strength and water content	Take suitable action to restore quality of oil.
14	Half yearly or at the end of 5000 operations	Oil in the diverter switch of OLTC	a. Dielectric strength	Filter or replace if BDV is less than specified value.
			b. Water content	Measure the water content using KARL FISHER method. Replace/ recondition if exceeds that limits specified
15	Yearly	Oil in transformer	Check acidity resistivity, tan delta and sludge	Filter or replace
16	Yearly	Oil filled condenser bushing	Refer to the maintenance schedule for OIP condenser bushings	As recommended
17	Yearly	Gasket joints		Tighten the bolts evenly to avoid uneven pressure

Sl No	Inspection frequency	Items to be inspected	To be checked	Action required if inspection shows unsatisfactory conditions
18	Yearly	Cable boxes	Check sealing arrangements and find out whether there is any leak	Replace gasket if leaking
19	Yearly	Relays alarm and other circuits	Examine relay and alarm contacts, their operation fuses etc. check relay accuracy.	Clean the components. Replace contacts and fuse if necessary
20	Yearly	Painting	Rusting/colour	Touch up to be done
21	Yearly	Earth resistance	--	Take suitable action if earth resistance is high
22	After 50000 operations of the OLTC	Arcing contacts	--	Replace if necessary
23	-do-	Lubricating oil in the gear box of driving mechanism	Low oil level	Add or replace with lubricating oil
24	5 yearly	1000 kVA to 2000 kVA	Overall inspection including core and coil	Wash the core and coils with clean oil
	7 – 10 yearly	above 3000 kVA		

Note :

In case of abnormal phenomena occurring during service, inform the manufacturer the exact nature of the phenomena together with the name plate particulars for easy identification.

5^{TH} SEM./ ELECTRICAL/2020(W)OLD

EET 501-ENERGY CONVERSION II

Full Marks: 80 Time: 3 Hours

Answer any Five Questions including Q No. 1& 2

Figures in the right hand margin indicates marks

1. **Answer all the questions** 10x2

a) Define pitch factor in alternator and state its relation with short pitch angle α.

b) State any two applications of stepper motor.

c) Write any two advantages of polyphase induction motor over AC motors.

d) What is 'up' voltage regulation in alternators?

e) What are the V-curves in synchronous motor?

f) What is hunting and how it can be prevented?

g) How a single phase induction motor is made self starting?

h) What is the function of compensating winding in compensated repulsion motor?

i) How the direction of rotation of split phase induction motor can be reversed?

j) What is the effect of change in supply voltage on Torque and Speed in 3 phase induction motor?

2. **Answer any six questions** 6x5

a) Explain the principle of operation of universal motor with neat diagram.

b) Explain about the determination of voltage regulation of alternator by synchronous impedance method.

c) Derive the torque developed by the 3 phase induction motor at the instant of starting.

d) Describe about the operation of ON load tap changing transformer using resistors.

e) Write a short note on single phase capacitor start capacitor run induction motors.

f) Explain the 2-phase ON mode of operation in variable reluctance stepper motor briefly.

g) Describe the power flow within a 3 phase synchronous motor and find the mechanical power in rotor.

Describe the working principle of shaded pole motor with neat diagrams 10

Explain the double field revolving theory in single phase induction motor with Torque-slip graph. 10

Explain the effect of armature reaction on main flux in alternators at Unity Power Factor, Zero Power Factor lagging and leading loads. 10

Describe the effect of excitation on armature current and power factor in synchronous motor in details. 10

The power input to the rotor of a 440V, 50Hz, 6-pole,3 phase induction motor is 100 kW. The rotor electromotive force is observed to make 120 cycles per minute. Calculate (i) the slip (ii) the rotor speed (iii) mechanical power developed (iv) the rotor copper loss per phase and (v) speed of stator field with respect to rotor. 10

5TH SEM./ ELECTRICAL/2020(W)NEW
TH2-ENERGY CONVERSION II

Full Marks: 80 | Time: 3 Hours

Answer any Five Questions including Q No. 1& 2
Figures in the right hand margin indicates marks

1. Answer all the questions 1
   a) Define slip speed in 3 phase induction motor and state its equation.
   b) What is plugging in 3 phase induction motor?
   c) Define pitch factor in alternator and state its value.
   d) What is the purpose of damper windings in alternators?
   e) State two applications of synchronous motor.
   f) What are the V-curves in synchronous motor?
   g) Define step angle in stepper motor and state its value.
   h) How a single phase induction motor is made self starting?
   i) What is the function of compensated winding in compensated repulsion motor?
   j) How the direction of rotation of split phase induction motor can be reversed?

2. Answer any six questions 6
   a) *Explain the principle of operation of synchronous motor in details.*
   b) *Describe the power flow stages in 3 phase induction motor with a neat diagram.*
   c) *Derive the relation between torque and rotor power factor in 3 phase induction motor.*
   d) Explain about the determination of voltage regulation of alternator by synchronous impedance method.
   e) Describe about types of rotors in alternators in details.
   f) Write a short note on capacitor start induction run motors.
   g) Explain the 1-phase ON or full step operation in variable reluctance stepper motor briefly.

3. Derive the relationship between rotor input, mechanical power & copper loss in 3-ph induction motor.
4. Explain about the double field revolving theory in 1-phase induction motor with torque-slip graph.
5. Describe the synchronizing of 3 phase alternator using two bright and one dark lamp method.
6. Write a short note on (a)Direct-On-Line starter (b)Parallel operation of alternators.
7. Explain the effect of excitation on armature current and power factor in synchronous motor in details.

(*b*) Explain with vector diagram the effect of excitation on armature current and power factor. 6

(*c*) A 2200 V, 373 kW, 3-phase star connected synchronous motor has a resistance of 0.3 ohm and a synchronous reactance of 3.0 ohm per phase respectively. Determine the induced emf per phase if the motor works on full-load with an efficiency of 94% and a p.f. of 0.8 leading. 8

6. (*a*) How the direction of rotation of a capacitor start, induction run single phase motor is changed?

(*b*) Explain split phase motor.

(*c*) Explain single phase series motor.

7. Write short notes on any *two* : 8

(*a*) ON load and OFF load tap changer

(*b*) Starting of sq.cage motor by Star-Delta starter

(*c*) S.C and O.C tests on alternator.

(b) For a 3-phase winding with 4 slots per pole per phase and with coil span of 10 slot pitch, calculate the values of the distribution factor and coil span factor.

(c) A 3-phase, 50 Hz, 8-Pole induction motor has full load slip 4%. The rotor resistance is 0.001Ω per phase and standstill reactance of 0.005 ohm per phase. Find the ratio of maximum to full load torque and the speed at which the maximum torque occurs.

4. (a) Why are induction motors called 'asynchronous'?

(b) A 3-phase induction motor is wound for 4-poles and is supplied from 50 Hz system. Calculate (i) the synchronous speed (ii) the rotor speed when slip is 4% and (iii) rotor frequency when rotor runs at 600 rpm.

(c) A 3-phase, star connected alternator is rated at 1600 kVA, 13,500 V. The armature resistance and synchronous reactance are 1.5 ohm and 30 ohm respectively per phase. Calculate the percentage regulation for a load of 1280 kW at 0.8 leading power factor.

. (a) What factors determine the number of poles of a synchronous motor ?

V/SEM/ELECT/2013(S)-
BP-NEW

ENERGY CONVERSION-II

[Theory-1]

Full Marks : 80

Time : 3 hours

Answer any **five** questions

The figures in the right-hand margin indicate marks

1. (*a*) Which type of alternator is used in Thermal Power Plant ? 2

(*b*) Derive emf equation of Alternator. 6

(*c*) Explain parallel operation of 3-phase alternator by dark and bright lamp method. 8

2. (*a*) What is Percent of Slip ? 2

(*b*) Explain principle of operation induction motor. 6

(*c*) Briefly discuss speed control of induction motor. 8

3. (*a*) What is voltage regulation of an alternator ? 2

(*Turn Over*)

motor.

(*c*) Explain repulsion motor.

7. Write short notes on any *two* :

(*a*) Maintenance of transformer

(*b*) Split phase motor

(*c*) Voltage regulation by synchronous impedanc method

(*d*) Induction generator.

load slip of 4 percent. The rotor resistance is 0·001 ohm per phase and the standstill reactance is 0·005 ohm per phase. Find the ratio of maximum to full load torque. 6

(c) The power input to a 3-phase induction motor is 40 kW. The stator losses total 1kW and the friction and windage losses total 2kW. If the slip of the motor is 4%, find (i) The mechanical power output (ii) the rotor cu loss per phase (iii) efficiency. 8

5. (a) Why damper bars are used in synchronous motor ? 2

(b) Explain principle of operation of synchronous motor with phasor diagram. 6

(c) Explain effect of varying load with constant excitation. 8

6. (a) Write condition of parallel operation of 3-phase transformer. 2

(b) Explain principle of operation of shaded pole

 (Turn Over

3-phase, 8-pole, star connected alternator running at 750 r.pm, flux per pole 55 mWb, no of slots on the armature = 72, number of conductor per slot = 10, k_d = 0·96, assume full pitch coils.

(*c*) A 1200 kVA, 6600 V, 3–phase alternator (star connected) with a resistance of 0·4 ohm and reactance of 6 ohm per phase delivers full load current at p.f. 0·8 lagging and normal rated voltage. Estimate the terminal voltage for the same excitation and load current at 0·8 p.f. leading.

3. (*a*) Define slip of an induction motor.

(*b*) Explain relation between Torque and Slip of induction motor.

(*c*) Explain speed control of induction motor by pole changing with diagram.

4. (*a*) What is the synchronous speed of a 3-phase, 50 Hz, 6 pole induction motor ?

(*b*) A 50 Hz, 8 pole induction motor has a full

V/SEM/ELECT/2013 (W)-OLD

ENERGY CONVERSION-II

[Theory-3]

Full Marks : 80

Time : 3 hours

Answer any **five** questions

The figures in the right-hand margin indicate marks

1. (*a*) What are the advantages of distributed windings? 2

   (*b*) Explain pitch factor and distribution factor. 6

   (*c*) Explain parallel operation of 3-phase alternator. 8

2. (*a*) Why armature winding is placed in the stator for large alternator? 2

   (*b*) Calculate the no load terminal voltage of a

(*Turn Over*

(*c*) Percentage regulation on full load

(*d*) Value of synchronous reactance which replaces armature reaction. $2 \times 4 = 8$

(*i*) Explain the effect of variation of excitation of synchronous motor by means of phasor diagram and draw its V curve. 8

(*ii*) The grouping of a $3-\phi$ transformer are star-star, delta-delta, star-delta and delta-star. Show their connection diagram. 8

Vrite short notes on any *two* of the following : $2 \times 8 = 16$

) Maintenance of power transformer

) Permanent magnet stepper motor

) Speed control of induction motor by any one method

Speed - torque characteristics of a $3-\phi$ induction motor.

(ii) What is parallel operation ? Why it is needed ? State the necessary condition for parallel operation in $3-\phi$ transformer. 6

(iii) For a $3-\phi$ slip ring induction motor, the maximum torque is 2.5 times the full load torque and the starting torque is 1.5 times the full load torque. Determine the percentage reduction in rotor circuit resistance to get a full load slip of 3%. Neglect stator impedance. 8

5. (i) Mention some specific applications of synchronous motor. 2

(ii) Explain why $1-\phi$ induction motor is not self starting. 6

(iii) In a 50 kVA, star connected, 400 V, $3-\phi$, 50 Hz alternator, the effective armature resistance is 0.25 Ω/phase. The synchronous reactance is 3.2 Ω/phase and leakage reactance is 0.5 Ω/phase. Determine at rated load and unity power factor :

(a) Internal emf (Ea)

(b) No load emf

2. (*i*) Write the applications of universal motor. 1×2

(*ii*) Derive the emf equation of an alternator from first principle.

(*iii*) A $3-\phi$, 6600 volts, 50 Hz star connected synchronous motor takes 50 A current. The resistance and synchronous reactance per phase are 1 Ω and 20 Ω respectively. Find the power supplied to the motor and induced emf for a power factor of (*a*) 0.9 lagging (*b*) 0.9 leading. 8

3. (*i*) What is slip in a $3-\phi$ induction motor. 2

(*ii*) Derive the condition for maximum starting torque in a $3-\phi$ induction motor. 6

(*iii*) A $3-\phi$, 10 pole, Y connected alternator runs at 600 rpm. It has 120 stator slots with 8 conductors per slot and the conductors of each phase are connected in series. Determine the phase and line emf's if the flux per pole is 56 mWb. Assume full pitch coils. 8

(*i*) What is voltage regulation ? 2

ENERGY CONVERSION-II

[Theory- 1]

Full Marks : 80

Time : 3 hours

Answer any **five** questions

The figures in the right-hand margin indicate marks

1. (*i*) Why transformer rating is expressed in kVA? 2

(*ii*) Explain with vector diagrams how a rotating field is created by a $3-\phi$ stator winding. 6

(*iii*) A 20 kW, 4 pole, 50 Hz, $3-\phi$ induction motor has friction and windage loss of 3% of the output. The full load speed of the motor is 1440 rpm. Find for full load

(*a*) The rotor copper loss

(*b*) The rotor input

(*c*) Shaft torque

(*d*) Gross electromagnetic torque. $4 \times 2 = 8$

(*Turn Over*)

(*b*) Explain speed control of induction motor by Rotor Rheostatic control method. 5

(*c*) A 500 V, 50 kVA, 1-phase alternator has an effective resistance of 0.2 ohm. A field current of 10A produces an armature current of 200 A on short circuit and an emf of 450 V on open circuit. Calculate the full-load regulation at p.f. 0.8 lag. 9

6. (*a*) When a d.c. series motor is connected to single phase a.c. supply what will happen ? 2

(*b*) Explain Universal motors. 5

(*c*) Explain permanent-magnet stepping motor. 9

7. Write notes on any *two* : 8 × 2

(*a*) Explain tap changer, on load and off load transformer.

(*b*) Repulsion motor.

(*c*) Star-Delta starter with sketch.

(*d*) Parallel operation of 3–phase alternators.

(b) Derive induced emf for alternator. 5

(c) A 4-pole, 50 Hz, 3-phase, Y-connected alternator has a single-layer, full pitch winding with 21 slots per pole and two conductors per slot. The flux per pole 0.6 Wb. The coil span is 150°. Find the r.m.s values of phase emf and line emf. 9

3. (a) What do you mean load angle α in case of synchronous motor ? 2

(b) Explain effect of changing Excitation on constant load. 5

(c) A synchronous motor having 40% reactance and negligible resistance is to be operated at rated load at (i) u.p.f (ii) 0.8 p.f. lag (iii) 0.8 p.f lead. What are the values of induced emf ? Indicate assumptions made if any.. 9

4. (a) Why single phase motor is not self starting ? 2

(b) Explain principle of split-phase induction motor with diagram. 5

(c) Explain double field revolving theory for single phase motors. 9

5. (a) What is slip ? 2

5

V/SEM/ELECTRICAL/2015 (S) BP

ENERGY CONVERSION – II

[Theory – 1]

Full Marks : 80

Time : 3 hours

Answer any **five** questions

The figures in the right-hand margin indicate marks.

1. (*a*) Why rotor slots of a induction motor are not parallel to its shaft but slight skew ? 2

   (*b*) Derive torque of an induction motor under running condition. 5

   (*c*) A 4-pole, 3-phase, 50 Hz induction motor has a voltage between slip-rings on-open-circuit of 520V. The star connected rotor has a standstill reactance and resistance of 2.0 and 0.4 ohm per phase respectively. Determine : (*i*) the full-load torque if full load speed is 1425 r.p.m. (*ii*) the ratio of starting torque to full load torque. (*iii*) the additional rotor resistance required to give maximum torque at standstill. 9

2. (*a*) What is the advantages of open type slot in stator of alternator ? 2

(Turn Ove

(a) What are the types of alternator ?

(b) What is the effect of changing excitation o[n] constant load of a synchronous motor ?

(c) Explain about double field revolving theory.

Write short notes on any *two* : 7

(i) AC series motor

(ii) Shadded pole motor

(iii) Conditions for parallel operation of 3-ϕ transformer.

148 N-m. at it's pulley rim. The Friction and windage losses are 200 W and stator copper and iron loss equal to 1620 W. Calculate (*i*) output power (*ii*) Rotor Copper Loss (*iii*) Efficiency at full load. 7

4. (*a*) What is Damper winding ? 2

(*b*) What do you mean by hunting ? 5

(*c*) Describe about armature reaction of Alternator. 7

5. (*a*) What do you mean by voltage regulation of Alternator ? 2

(*b*) What is the principle of synchronous motor ? 5

(*c*) A 3-ϕ, 50 Hz, star connected 2000 kVA, 2300V Alternator gives a short circuit current of 600 A. For a certain field excitation, with the same excitation the open circuit voltage was 900V. The resistance between a pair of terminal was $0{\cdot}12\Omega$. Find the full load regulation at (*i*) U.P.F. (*ii*) 0·8 lagging. 7

the motor is running, Also calculate the speed at which the torque is maximum and corresponding value of I/P power to the motor, assuming flux remaining constant.

(*a*) What do you mean by plugging ? 2

(*b*) Derive expression for starting torque in case of 3-ϕ induction motor. 5

(*c*) A 8-pole, 50 Hz, 3-ϕ slip ring induction motor has effective rotor resistance of 0·08Ω/ph. Stalling speed is 650 r.p.m, how much resistance must be inserted in the rotor phase to obtain the maximum torque at starting. Ignore the magnetising current and stator leakage impedance. 7

(*a*) What do you mean by distribution factor ? 2

(*b*) What is torque-slip characteristics of 3-ϕ induction motor ? 5

(*c*) A 6-pole, 50 Hz, 3-ϕ induction motor running on full load with 4% slip develop a torque of

 V—Sem/ELECT/2015 (W)

ENERGY CONVERSION-II

(Code : EET-501)

Full Marks : 70

Time : 3 hours

Answer any **five** questions

Figures in the right-hand margin indicate marks

1. (*a*) In which rotor high starting torque is produced and why ? 2

   (*b*) What is the principle of operation of 3-ϕ induction motor ? 5

   (*c*) A 3-ϕ, 4 pole 50 Hz induction motor has a star connected rotor. The voltage of each rotor phase at standstill and on open circuit is 121 V. The rotor resistance per phase is 0·3 Ω and reactance at standstill is 0·8 Ω. If the rotor current is 15A, calculate the speed at which

(*Turn Over*)

7. Write notes on any *two* : 8 × 2

(*i*) Parallel operation of alternator using lamp method

(*ii*) Production of rotating magnetic field

(*iii*) Effect of varying excitation with constant load on synchronous motor

(*iv*) Permanent magnet stepper motor.

(c) A 2300 V, 3-phase, star connected synchronous motor has a resistance of 0·21 ohms per phase and a synchronous reactance of 2·3 ohm per phase. The motor is operating at 0·6 leading p.f. with a line current of 200 A. Determine value of the generated emf per phase. Draw the vector diagram. 8

4. (a) Why skewing is necessary ? 2

(b) Explain capacitor motor with principle. 6

(c) Explain Ferrair's principle, net torque. 8

5. (a) How can a universal motor be reversed ?

(b) Explain speed control of induction motor by pole changing method.

(c) Explain single phase series motor.

6. (a) What do you mean by transformer grouping ?

(b) Explain tap changer on load.

(c) State maintenance of Transformer.

at which the torque is a maximum and the corresponding value of the input power to the motor, assuming the flux to remain constant. 8

2. (a) State different types of slots used in alternator armature. 2

(b) Derive EMF equation of Alternator. 6

(c) A 3-phase, 50 Hz star connected 2000 kVA, 2300 V alternator gives, a short circuit current of 600 A for a certain field excitation. With the same excitation the 0-C voltage was 900 V, the resistance between pair of terminal was 0·12 ohm find full load regulation at (*i*) unit power factor (*ii*) 0·8 lagging power factor. 8

(a) What is the function of damper bar ? 2

(b) Explain the effect of changing load at a constant excitation of a 3-phase synchronous motor. 6

 V—Sem/ELECT/2015(W) (Old)

ENERGY CONVERSION-II

(Theory – 1)

Full Marks : 80

Time : 3 hours

Answer any **five** questions

Figures in the right-hand margin indicate marks

(*a*) State the relationship between rotor frequency and stator frequency of induction motor. 2

(*b*) Derive starting torque of an induction motor. 6

(*c*) A 3-phase, 4-pole, 50 Hz induction motor has a star-connected rotor. The voltage of each rotor phase at standstill and on open circuit is 121 V. The rotor resistance per phase is 0·3 ohm and the reactance at standstill is 0·8 ohm. If the rotor current is 15 A, calculate the speed at which the motor is running. Also calculate the speed

(Turn Over)

(c) What is an universal motor ? How it is different from a dc series motor ? Mention its applications. 7

6. (a) What is the relation between electrical degrees and mechanical angle of an alternator ? 2

(b) Explain the principle and applications of a hybrid stepper motor. 5

(c) A 3-ϕ star-connected synchronous generator driven at 750 rpm is required to generate a line-to-line voltage of 440 V at 50 Hz on open circuit. The stator is wound with 2 slots per pole per phase and each coil has 4 terms. Calculate the useful flux per pole. 7

(a) State the difference between coil pitch and pole pitch. 2

(b) Explain the effect of change of excitation of a synchronous motor driving a constant load. 5

(c) Explain power angle characteristics of cylindrical rotor of synchronous motor. 7

diagram, the effect on power factor with

(*i*) Resistive load

(*ii*) Inductive load

(*iii*) Capacitive load. 7

4. (*a*) What do you mean by an infinite bus ? 2

(*b*) Explain Ferrari's principle for 1-ϕ motor. 5

(*c*) The power input to the rotor of a 440 V, 50 Hz, 6-pole, 3-ϕ induction motor is 80 kW. The rotor emf is observed to make 120 alterations per minute. Calculate

(*i*) Slip

(*ii*) Rotor speed

(*iii*) Mechanical power developed

(*iv*) Rotor copper loss per phase

(*v*) Rotor resistance per phase if rotor current is 60 A. 7

5. (*a*) Which type of alternator is used in hydro-electric power plants and why ? 2

(*b*) Explain with vector diagram how a rotating field is created by the three-phase stator winding.

(*Turn Over*)

2. (*a*) What are the different vector groups of 3-ϕ transformer winding connections ?

(*b*) Derive the equation for distribution factor of an alternator. State the expression for emf equation of an alternator showing the effect of pitch factor and distribution factor. 5

(*c*) A 1200 kVA, 3300 V, 50 Hz, 3-phase star-connected alternator has armature resistance of 0·25 Ω per phase. A field current of 40 A produces a short-circuit current of 200 A and an open-circuit emf of 1100 V line-to-line value. Calculate the regulation on

(*i*) full-load 0·8 pf lagging. 7

(*ii*) full-load 0·8 pf leading.

3. (*a*) What is the function of thermal overload relay and fuses present in the Direct-on line starter of an Induction Motor ? 2

(*b*) Explain the parallel operation of alternator by dark and bright lamp method. 5

(*c*) What do you mean by armature reaction of a synchronous generator ? Explain with phasor

(*Continued*)

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otal Pages—4 V—Sem/ELECT/2017(W) (New)

ENERGY CONVERSION-II

(Code : EET-501)

Full Marks : 70

Time : 3 hours

Answer any **five** questions

Figures in the right-hand margin indicate marks

1. (*a*) What are the different modes of operation of an Induction Machine ? In which operating mode, the developed torque opposes the rotation of the rotor. 2

(*b*) Derive the relation between full-load torque and starting torque in case of a 3-ϕ Induction Motor. 5

(*c*) A 6-pole, 50 Hz, 3-ϕ Induction Motors has rotor resistance and reactance per phase of 0·02 Ω and 0·1 Ω respectively. At what speed is the torque maximum ? What must be the value of external rotor resistance/phase to produce two-third of the maximum torque at starting ? 7